

Modelling of gyration effects on jets in crossflow

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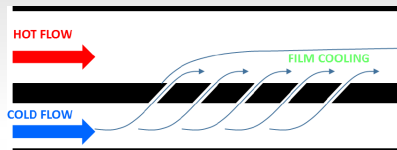


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Journée thématique SFT
Aérodynamique des systèmes propulsifs pour l'aéronautique
Paris, 20 octobre 2022

Introduction

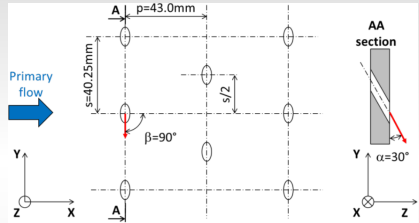
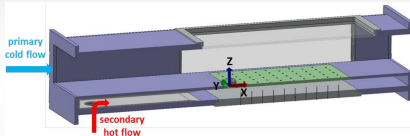
- ✓ European project SOPRANO
- ✓ Collaboration ONERA
Toulouse/LMAP: effects of gyration on effusion cooling
- ✓ Experiments (ONERA) and second-moment RANS simulations (LMAP)
- ✓ Challenges
 - ▷ Complex physics: jet/boundary layer interaction with gyration, and jet/jet interactions
 - ▷ Importance of the wall/turbulence interaction for heat transfer
- ✓ Questions:
 - ▷ Is the second-moment closure (EB-RSM) sufficiently robust for this type of problems
 - ▷ Accuracy? Superiority to standard eddy-viscosity models?
- ✓ Mid-term objective: proposing a reliable and low-cost approach
 - ▷ Parametric studies
 - ▷ Develop homogeneous or heterogeneous boundary conditions for industrial computations and/or LES



Outline of the presentation

- ✓ Experimental configuration
- ✓ Simulations
 - ▷ Presentation of the EB-RSM
 - ▷ Comparison with experiments
- ✓ Ongoing work
 - ▷ Presentation of the hybrid RANS-LES approach (HTLES)
 - ▷ Some illustrative results

Configuration



✓ Geometry:

- ▷ 10 rows of 9 holes in staggered arrangement. Diameter $D = 5$ mm.
- ▷ Pitch angle $\alpha = 30^\circ$. Yaw angle $\beta = 90^\circ$ (gyration).
- ▷ Spacing: $s = 8.05D$ and $p = 8.6D$

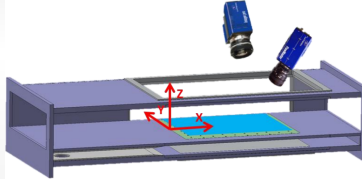
✓ Flows:

- ▷ Main: 3.39 m s^{-1} ($Re_p = 45500$)
- ▷ Secondary 2.88 m s^{-1} ($Re_s = 10400$)
- ▷ Leads to 26 m s^{-1} inside the holes: $V_j/V_p = 7.88$
- ▷ Momentum flux ratio $I = \rho_j V_j^2 / \rho_p V_p^2 = 58.2$

