

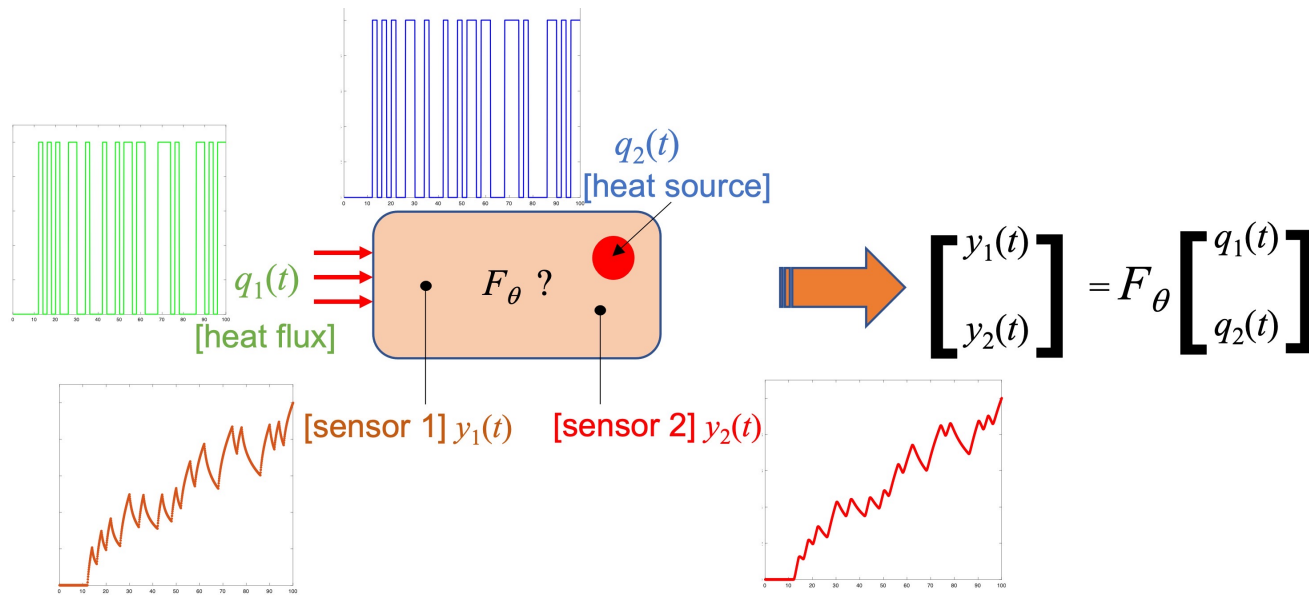
Identification de systèmes thermiques linéaires et non linéaires par des structures mathématiques d'intégration d'ordre non entier

Identification of linear and non linear thermal systems from non integer integral mathematical structures

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Journée SFT : Inversion de données faisant appel à un modèle en thermique, quels apports de l'intelligence artificielle ?

System identification

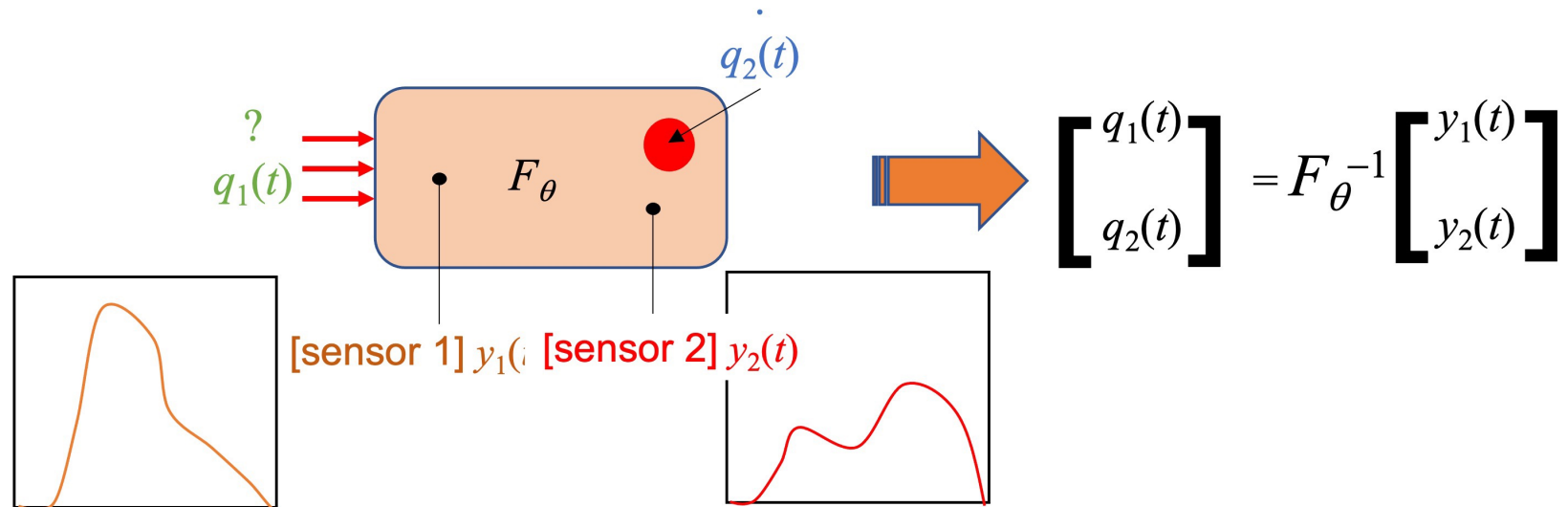


A model F_θ that relates the temperature change $y_j(t)$, $j=1,\dots,N_c$, of sensors to the thermal BC $q_i(t)$, $i=1,\dots,N_q$ (can be either a temperature, a heat flux or a source) is **identified** from measurements of those quantities.

The model « learns » from the data

Potential applications

- Simulation
- Control
- Estimation of $q(t)$ (IHCP)
- ...



