

Application d'une méthode de type 'meshless' à la résolution de problèmes de transferts radiatifs

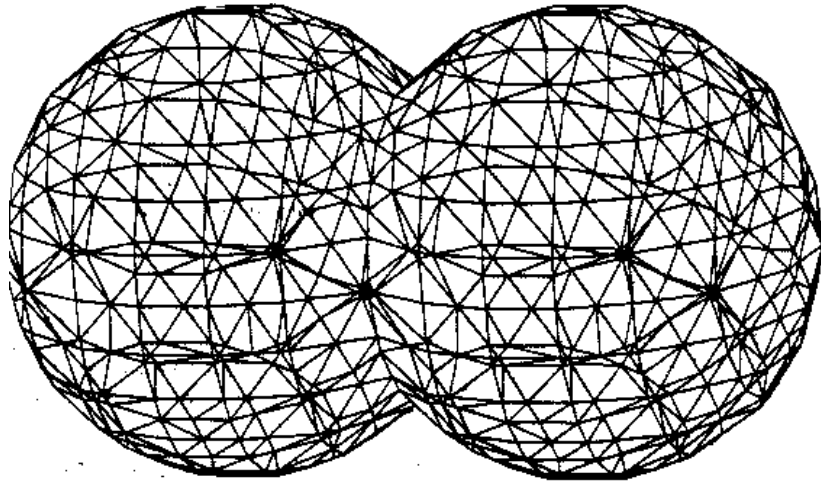
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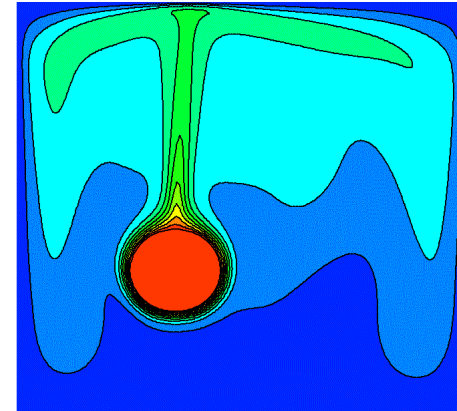
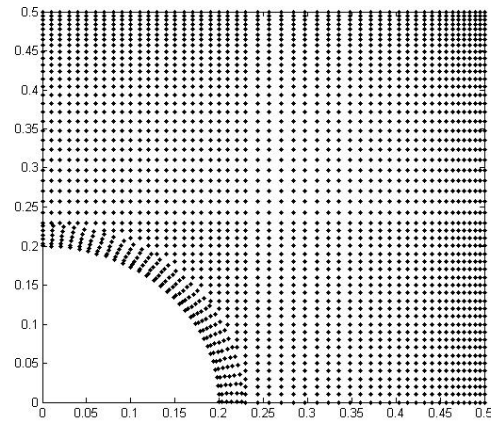
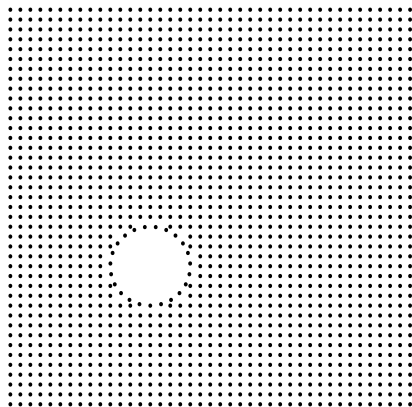
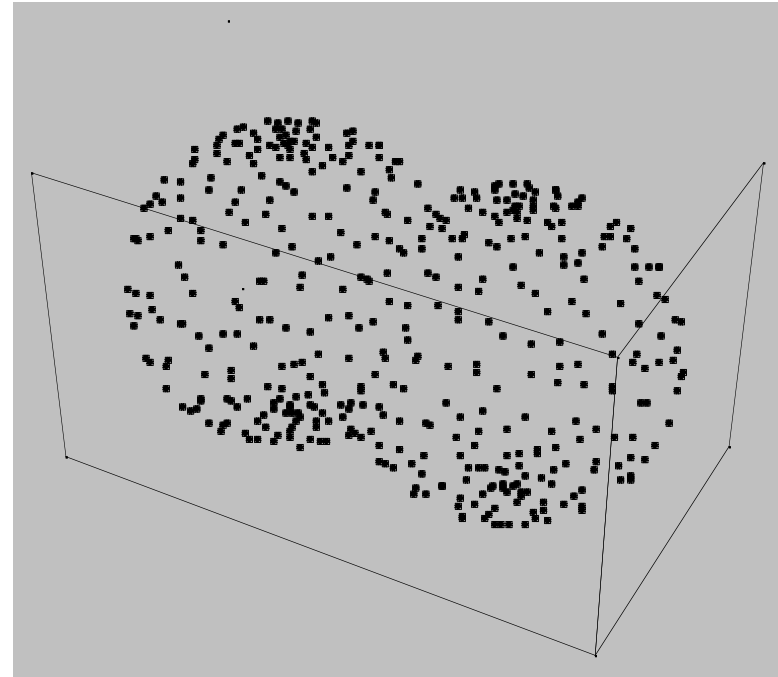


Discretisation

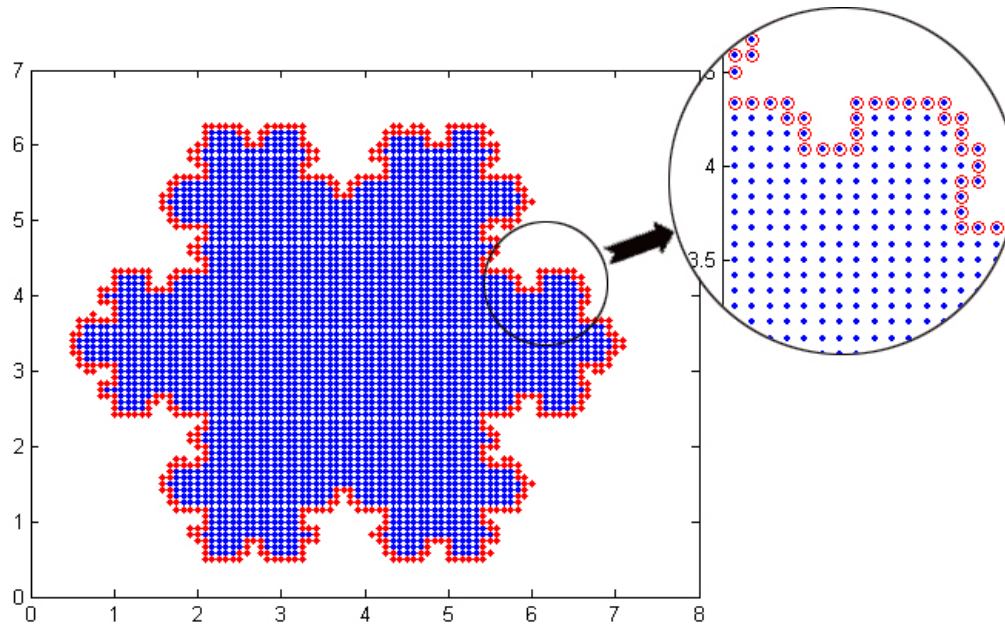
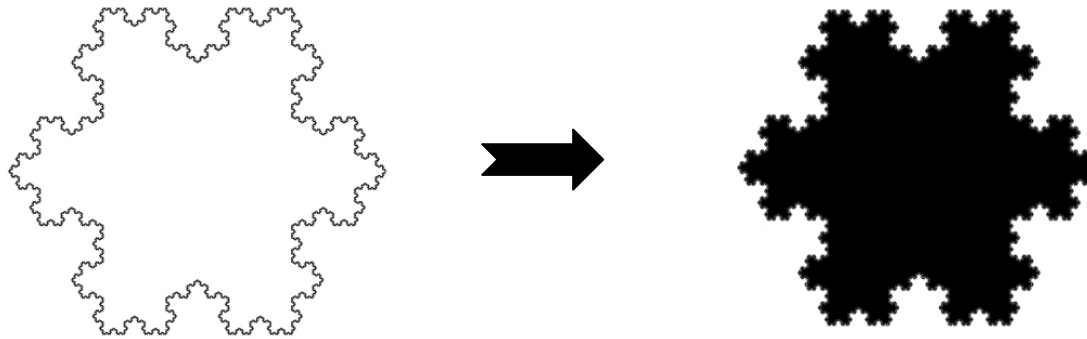
Avec maillage