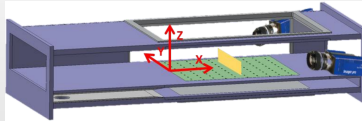
Experimental database

✓ Velocity measured by stereo-PIV

▷ Horizontal planes at $z/D = 1.16; 2.36; 3.96; 5.26; 6.96; 8.36$



▷ Vertical planes at constant x through the first 4 rows and inter-rows

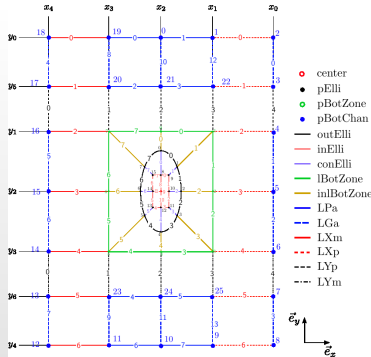


✓ Temperature field: cold wires

✓ Surface temperatures: infrared thermography

Presentation of the simulations

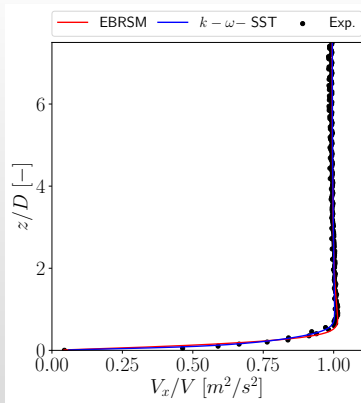
- ✓ Open-source code Code_Saturne developed by EDF (Archambeau et al., 2004)
- ✓ RANS models: EB-RSM and $k-\omega$ -SST for comparison
- ✓ Structured mesh generated with Gmsh by duplication of the 1-hole pattern



- ✓ Refined near-wall mesh ($y^+ = 1$ criterion), geometric expansion
- ✓ Grid convergence checked (4 grid levels). Results plotted for 70×10^6 cells

Presentation of the simulations

- ✓ Experimental profile available in the boundary layer at $3.05D$ upstream of the first row (location $x = 0$)
- ✓ Generation of the inlet conditions:
 - ▷ Precursor simulation of a developing boundary layer
 - ▷ Extraction of the profile corresponding to the correct boundary layer thickness
 - ▷ Make possible the injection at the inlet of all the variables of the model (velocities, Reynolds stresses, dissipation)

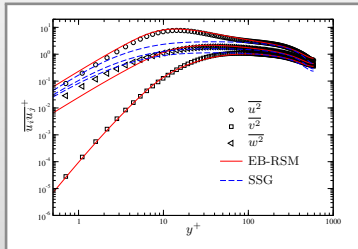
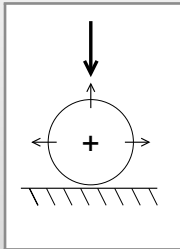


Second-moment closure EB-RSM

- ✓ Eddy-viscosity models: $\overline{u_i u_j} = -2\nu_t S_{ij} + \frac{2}{3}k\delta_{ij}$
- ✓ Second-moment closures (RSM): Reynolds-stress transport equations

$$\begin{aligned} \frac{d\overline{u_i u_j}}{dt} = & \underbrace{\nu \frac{\partial^2 \overline{u_i u_j}}{\partial x_k \partial x_k}}_{D_{ij}^\nu} - \underbrace{\frac{\partial \overline{u_i u_j u_k}}{\partial x_k}}_{D_{ij}^T} - \underbrace{\frac{1}{\rho} \overline{u_i \frac{\partial p}{\partial x_j}} - \frac{1}{\rho} \overline{u_j \frac{\partial p}{\partial x_i}}}_{\phi_{ij}^*} \\ & - \underbrace{\overline{u_i u_k} \frac{\partial U_j}{\partial x_k} - \overline{u_j u_k} \frac{\partial U_i}{\partial x_k}}_{P_{ij}} - \underbrace{2\nu \frac{\partial \overline{u_i}}{\partial x_k} \frac{\partial \overline{u_j}}{\partial x_k}}_{\varepsilon_{ij}} \end{aligned}$$

- ✓ Influence of the wall: nonlocal blockage effect $\Rightarrow$ two-component limit



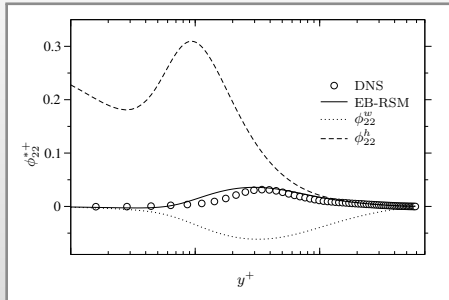
Second-moment closure EB-RSM

✓ Elliptic relaxation (Durbin) : $(1 - L^2 \nabla^2) \frac{\phi_{ij}^*}{\lambda} = \frac{\phi_{ij}^h}{\lambda} \Rightarrow 6$ additional equations, unstable