F_θ model structure (monovariable system)

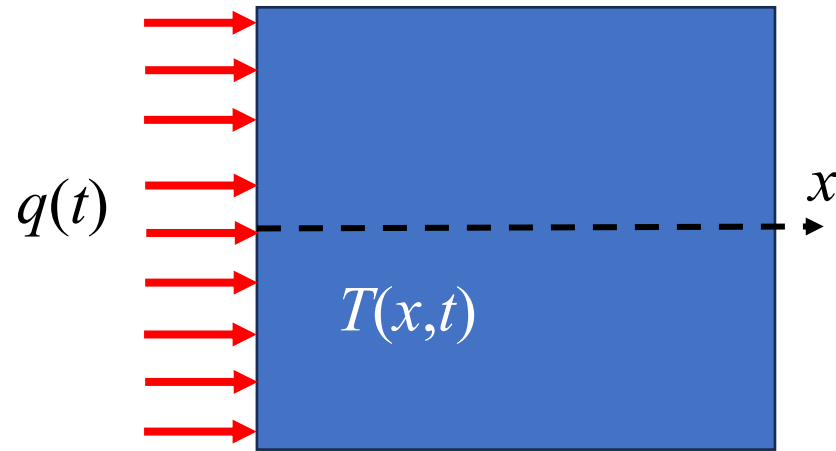
$$\sum_{k=0}^{\infty} a_k D^k \{y(t)\} = \sum_{k=0}^{\infty} b_k D^k \{q(t)\} + \varepsilon(t), \quad a_0 = 1$$

$$D^k \{f(t)\} = d^k f(t) / dt^k$$

Using finite difference discretization for the derivatives, the relation is equivalent to the family of exogenous auto-regressive structures (AR, ARMA, ARMAX, OE, etc.)

$$\sum_{k=0}^{\infty} \alpha_k y(t-k) = \sum_{k=0}^{\infty} \beta_k q(t-k) + \varepsilon(t), \quad a_0 = 1$$

Heat diffusion in a semi-infinite medium



$$\theta(x, p) = H(x, p) Q(p)$$

$$H(x, p) = \frac{e^{-\frac{x}{\sqrt{\alpha}} \sqrt{p}}}{\lambda \sqrt{p/\alpha}} = \frac{e^{-\frac{x}{\sqrt{\alpha}} \sqrt{p}}}{E \sqrt{p}}$$

At $x = 0$

$$H(0, p) = \frac{1}{E \sqrt{p}}$$

Let us recall that the solution is: $T(0, t) = \frac{1}{E \sqrt{\pi} \sqrt{t}} * q$

The non integer derivative

$$\mathcal{L} \left(\frac{d^v f(t)}{dt^v} \right) = s^v F(s) - \sum_{k=0}^{n-1} s^{n-k-1} \frac{d^k f(0)}{dt^k}$$

Liouville demonstrated that this definition remains exact when v is a real and even more generally a complex number

$$D^v \{f(t)\} = D^n \{I^{n-v} \{f(t)\}\}, n \in \mathbb{N}, \operatorname{Re}(v) > 0, n-1 \leq \operatorname{Re}(v) < n$$

Non-integer derivative

$$I^v \{f(t)\} = \frac{1}{\Gamma(v)} \int_0^t (t-u)^{v-1} f(u) du, \operatorname{Re}(v) > 0$$

Non-integer integral

$$\Gamma(v) = \int_0^\infty u^{v-1} \exp(-u) du$$

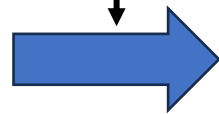
Convolution product of $f(t)$ with t^{v-1} (infinite memory)

New expression of the solution using the non-integer model structure

$$\mathcal{L}^{-1} \left(\frac{1}{\sqrt{p}} F(p) \right) = \mathcal{I}^{1/2} \{f(t)\}$$

If one wants to use the integer structure, an infinite number of terms must be considered

$$H(0, p) = \frac{1}{E \sqrt{p}}$$



$$T(0, t) = \frac{1}{E} \mathcal{I}^{1/2} q$$

$$T(x, t) = \sum_{n=0}^{\infty} b_n \mathcal{I}^{n/2} \{q(t)\}$$

Optimal model structure for this configuration:

$$y = \beta_1 \mathcal{I}^{1/2} q + \varepsilon$$

$$\beta_{1, \text{th}} = 1/E$$

How to calculate the non integer integral ?

Several discretization schemes (Grünwald for instance)

$$D^\nu f(t_0) \sim \frac{1}{h^\nu} \sum_{k=0}^{n-1} (-1)^k \binom{\nu}{k} f(t_0 - kh), \quad \nu > 0 \quad \binom{\nu}{k} = \frac{\nu(\nu-1)\cdots(\nu-k+1)}{k!}$$