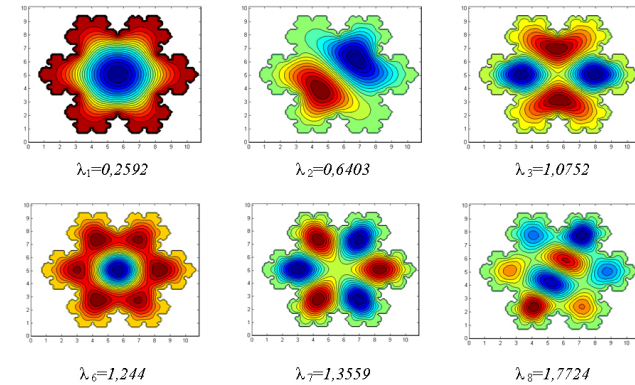
Sans maillage



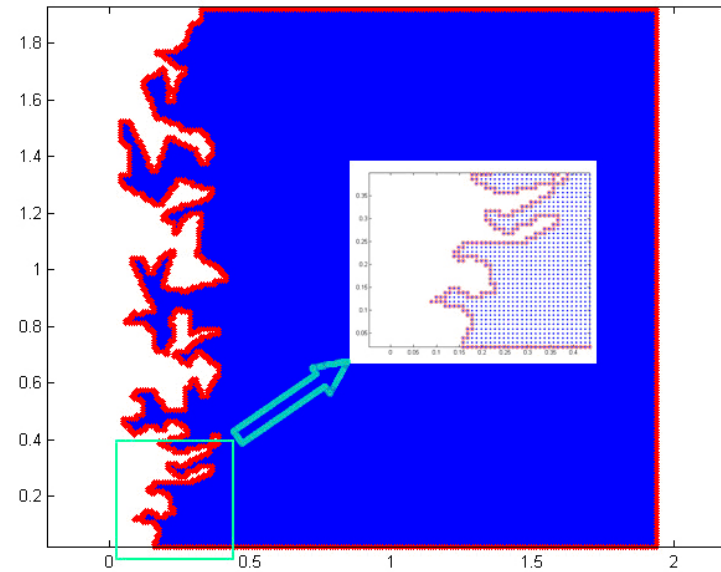
Construction du nuage de points: mailleurs, tir aléatoire, reconstruction de volumes..



valeurs et fonctions propres



Interface d'une surface catalytique



Approximation Diffuse

Approximation glissante à moindres carrés

$$\varphi_i^*(x_i, y_i) = \varphi + (x_i - x) \frac{\partial \varphi}{\partial x} + (y_i - y) \frac{\partial \varphi}{\partial y} + \frac{(x_i - x)^2}{2!} \frac{\partial^2 \varphi}{\partial x^2} + (x_i - x)(y_i - y) \frac{\partial^2 \varphi}{\partial x \partial y} + \frac{(y_i - y)^2}{2!} \frac{\partial^2 \varphi}{\partial y^2} + O(h^2)$$

$$\varphi_i^*(x_i, y_i) = \langle p(M_i, M) \rangle \cdot \langle \alpha_M \rangle^T$$

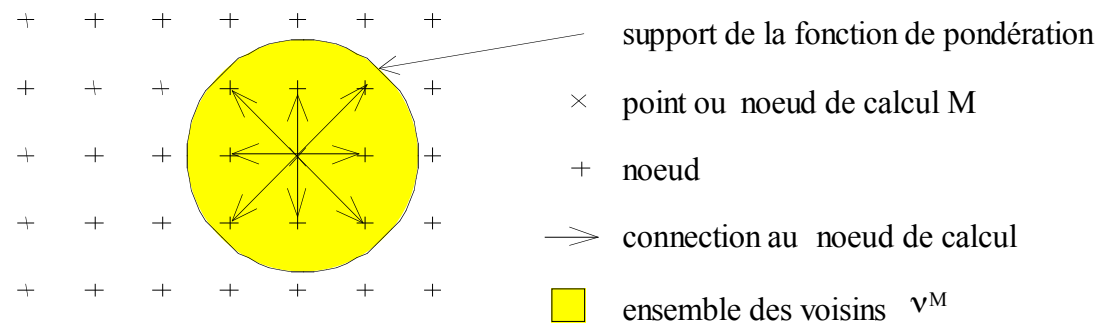
$$\langle p(M_i, M) \rangle = \left\langle 1, (x_i - x)(y_i - y), (x_i - x)^2, (x_i - x)(y_i - y), (y_i - y)^2 \right\rangle$$

$$\langle \alpha_M \rangle^T = \left\langle \varphi(x, y), \left(\frac{\partial \varphi}{\partial x} \right)^*, \left(\frac{\partial \varphi}{\partial y} \right)^*, \frac{1}{2!} \left(\frac{\partial^2 \varphi}{\partial x^2} \right)^*, \left(\frac{\partial^2 \varphi}{\partial x \partial y} \right)^*, \frac{1}{2!} \left(\frac{\partial^2 \varphi}{\partial y^2} \right)^* \right\rangle^T$$

Erreur Quadratique – Fonction De Pondération

$$I(\alpha_M) = \sum_{M_j \in \mathcal{V}^M} \left\{ \omega(M_j, M) \left[\varphi_j - \langle p(M_j, M) \rangle \cdot \langle \alpha_M \rangle^T \right]^2 \right\}$$