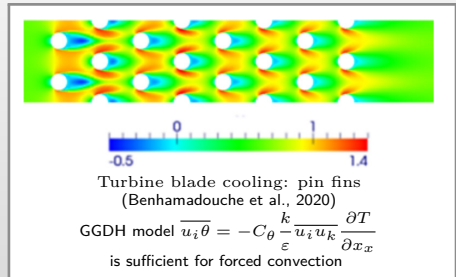
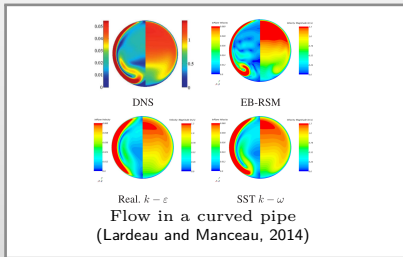
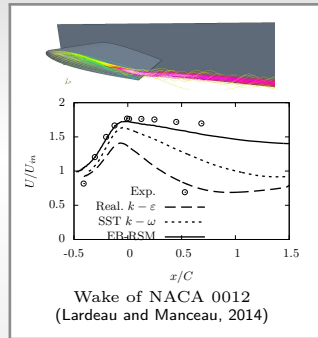
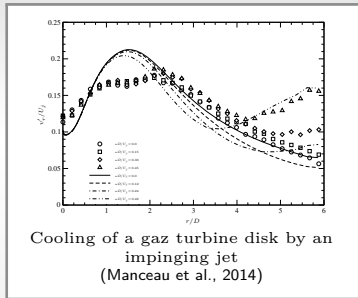
✓ Elliptic blending:
$$\begin{cases} (1 - L^2 \nabla^2) \alpha = 1 \\ \phi_{ij}^* = (1 - \alpha^3) \phi_{ij}^w + \alpha^3 \phi_{ij}^h \end{cases}$$

✓ Taylor series expansion

$$\Rightarrow \phi_{ij}^w = -5 \frac{\varepsilon}{k} \left[\overline{u_i u_k} n_j n_k + \overline{u_j u_k} n_i n_k - \frac{1}{2} \overline{u_k u_l} n_k n_l (n_i n_j + \delta_{ij}) \right]$$



EB-RSM: examples of applications



Applications by other groups

Compressor blades

(Borello et al., 2005)

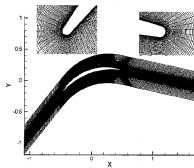


Fig. 10 DCA cascade—computational mesh (coarse discretization)

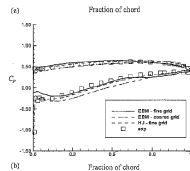


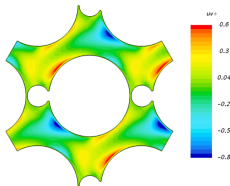
Fig. 11 DCA cascade— C_p distribution: (a) HJ simulations and (b) EBM simulations



Control by vortex generators
(Törnblom and Johansson, 2007)

Assemblage combustible

(Dovizio et al., 2019)

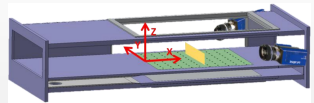
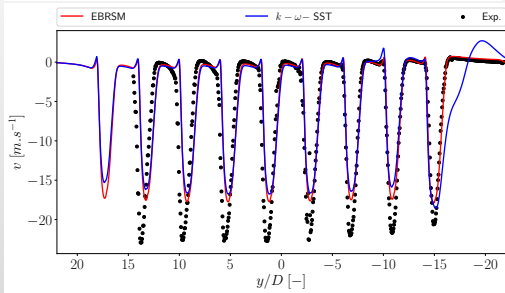
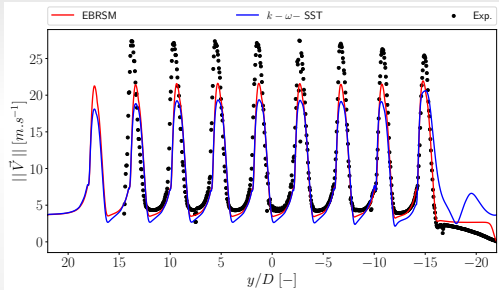