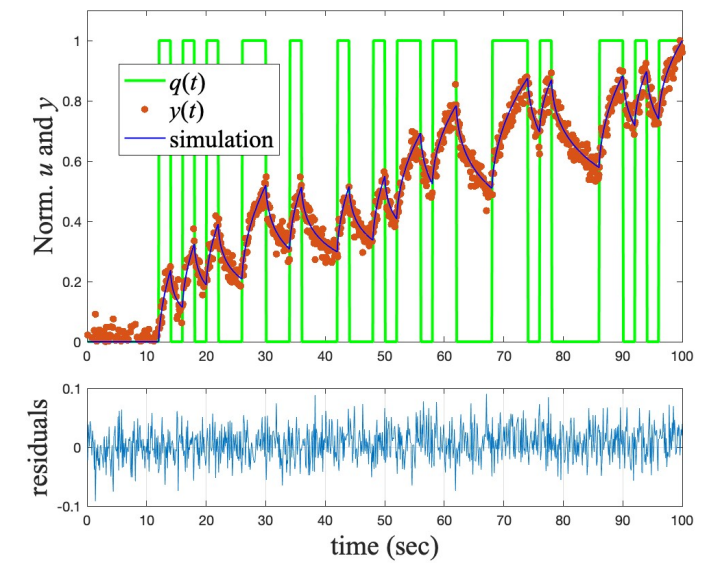
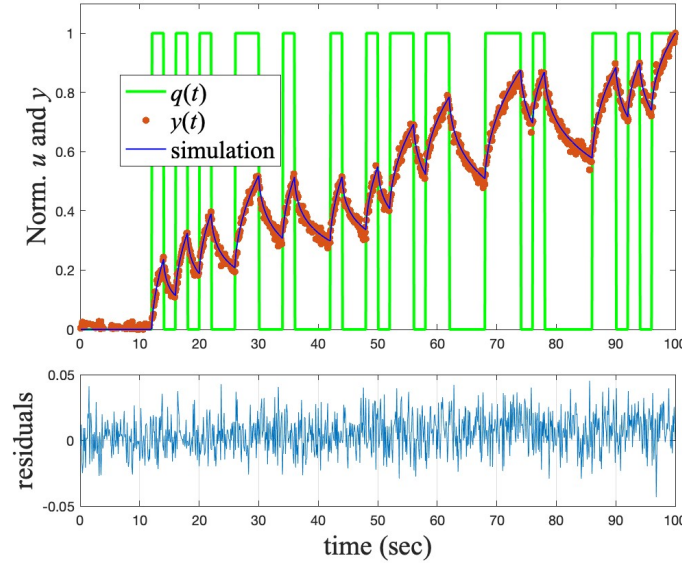
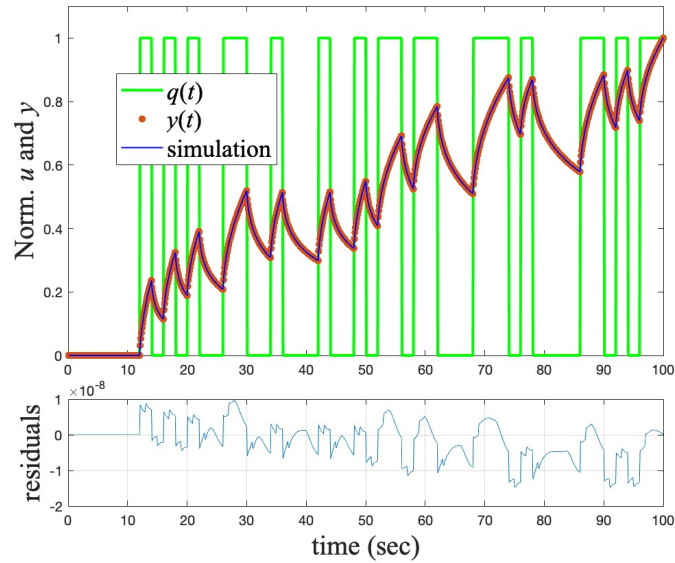
Another way:

$$I^\nu \{f(t)\} = \frac{1}{\Gamma(\nu)} \int_0^t (t-u)^{\nu-1} f(u) du, \operatorname{Re}(\nu) > 0 \quad \longrightarrow \quad I^\zeta \{f(t)\} = \mathcal{L}^{-1} \left(\frac{1}{p^\zeta} \right) * f(t) = \frac{t^{\zeta-1}}{\Gamma(\zeta)} * f(t), \quad \zeta \geq 0$$

FFT is fast

$$\frac{t^{\zeta-1}}{\Gamma(\zeta)} * f(t) = \text{FFT}^{-1} \left[\text{FFT} \left[\frac{t^{\zeta-1}}{\Gamma(\zeta)} \right] \times \text{FFT} [f(t)] \right]$$

Illustration



$$y(t) = T(0, t) + \varepsilon N(t) \quad (\text{simulated from the exact solution})$$

Noise amp.	$\beta_{1,\text{id}}$ (LS, RLS)	$\beta_{1,\text{th}} = 1/E$
$\varepsilon = 0$	$1.26 \times 10^{-4} \pm 1.82 \times 10^{-14}$	1.26×10^{-4}
$\varepsilon = 5\%$	$1.26 \times 10^{-4} \pm 1.0 \times 10^{-7}$	1.26×10^{-4}
$\varepsilon = 10\%$	$1.26 \times 10^{-4} \pm 2 \times 10^{-7}$	1.26×10^{-4}

The parameter identification is based on the linear least squares (recursive RLS or not LS)

What happens if the sensor is located at $x > 0$

$$\exp(z) = \sum_{n=0}^{\infty} z^n / n! \quad \Rightarrow \quad H(x, p) = \sum_{n=0}^{\infty} \frac{\left(-\frac{x}{\sqrt{\alpha}} \sqrt{p}\right)^n}{n! E \sqrt{p}} = \frac{1}{E \sqrt{p}} \left(1 + \sum_{n=1}^{M \rightarrow \infty} \frac{-x^n}{\alpha^{n/2} n!} p^{n/2}\right)$$

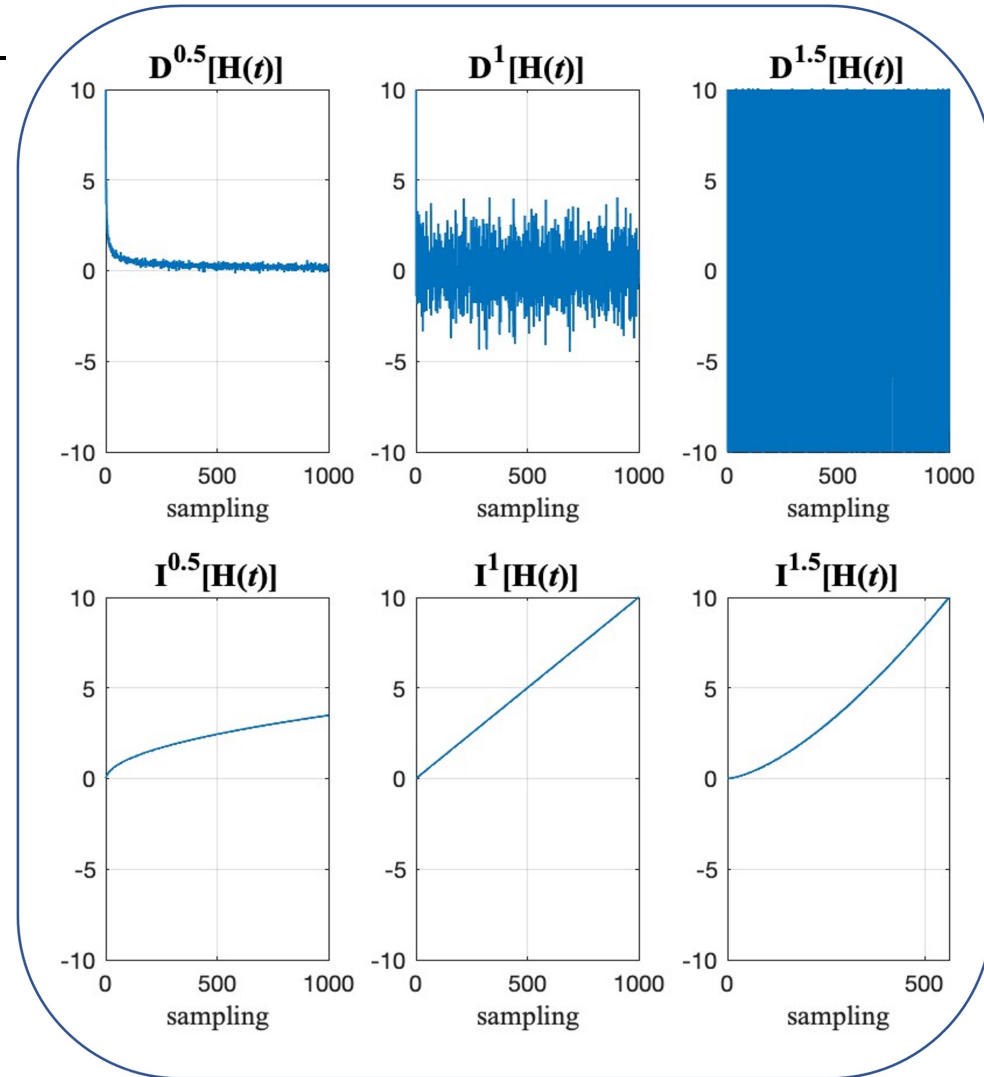
$$\boxed{x = 1 \text{ mm}} \quad \boxed{M = 2} \quad H(x, p) = \frac{1}{\sqrt{p}} (b_0 + b_1 p^{1/2} + b_2 p), \quad b_0 = \frac{1}{E}, \quad b_1 = -\frac{x}{\sqrt{\alpha} E}, \quad b_2 = \frac{x^2}{2 \alpha E}$$