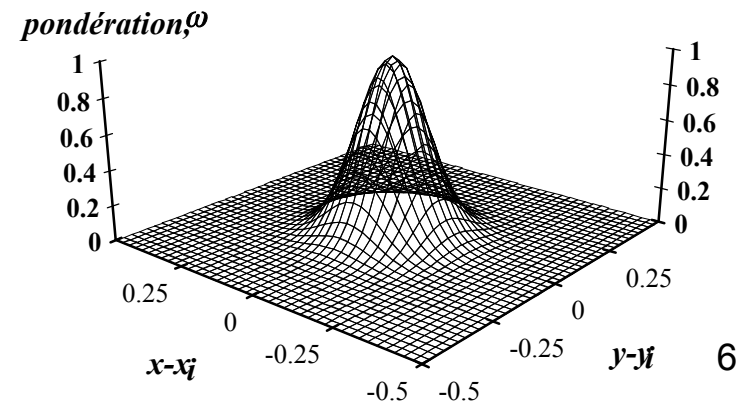
$\omega(M_j, M)$: fonction de pondération définie sur un support borné



Fonction de Gauss:

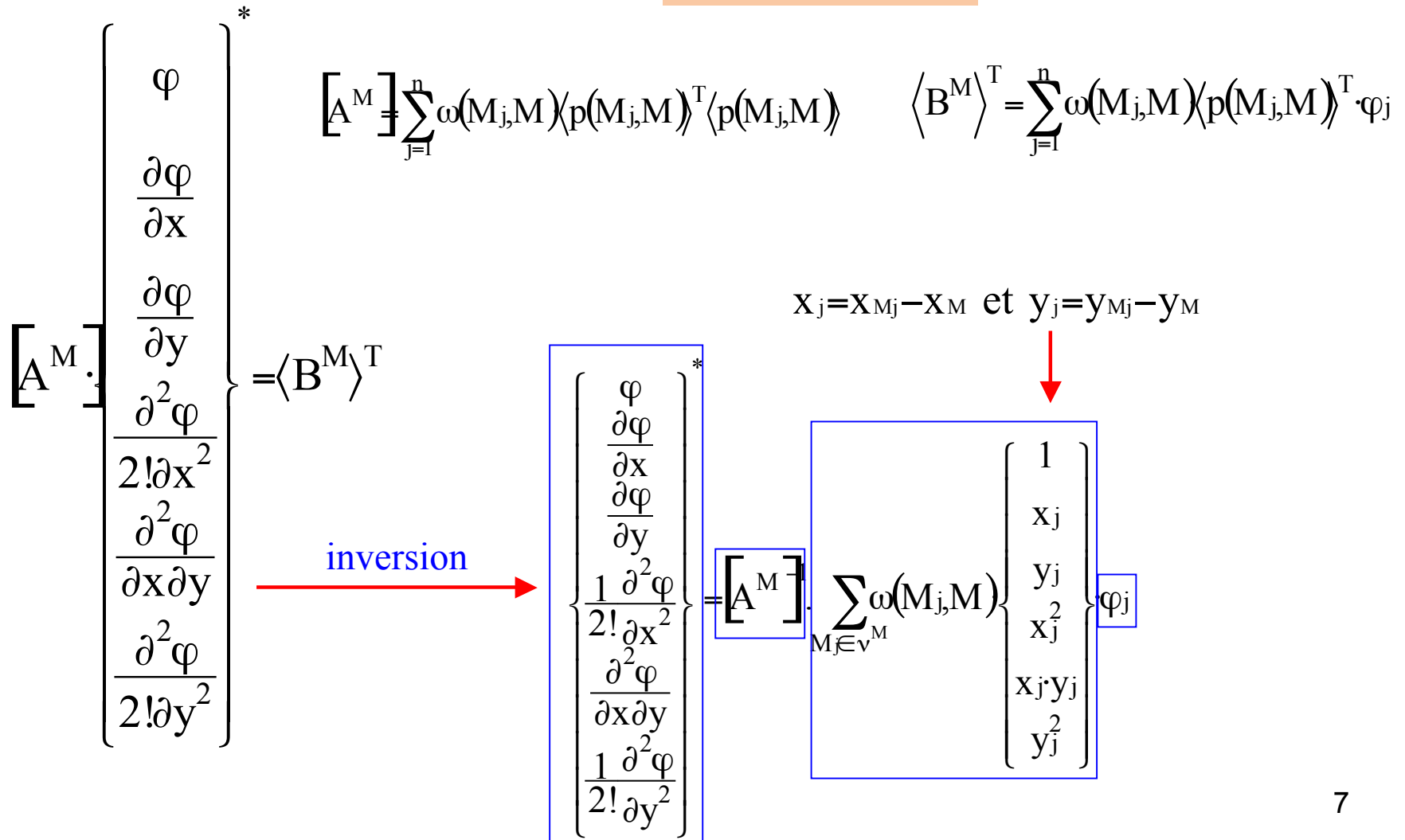
$$\omega(M_j, M) = \exp \left[-3 \ln(10) \cdot \left(\frac{r}{\sigma} \right)^2 \right]$$

$$\omega(M_j, M) = 0 \quad \text{si } r > \sigma$$



Expression Des Dérivées Partielles

Minimisation de l'erreur quadratique : $\frac{\partial I(\alpha_M)}{\partial \alpha_i} = 0 \quad i=0, \dots, 5$



Expression Des Dérivées Partielles

2D : Matrice 6x6

$$[A^M] = \sum_{M_j \in v^M} \omega(M_j, M) \begin{bmatrix} 1 & x_j & y_j & x_j^2 & x_j y_j & y_j^2 \\ x_j & x_j^2 & x_j y_j & x_j^3 & x_j^2 y_j & x_j y_j^2 \\ y_j & x_j y_j & y_j^2 & x_j^2 y_j & x_j y_j^2 & y_j^3 \\ x_j^2 & x_j^3 & x_j^2 y_j & x_j^4 & x_j^3 y_j & x_j^2 y_j^2 \\ x_j y_j & x_j^2 y_j & x_j y_j^2 & x_j^3 y_j & x_j^2 y_j^2 & x_j y_j^3 \\ y_j^2 & x_j y_j^2 & y_j^3 & x_j^2 y_j^2 & x_j y_j^3 & y_j^4 \end{bmatrix}$$

$\langle a_i \rangle$: i^{ème} ligne de la matrice $[A^M]^{-1}$

$$\langle p_j \rangle = \langle p(M_j, M) \rangle$$

$$\frac{\partial \varphi}{\partial y} = \sum_{M_j \in v^M} \omega(M_j, M) \langle a_3 \rangle \langle p_j \rangle^T \varphi_j$$

$$\frac{\partial^2 \varphi}{\partial x^2} = 2! \sum_{M_j \in v^M} \omega(M_j, M) \langle a_4 \rangle \langle p_j \rangle^T \varphi_j$$