And many others

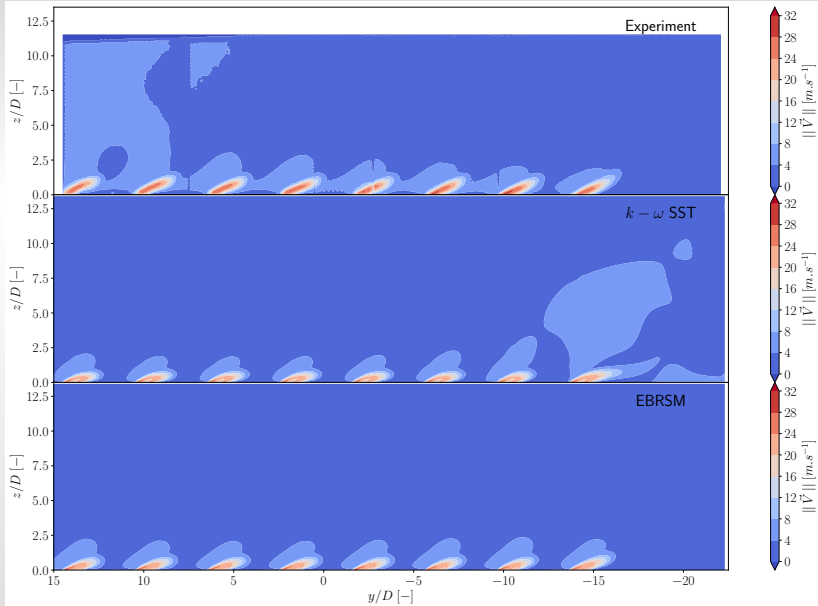
- ✓ 50 groups (incl. MIT, Stanford, Oxford, Imperial C., KTH, Chalmers, ...) in 15 countries
- ✓ In Code_Saturne (EDF, open-source)
- ✓ In CEDRE, AETHER
- ✓ In OpenFOAM
- ✓ In StarCCM+