$$H(x, p) = \frac{b_0 p^{-1} + b_1 p^{-1/2} + b_2}{p^{-1/2}} \quad \Rightarrow \quad \boxed{\mathcal{I}^{1/2} y = \beta_0 \mathcal{I} q + \beta_1 \mathcal{I}^{1/2} q + \beta_2 q + \mathcal{I}^{1/2} \varepsilon}$$

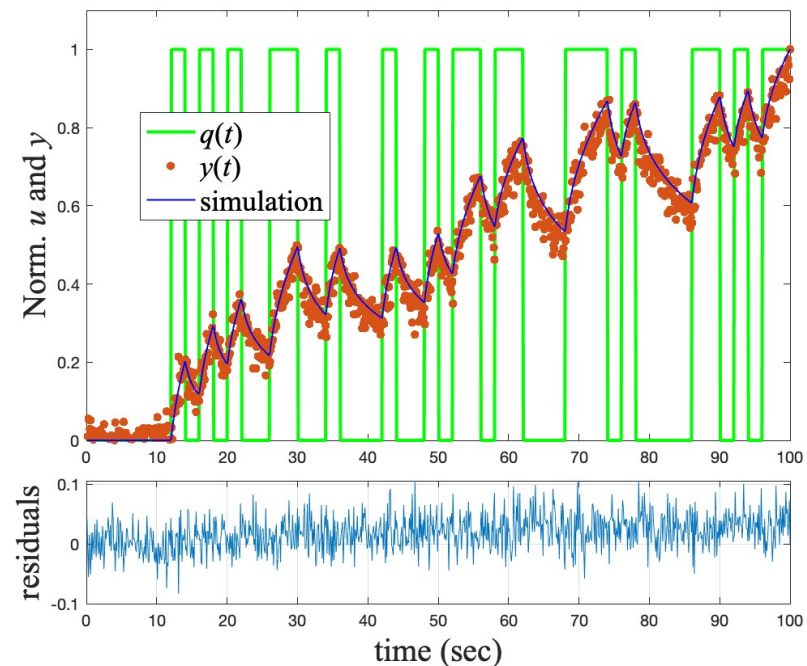
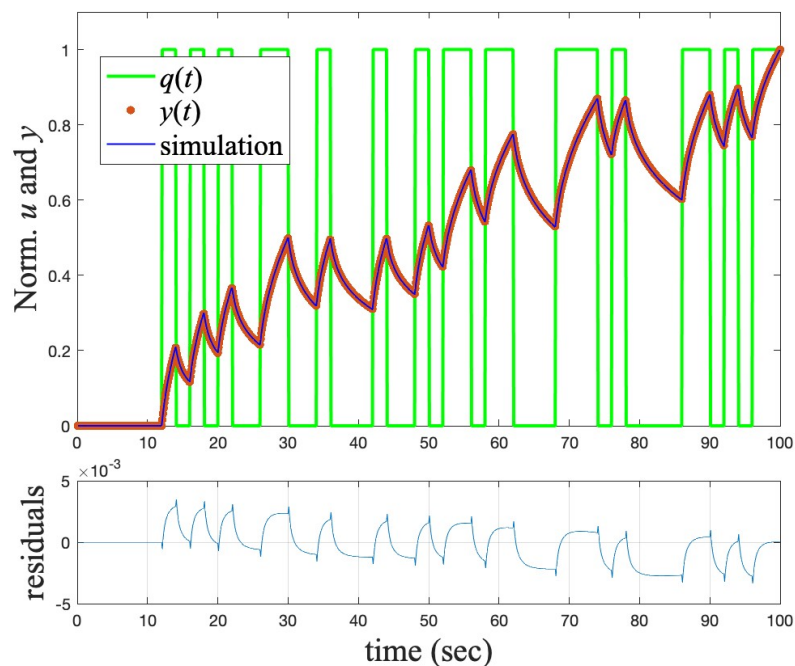
Why using the NI integral instead of the NI derivative ?