3D : Matrice 10x10

$$[A^M] = \sum_{M_j \in \mathcal{V}^M} \omega(M_j, M)$$

$$\begin{bmatrix} 1x_j & y_j & x_j^2 & x_j y_j & y_j^2 & z_j & x_j z_j & y_j z_j & z_j^2 \\ *x_j^2 & x_j y_j & x_j^3 & x_j^2 y_j & x_j y_j^2 & x_j z_j & x_j^2 z_j & x_j y_j z_j & x_j z_j^2 \\ ** & y_j^2 & x_j^2 y_j & x_j y_j^2 & y_j^3 & y_j z_j & x_j y_j z_j & y_j^2 z_j & y_j z_j^2 \\ ** & * & x_j^4 & x_j^3 y_j & x_j^2 y_j^2 & x_j^2 z_j & x_j^3 z_j & x_j^2 y_j z_j & x_j^2 z_j^2 \\ ** & * & * & x_j^2 y_j^2 & x_j y_j^3 & x_j y_j z_j & x_j^2 y_j z_j & x_j y_j^2 z_j & x_j y_j z_j^2 \\ ** & * & * & * & y_j^4 & y_j^4 z_j & x_j y_j^2 z_j & y_j^3 z_j & y_j^2 z_j^2 \\ ** & * & * & * & * & z_j^2 & x_j z_j^3 & y_j z_j^3 & z_j^4 \\ ** & * & * & * & * & * & x_j^2 z_j^2 & x_j y_j z_j^2 & x_j z_j^3 \\ ** & * & * & * & * & * & * & y_j^2 z_j^2 & y_j z_j^3 \\ ** & * & * & * & * & * & * & * & z_j^4 \end{bmatrix}$$

$\langle a_i \rangle$: i^{ème} ligne de la matrice $[A^M]^{-1}$

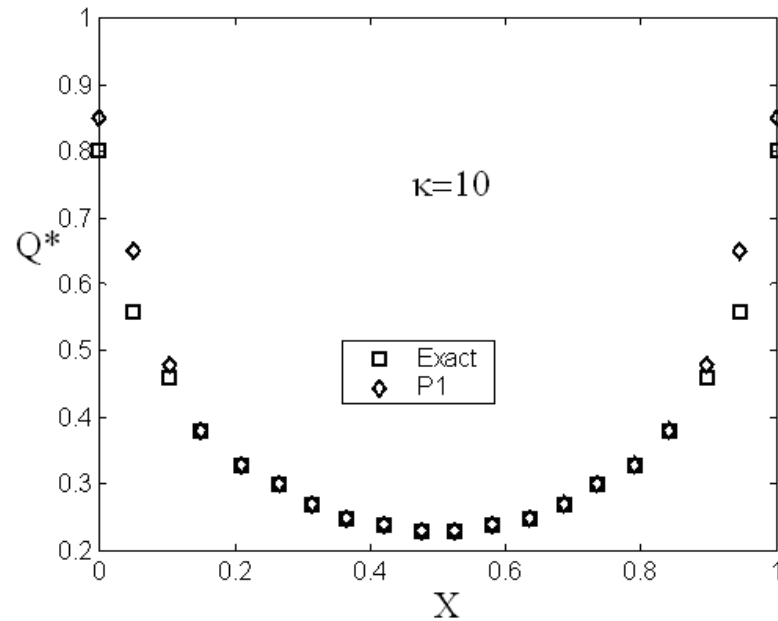
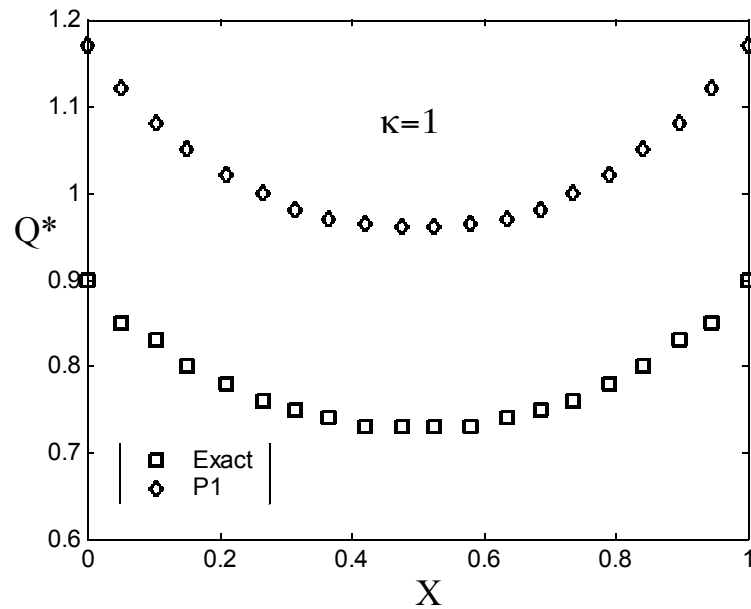
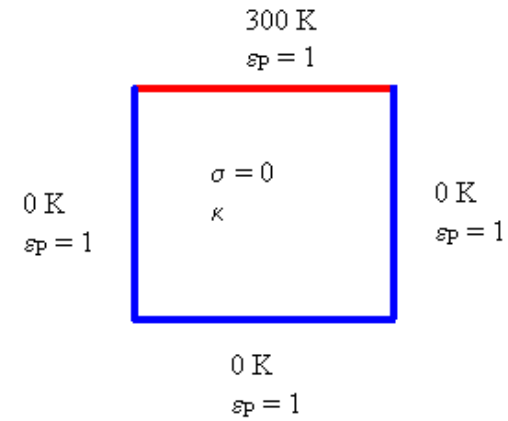
$$\langle p_j \rangle = \langle p(M_j, M) \rangle$$

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Méthode P1

Equilibre Radiatif dans une cavité Carrée



Méthode S_N

ETR (Variables primaires)

$$\frac{dI(\Omega_i)}{ds} = -\beta I(\Omega_i) + \kappa I_b + \frac{\sigma}{4\pi} \sum_{j=1}^J I(\Omega'_j) \Phi(\Omega'_j, \Omega_i) W(\Omega'_j)$$

ETR (Variables Secondaires: Flux pairs)