Comparison with experiments

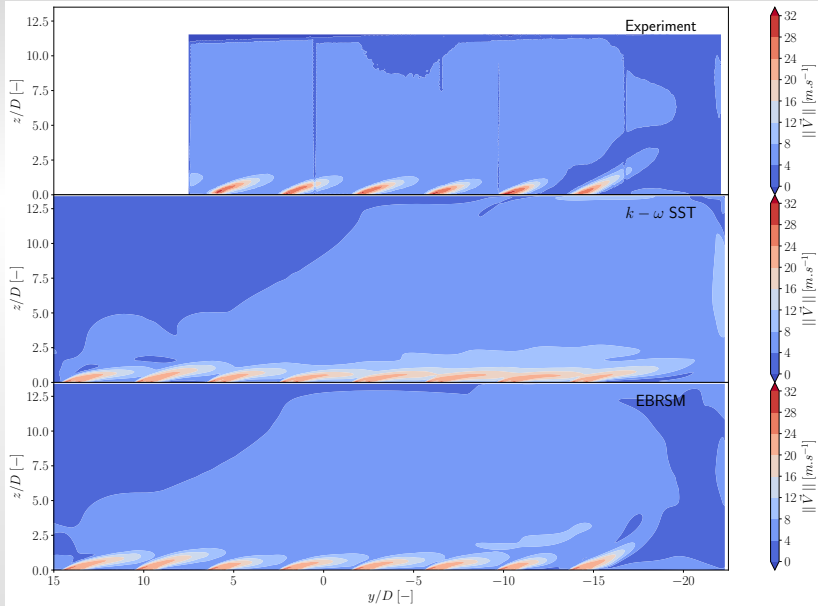
Velocity field



Profiles along the line
above the first row, at
 $x = 3.05D$ and $z = 0.58D$

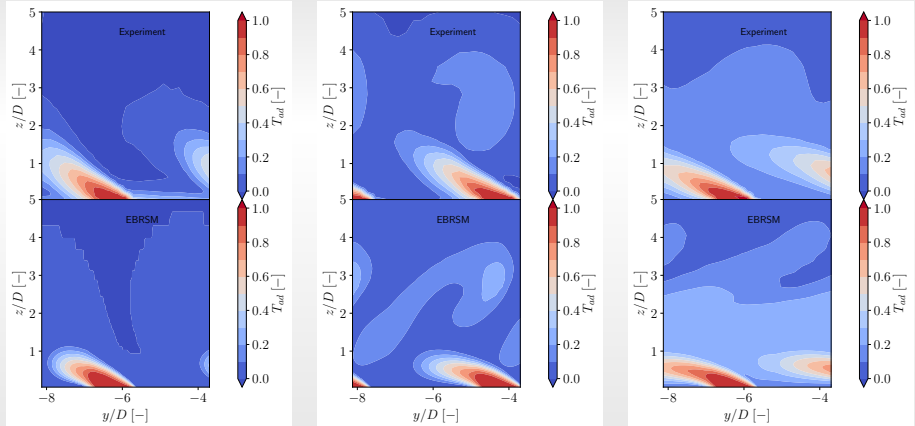


Isocontours of velocity magnitude in the plane $x/D = 0.305$ (row 1)



Isocontours of velocity magnitude in the plane $x/D = 1.165$ (row 3)

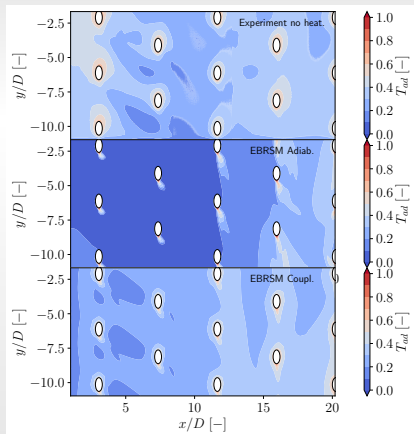
Temperature field



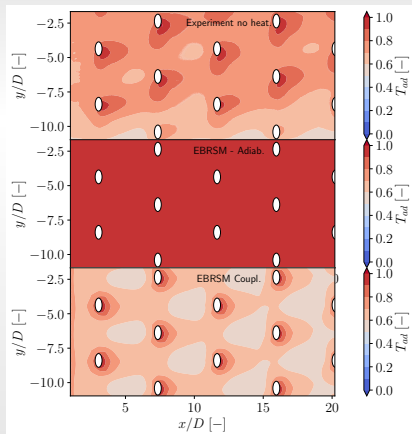
Non-dimensional temperature field in the planes

$x/D = 0.305; 0.735; 1.165$ (rows 1, 2 and 3)

Wall temperature

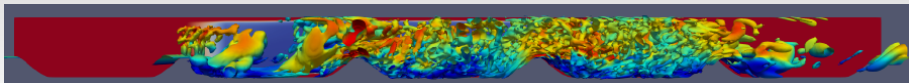


Upper surface of the plate.



Lower surface of the plate.