$U(t) = H(t)$ is the Heaviside function

$$U_{\varepsilon}(t) = U(t) + \varepsilon N(t)$$



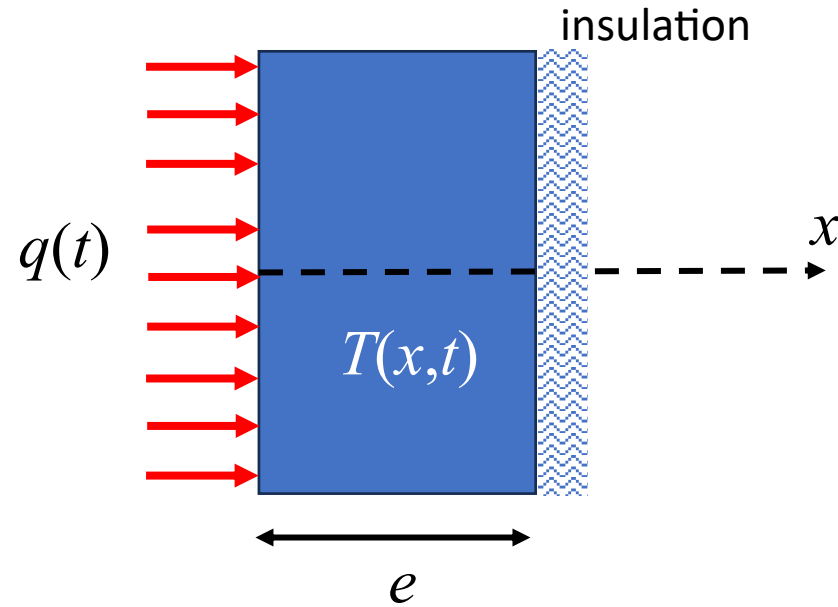
Illustration



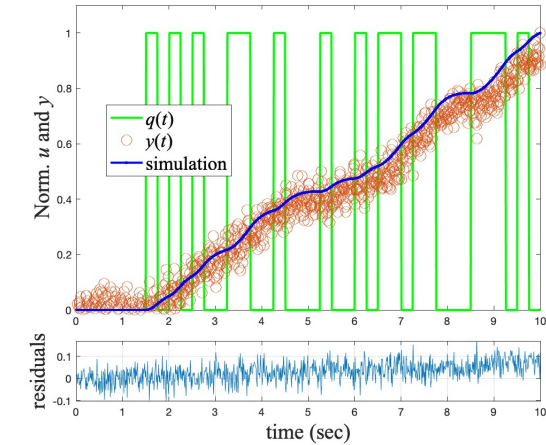
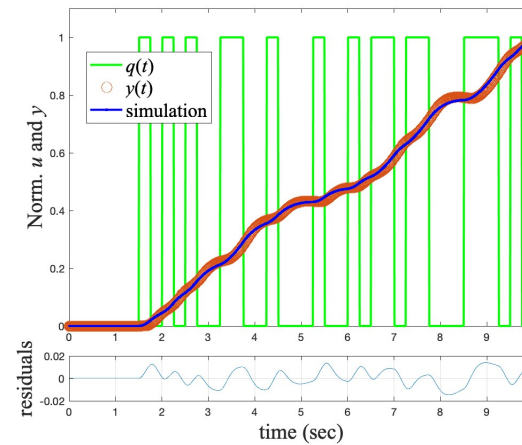
$$y(t) = T(0, t) + \varepsilon N(t) \quad (\text{simulated from the exact solution})$$

Noise amp.	β_0	β_1	β_2
theoretical values	1.261×10^{-4}	-6.67×10^{-5}	1.76×10^{-5}
id. values, $\varepsilon = 0$	$1.255 \times 10^{-4} \pm 1.67 \times 10^{-5}$	$-9.523 \times 10^{-5} \pm 1.27 \times 10^{-4}$	$1.3 \times 10^{-5} \pm 1.67 \times 10^{-4}$
id. values, $\varepsilon = 10\%$	$1.265 \times 10^{-4} \pm 1.65 \times 10^{-5}$	$-10.37 \times 10^{-5} \pm 1.27 \times 10^{-4}$	$1.7 \times 10^{-5} \pm 1.66 \times 10^{-4}$

Loss of the semi-infinite behaviour



$x = 3\text{mm}, e = 1\text{ cm}$

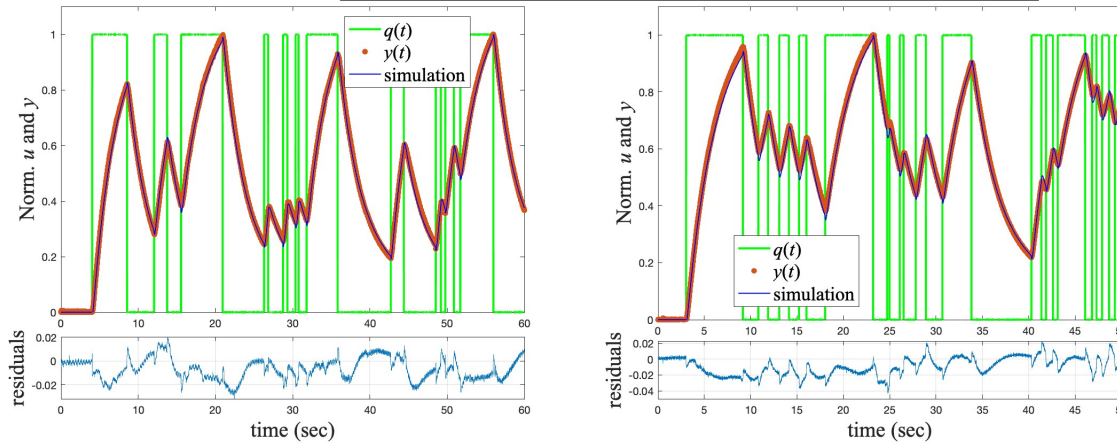


The best optimal structure is: $y + \alpha_1 I y = \beta_0 I^2 q + \beta_1 I^3 q + \beta_2 I^4 q$