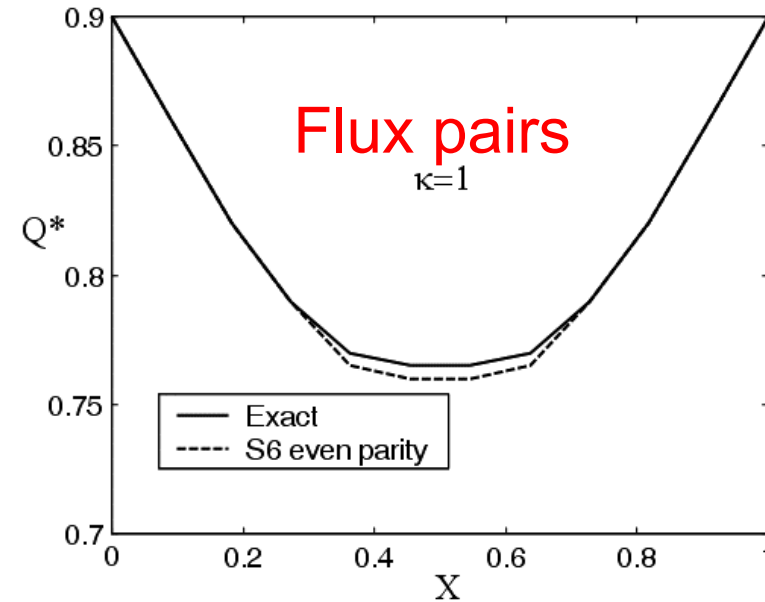
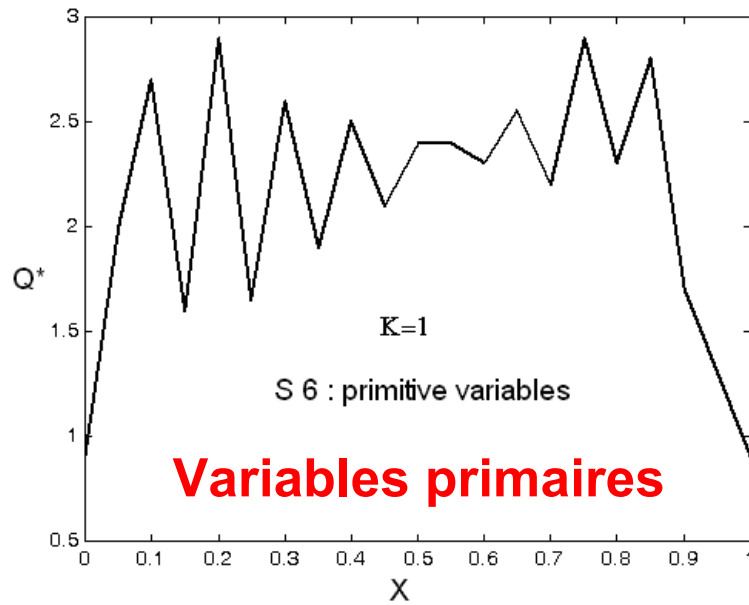
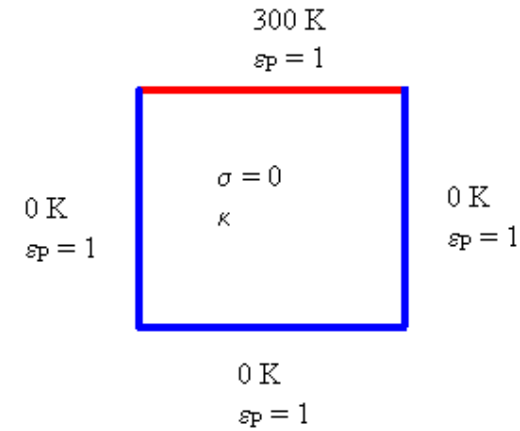
$$F(\Omega) = I^+(\Omega) + I^-(\Omega) \quad G(\Omega) = I^+(\Omega) - I^-(\Omega)$$

$$\left\{ \begin{array}{l} \frac{1}{\beta} \frac{d^2 F_i}{ds^2} - \beta F_i + \kappa I_b + \frac{\sigma}{4\pi} \sum_{j=1}^{J/2} (A_{ij} F_j + B_{ij} G_j) = 0 \\ \frac{\partial F_i(P, \vec{\Omega})}{\partial s_m} + \beta G_i(P, \vec{\Omega}) = 0 \end{array} \right.$$

Remarque: Autre formulation du second ordre possible

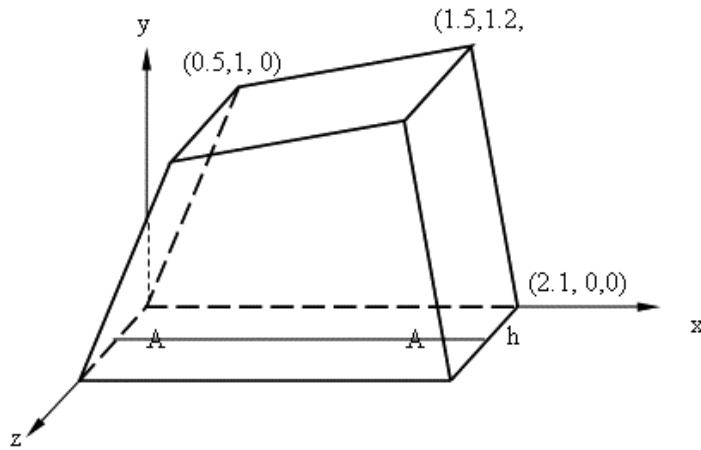
Méthode SN

Equilibre Radiatif dans une cavité carrée



Flux pairs \longrightarrow Equilibre radiatif et problèmes couplés

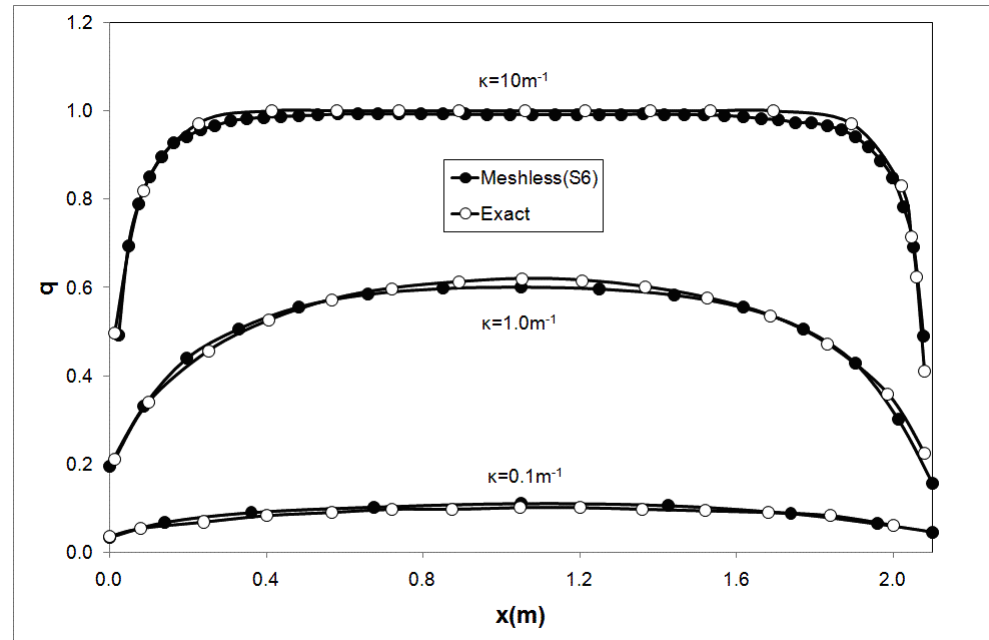
Equilibre radiatif dans une enceinte hexahédrique