Hybrid RANS-LES approach



Example of a periodic hill flow

HTLES $\rightarrow$ k - ω -SST

$$\nu_{\text{sfs}} = \frac{k_{\text{sfs}}}{\psi_{\omega}(r) \omega_{\text{sfs}}^*}$$

$$\begin{cases} \frac{Dk_{\text{sfs}}}{Dt} = P_{k_{\text{sfs}}} + D_{k_{\text{sfs}}} - \frac{k_{\text{sfs}}}{T(r)} \\ \frac{D\omega_{\text{sfs}}^*}{Dt} = \gamma_{\omega} \frac{\omega_{\text{sfs}}^*}{k_{\text{sfs}}} P_{\text{sfs}} + D_{\omega_{\text{sfs}}}^* - \beta_{\omega} \omega_{\text{sfs}}^{*2} + C_{\omega_{\text{sfs}}}^* \end{cases}$$

$$T_m = \frac{r}{\psi_{\omega}(r)} \frac{k}{C_{\mu} k_m \omega_m^*} \quad \psi_{\omega}(r) = \frac{\beta_{\omega}}{C_{\mu} \gamma_{\omega} + r(\beta_{\omega} - C_{\mu} \gamma_{\omega})}$$

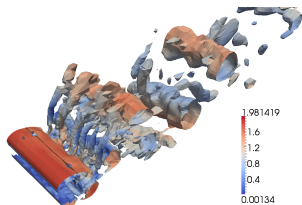
Energy ratio:
$$r = \frac{k_m}{k} = \frac{1}{\beta_0} \left(\frac{U_S}{\sqrt{k}} \right)^{2/3} \left(\omega_c \frac{k}{\varepsilon} \right)^{-2/3}$$

Cutoff frequency:
$$\omega_c = \min \left[\frac{\pi}{dt}; \frac{U_S \pi}{\Delta} \right]$$

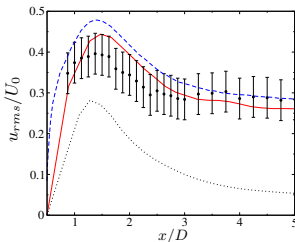
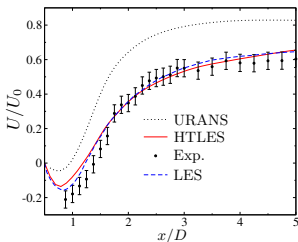
Model available in StarCCM+ under the name SRH

Square-sectioned cylinder

(Tran, Manceau, Perrin, Borée, and Nguyen)



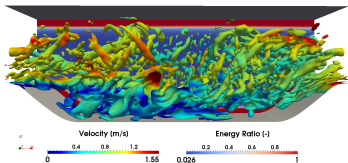
- ✓ $Re = 21400$
- ✓ Code_Saturne
- ✓ HTLES – $k-\omega$ -SST
- ✓ 0.5×10^6 cells



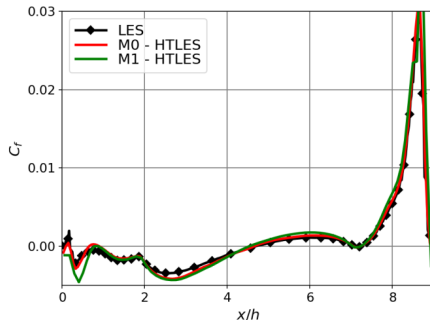
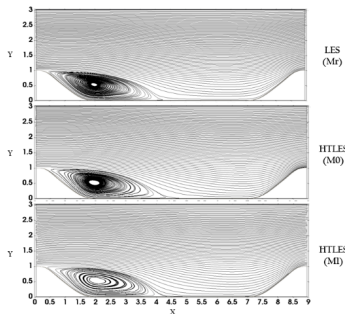
- ✓ Exp.: Lyn et al., 1995
- ✓ LES: Cao and Tamura, 2016 with 75×10^6 cells (factor 150)

Periodic hills

(Duffal2021b)