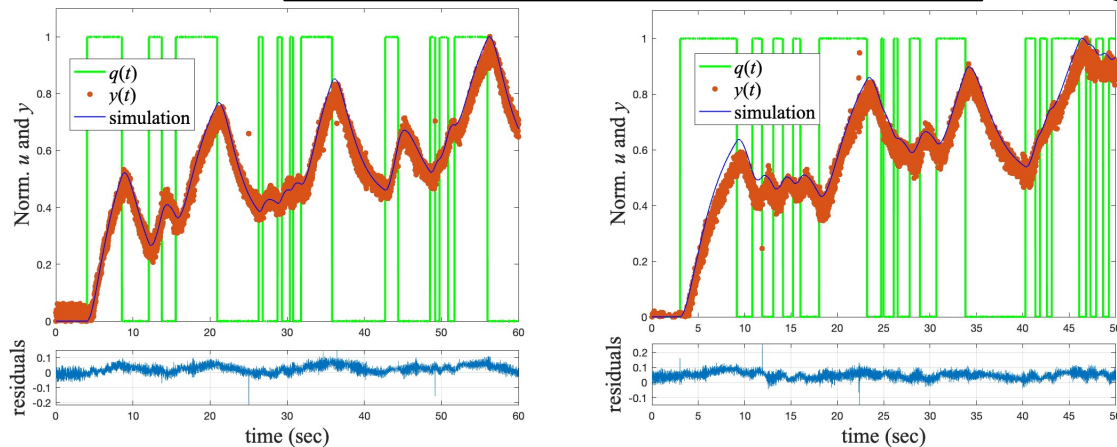
Can be derived from the exact solution of the transfer function: $H(x, p) = \frac{\cosh\left(\sqrt{p/\alpha}(e-x)\right)}{\lambda \sqrt{p/\alpha} \sinh\left(\sqrt{p/\alpha} e\right)}$

Real application

System identification for Sensor 1

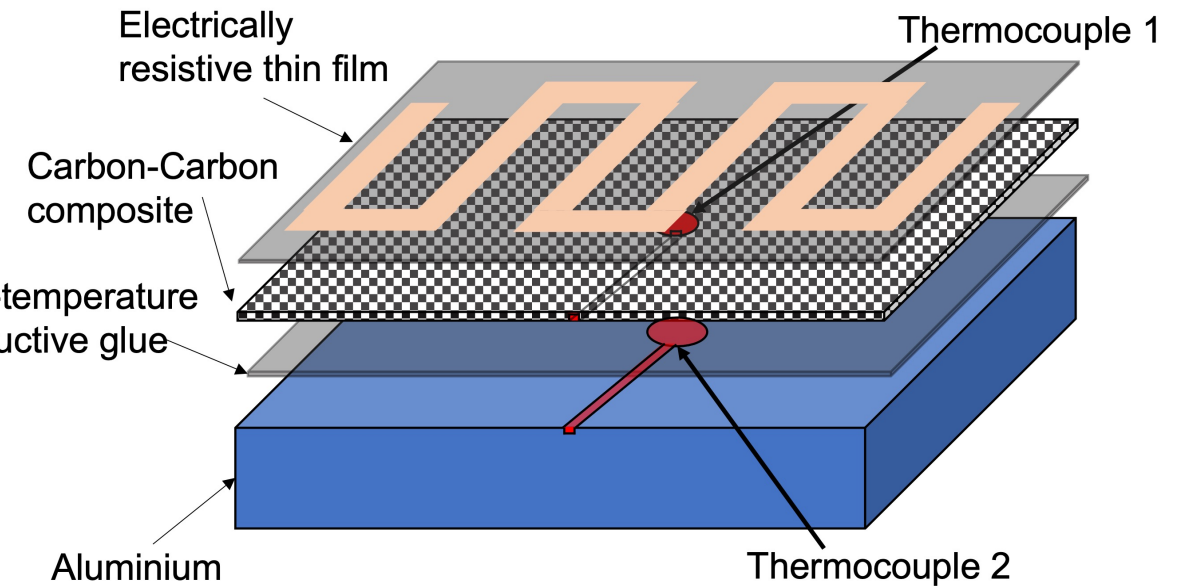


System identification for Sensor 2



Learning

validating

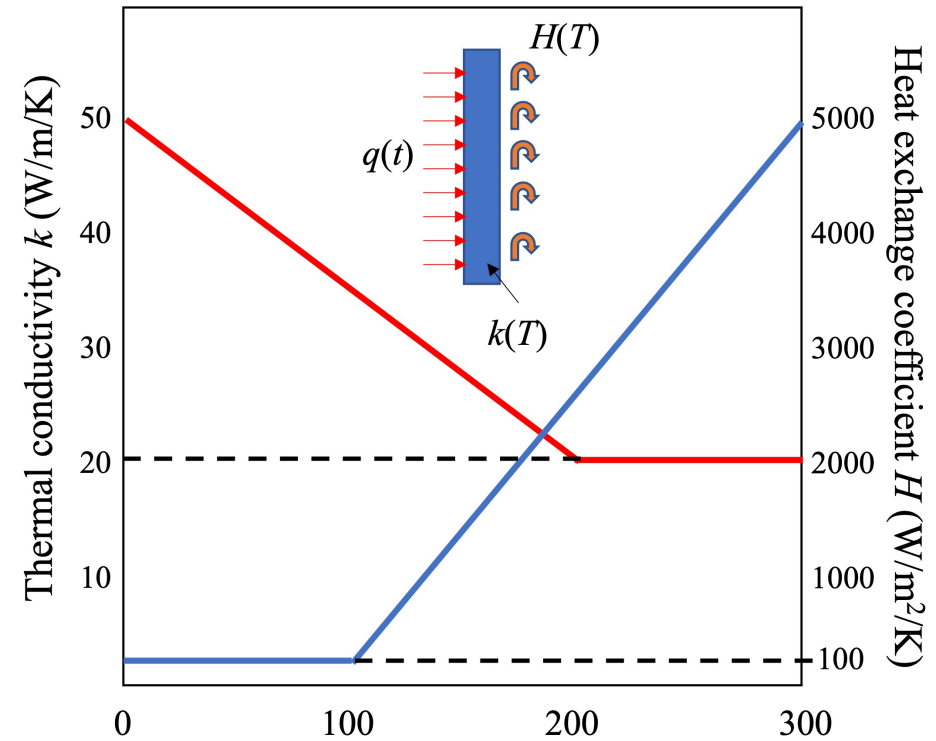
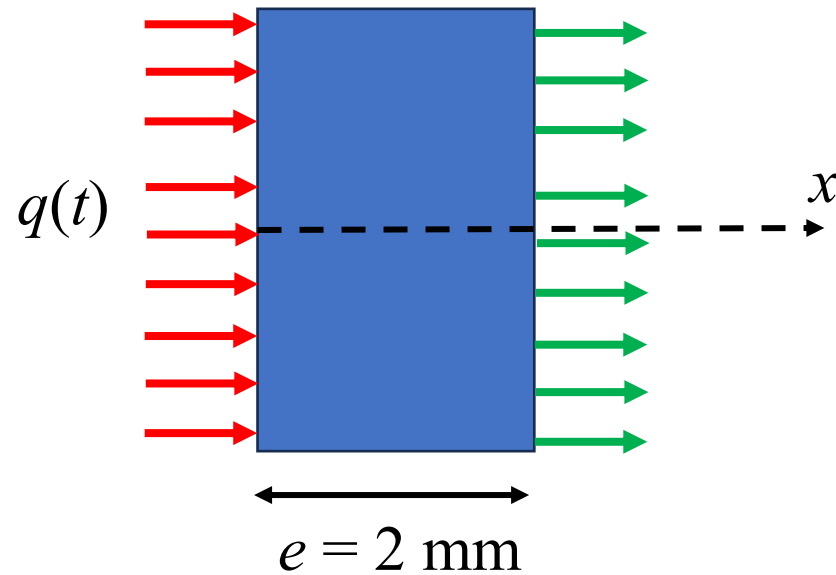