$h=1\text{ m}$

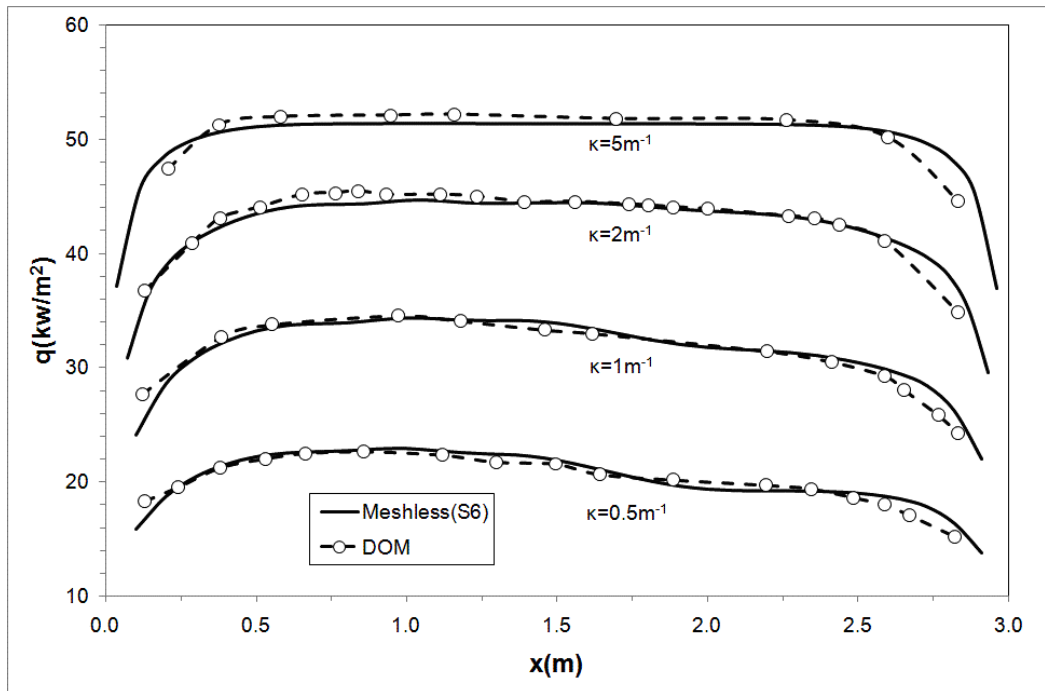
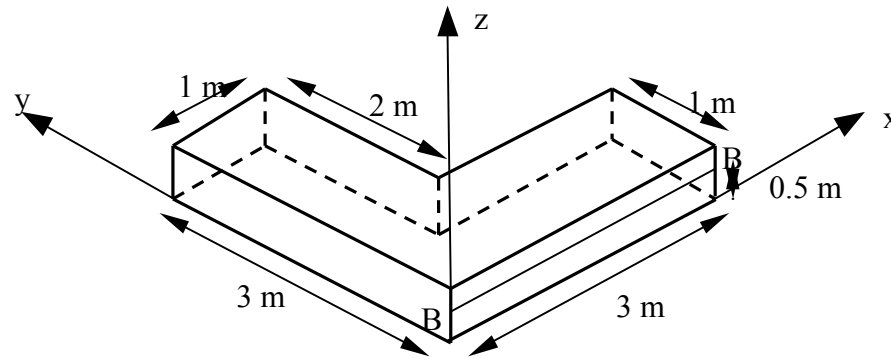
Milieu absorbant, émettant à T_m
Parois noires et froides à T_p

[Baek et al] NHT (Part B), 1998
Nonorthogonal finite volume



Flux sur la ligne AA

Equilibre radiatif dans une enceinte en forme de "L"



Milieu absorbant, émettant à 1000K

Parois noires à 500K

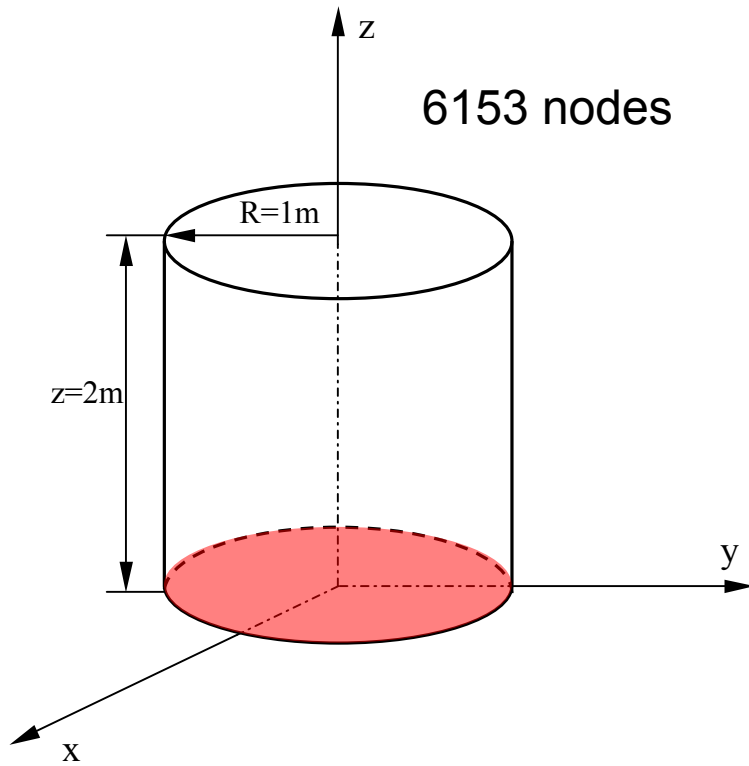
15105 noeuds pour $\kappa=2\text{ m}^{-1}$ et 5 m^{-1}