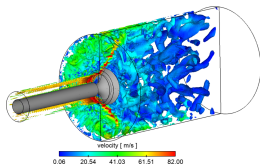


- ✓ $Re_b = 10600$
- ✓ Ref. LES by Breuer et al., 2006 with 12×10^6 cells
- ✓ Code_Saturne
- ✓ HTLES – $k-\omega$ -SST and HTLES – $BL-\overline{v^2}/k$
- ✓ $M0=160 \times 160 \times 80 = 2 \times 10^6$ cells (factor 6)
- ✓ $M1=80 \times 80 \times 40 = 256,000$ cells (factor 50)

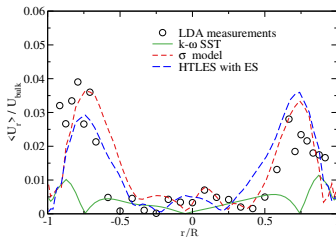
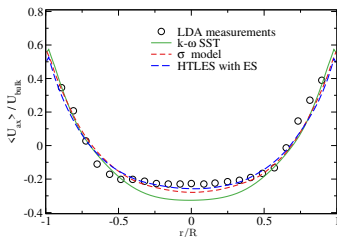


Simplified internal combustion engine

(Afailal et al., 2019)

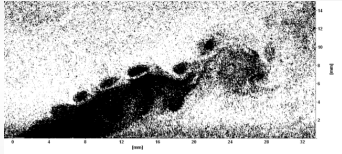


- ✓ Exp. by Dellenback et al., 1988
- ✓ Ref. LES by Thobois et al., 2004
- ✓ $Re_b = 30000$
- ✓ Code = *CONVERGE*
- ✓ HTLES – $k-\omega$ -SST
- ✓ 1.4×10^6 cells

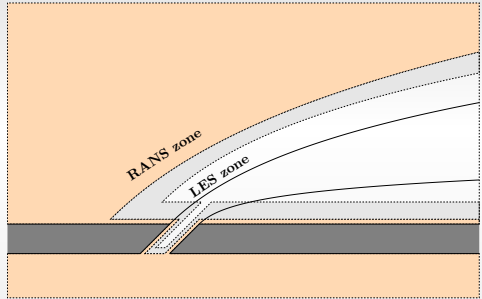


	EXP	RANS	HTLES	LES
ΔP [Pa]	1766	1713	1705	1957
Error [%]		-3	-3	+11

Single jet in crossflow



MAVERIC facility



(Q-isocontours)

Acknowledgements

- ✓ Project funded by the H2020 project SOPRANO (grant agreement 690764) and the ASTURIES project (grant E2S-20-ScientificChallenges-01) of E2S UPPA (ANR-16-IDEX-0002).
- ✓ Simulation tool: Code_Saturne (Archambeau et al., 2004)
- ✓ Computing resources: MCIA, Bordeaux and GENCI-IDRIS (Grant 2022-A0122A10980).

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Grid convergence study

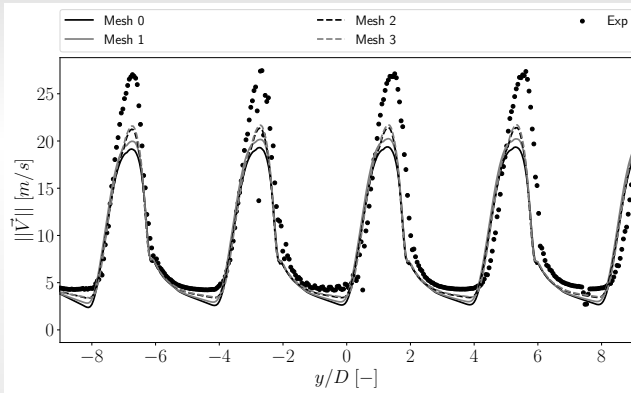


Figure: Velocity magnitude obtained with the $k\text{-}\omega\text{-SST}$ model extracted along the line above the first row, defined by $x = 3.05D$, at the elevation $z = 0.58D$, for the 4 meshes, compared with the experiments.