Identified models

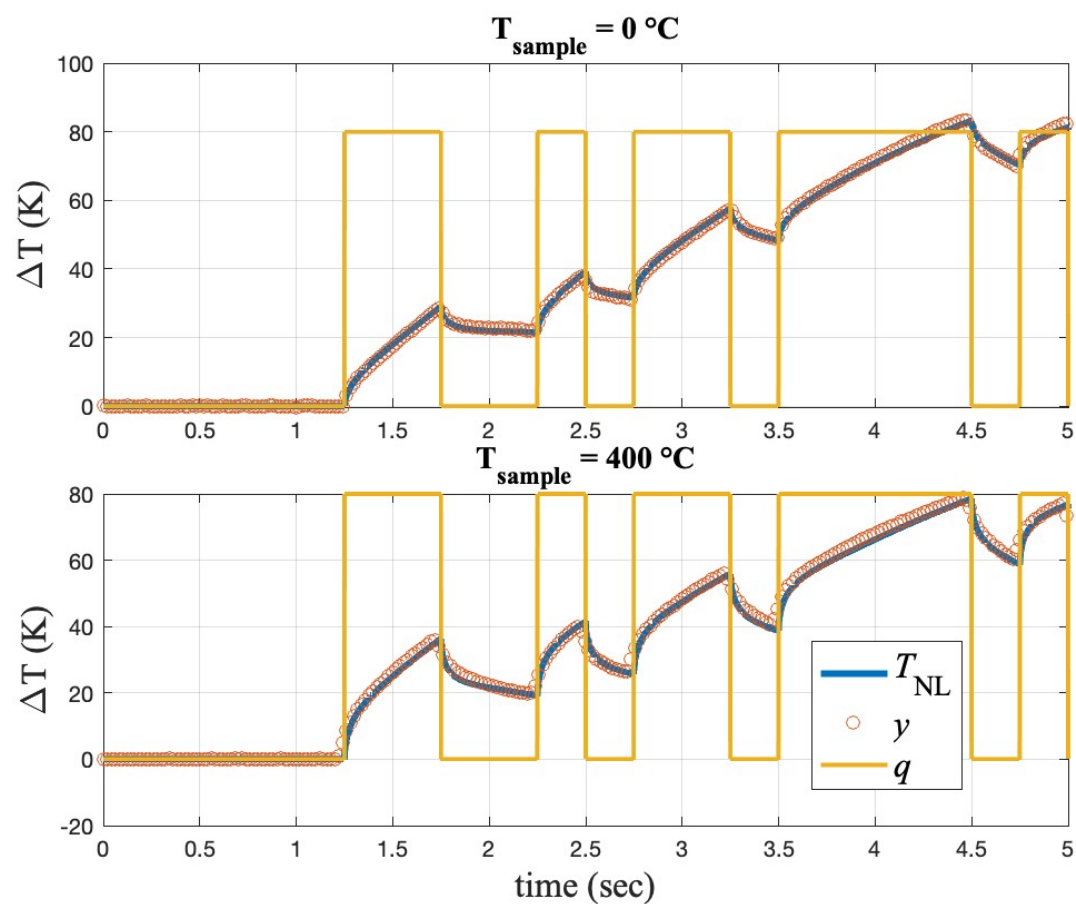
$y_1 = \beta_1 \text{I}^{0.5}q + \beta_2 \text{I}^1q + \beta_3 \text{I}^{1.5}q + \beta_4 \text{I}^2q + \beta_5 \text{I}^{2.5}q + \beta_6 \text{I}^3q + \beta_7 \text{I}^{3.5}q + \varepsilon(t)$							
parameter	β_0	β_1	β_2	β_3	β_4	β_5	
value	-0.9	3.04	-1.92	0.61	-0.1	0.007	
std	0.004	0.006	0.005	0.002	0.0004	3.5×10^{-5}	
$y_1 + \alpha_1 \text{I}^1y + \alpha_1 \text{I}^2y = \beta_1 \text{I}^2q + \beta_2 \text{I}^3q + \beta_3 \text{I}^4q + \beta_4 \text{I}^5q + \beta_5 \text{I}^6q + \varepsilon(t)$							
parameter	α_1	α_2	β_1	β_2	β_3	β_4	β_5
value	1.31	0.45	0.13	0.007	3.2×10^{-5}	-8.5×10^{-6}	2.67×10^{-7}
std	0.021	0.004	0.0017	0.0003	2.55×10^{-5}	1.84×10^{-6}	6.27×10^{-8}