Flux sur la ligne BB

Journal Heat Transfer, 1996

Couplage Conduction-Rayonnement

Milieu semi-transparent cylindrique

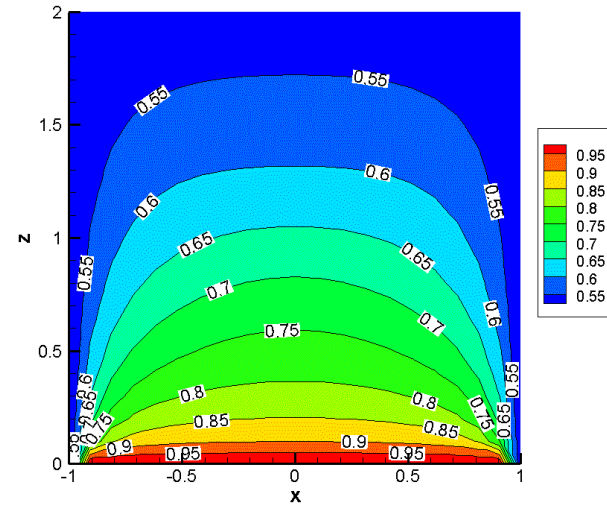


Base à T_c , les autres parois à T_f avec $T_f/T_c=0.5$

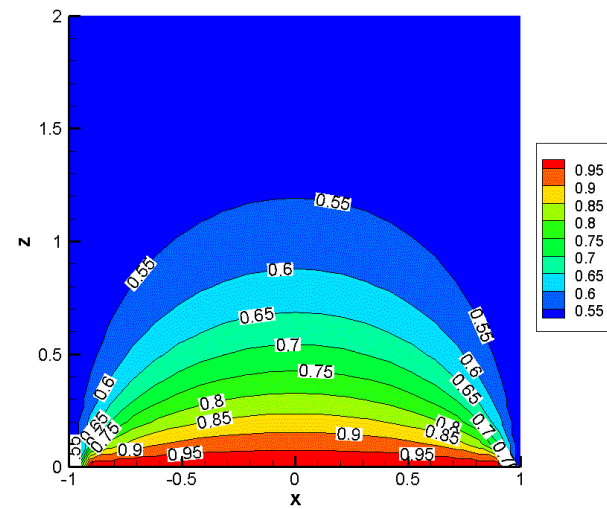
Effet du nombre de Planck

$$Pr = (\lambda\beta)/(4\sigma T_{ref}^3)$$

Isothermes dans le plan $y=0$

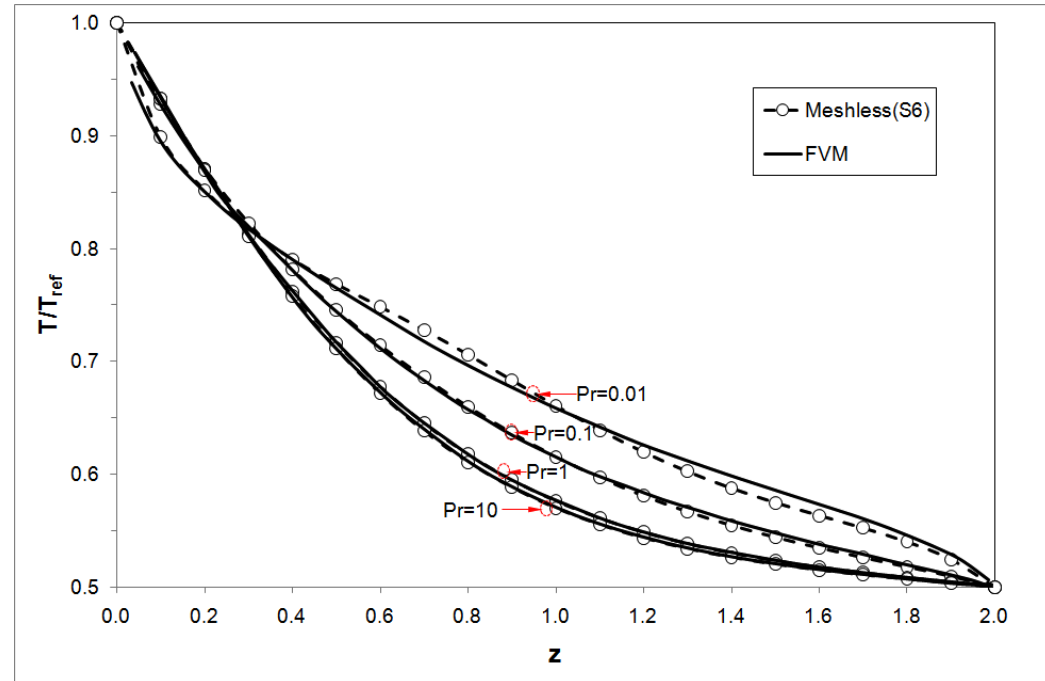
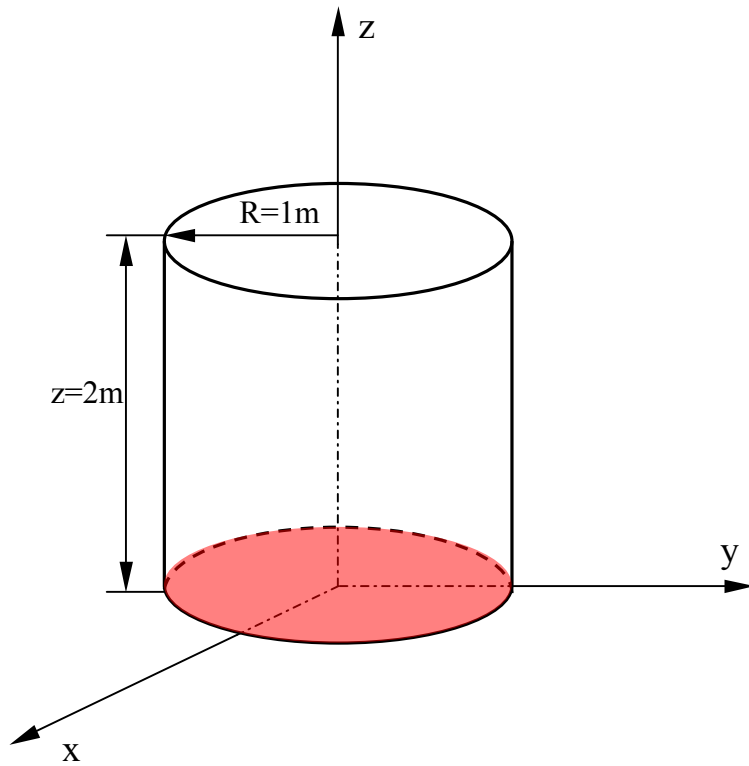


$Pr = 0.01$



$Pr = 1$

Milieu semi-transparent cylindrique



temperature sur l'axe z

Effet du paramètre conducto-radiatif

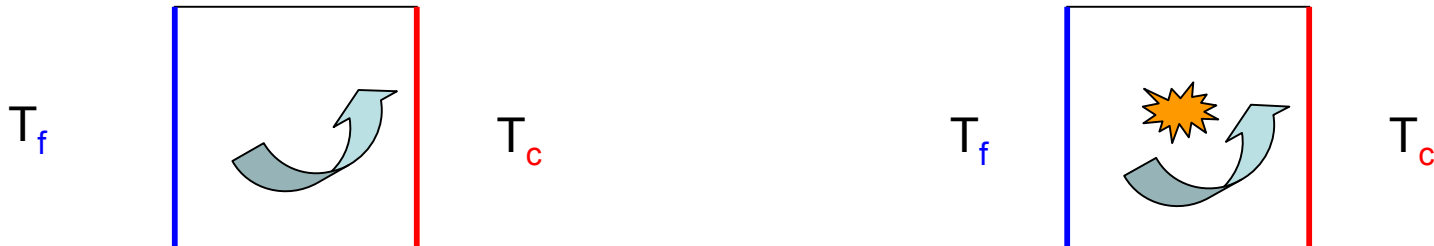
$$Pr = (\lambda\beta) / (4\sigma T_{\text{ref}}^3)$$