The case of non-linear heat diffusion

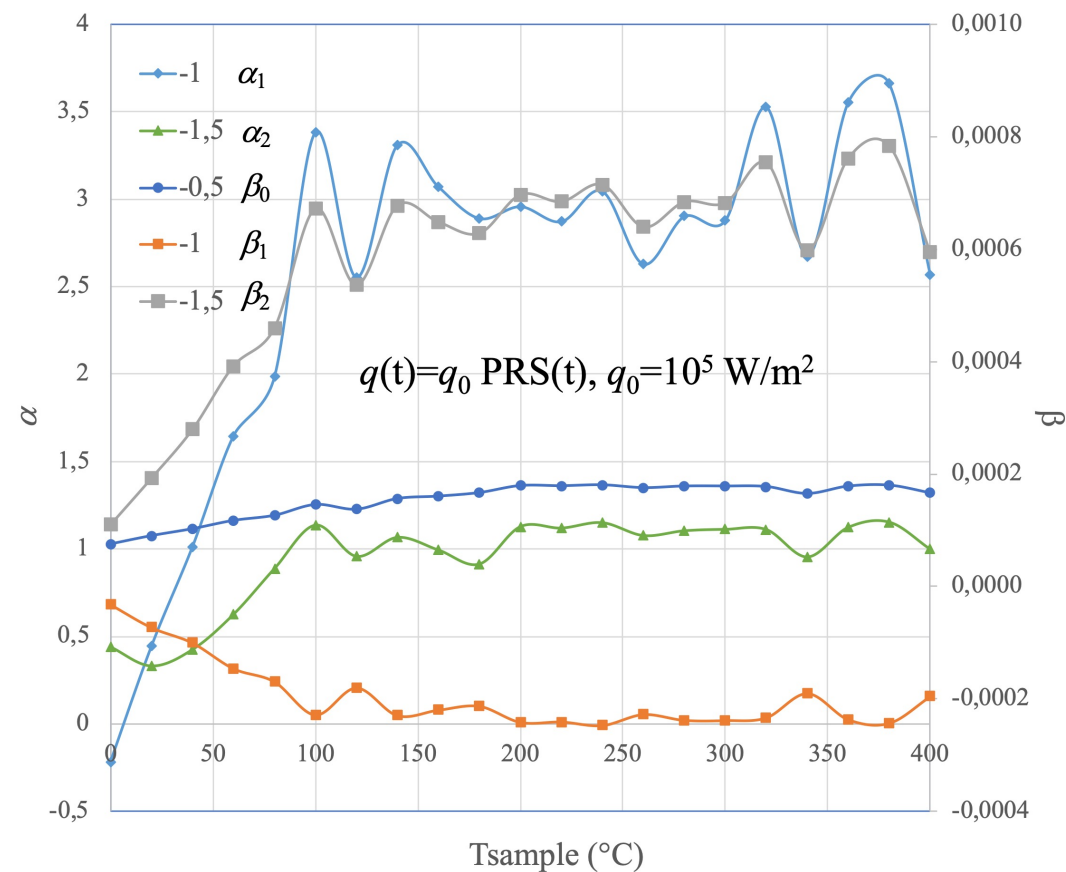
sensor $T(0,t)$



System identification



$$T + \alpha_1 I^1 q + \alpha_2 I^{1.5} q = \beta_0 I^{0.5} q + \beta_1 I^1 q + \beta_2 I^{1.5} q$$



Justification

Volterra series decomposition

$$T(t) = \sum_{j=1}^{\infty} T_j(t) = T_1(t) + T_2(t) + \cdots + T_j(t) + \cdots$$

$$T_j(t) = \int_0^{\infty} \cdots \int_0^{\infty} h_j(\tau_1, \cdots, \tau_j) \prod_{i=1}^j q(t - \tau_i) d\tau_i$$

\uparrow
 j^{th} order Volterra kernel

In practice the number of kernels can be limited to 2

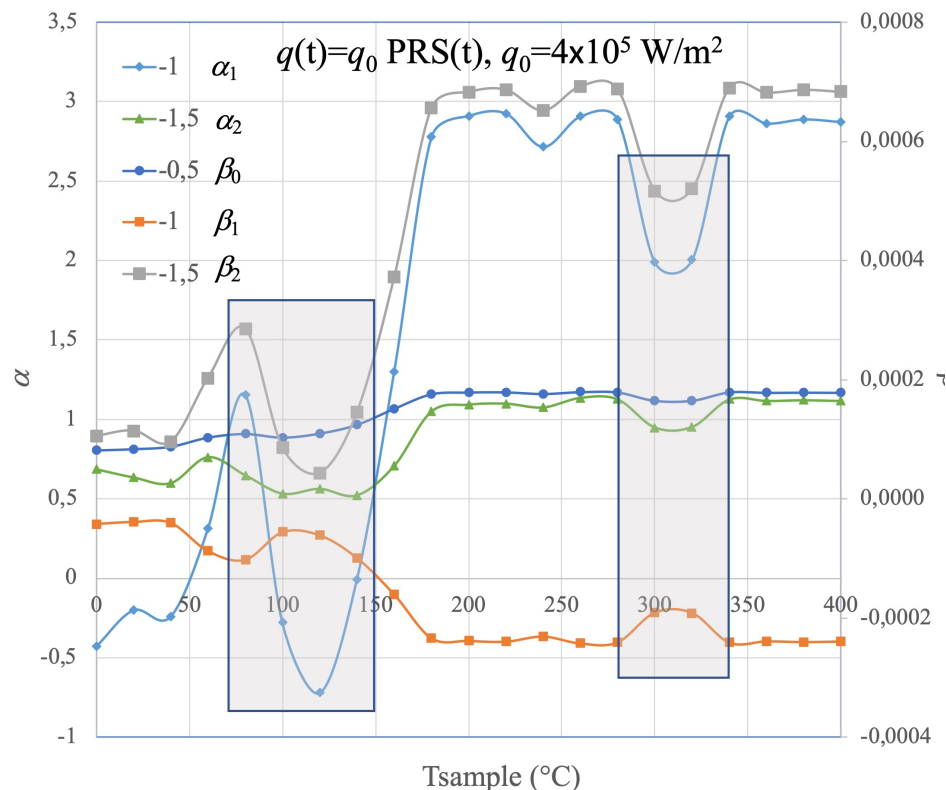
$$\begin{aligned} T(t) &= T_1(t) + T_2(t) = T_L(t) + T_{NL}(t) \\ &= \int_0^{\infty} h_1(\tau) q(t - \tau) d\tau + \int_0^{\infty} \int_0^{\infty} h_2(\tau_1, \tau_2) q(t - \tau_1) q(t - \tau_2) d\tau_1 d\tau_2 \end{aligned}$$

We propose to introduce a **generalized transfer function**:

$$T(t) = \int_0^{\infty} h_{NL}(\tau) q(t - \tau) d\tau$$

Justification

Since the non integer integral involves all the time history of the integrand function, it is well suited with the introduction of a generalized transfer function that accounts with non-linearities.



Increasing q_0 leads to involve larger non linearities and thus to limit the range of temperature investigated by the model

$$T + \alpha_1 I^1 q + \alpha_2 I^{1.5} q = \beta_0 I^{0.5} q + \beta_1 I^1 q + \beta_2 I^{1.5} q$$