Couplage Convection-Rayonnement

Algorithme de Projection (P-V)
ou
Formulation Vitesse-Vorticité

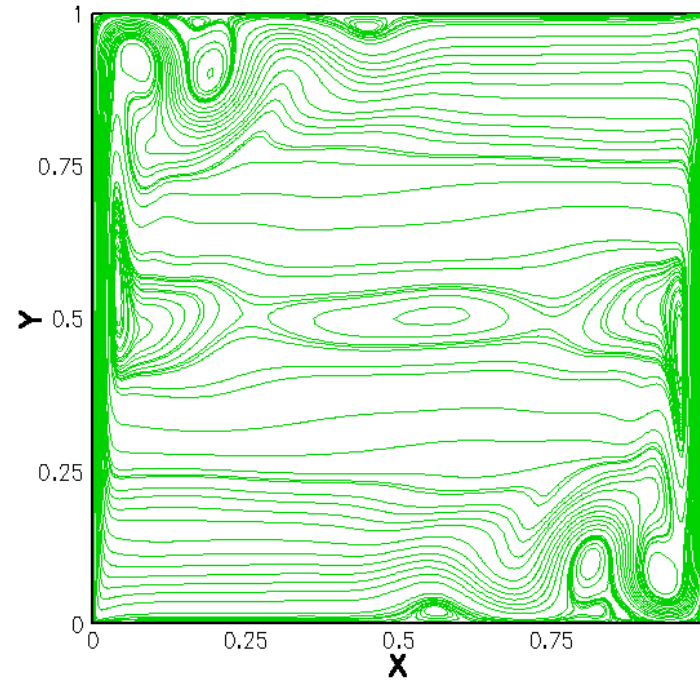
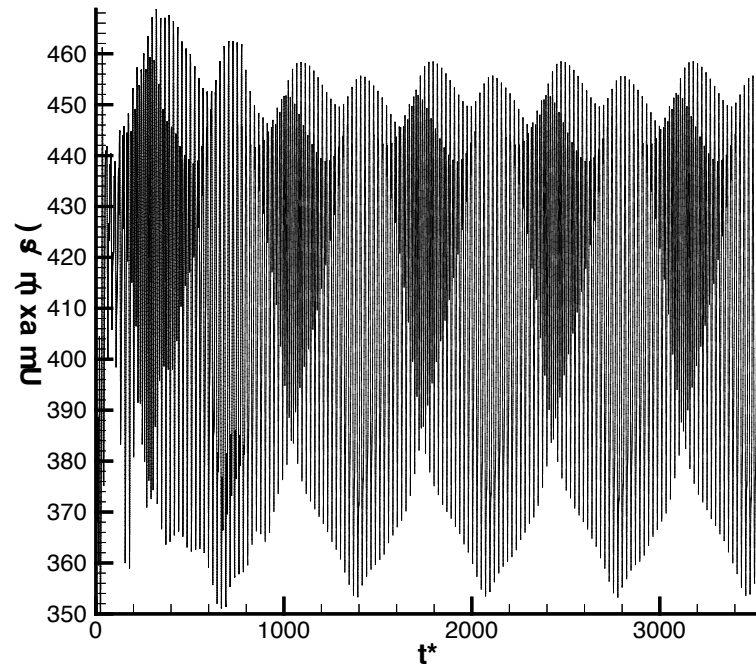
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Méthode des Flux pairs



Cavité différentiellement chauffée à $Ra=2 \cdot 10^8$

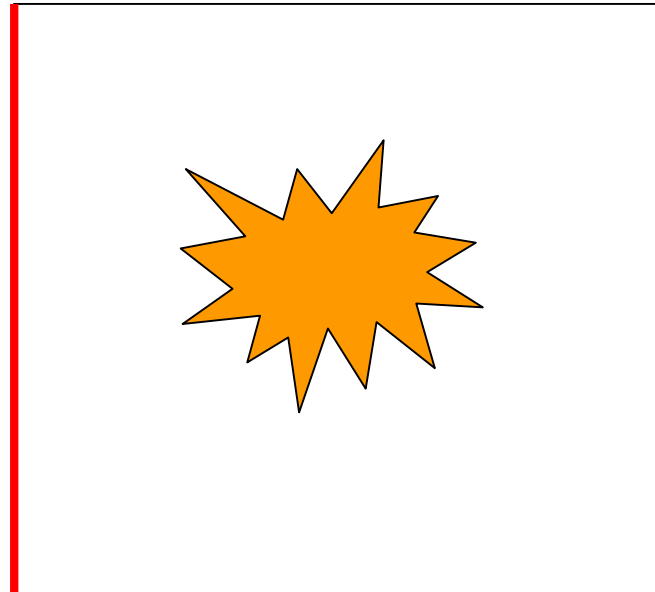
Évolution temporelle de la vitesse



Bifurcation à un régime pseudo périodique

Couplage Convection-Rayonnement

Cavité avec generation interne de puissance



$$Ra = 10^6$$

$$Ra^I = 4 \cdot 10^4$$

$$Ra^I = \frac{g\beta\dot{q}L^5}{\nu_0\alpha_0k}$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \nabla^2 T - \frac{1}{Pl} \cdot \frac{1}{\Delta T} \cdot \frac{\text{div} \vec{q}_r}{4\sigma T_{ref}^3} + \frac{Ra^I}{Ra}$$

Equations de Poisson pour la vitesse

$$\nabla^2 u = -\frac{\partial \xi}{\partial y} + \frac{\partial \eta}{\partial z}$$

$$\nabla^2 v = -\frac{\partial \xi}{\partial z} + \frac{\partial \zeta}{\partial x}$$

$$\nabla^2 w = -\frac{\partial \eta}{\partial x} + \frac{\partial \xi}{\partial y}$$

Equations de transport de la vorticit 

$$\frac{\partial \xi}{\partial t} + u \frac{\partial \xi}{\partial x} + v \frac{\partial \xi}{\partial y} + w \frac{\partial \xi}{\partial z} = \xi \frac{\partial u}{\partial x} + \eta \frac{\partial u}{\partial y} + \zeta \frac{\partial u}{\partial z} + Pr \nabla^2 \xi + Ra Pr \cos \phi \left(\frac{\partial T}{\partial y} \right)$$

$$\frac{\partial \eta}{\partial t} + u \frac{\partial \eta}{\partial x} + v \frac{\partial \eta}{\partial y} + w \frac{\partial \eta}{\partial z} = \xi \frac{\partial v}{\partial x} + \eta \frac{\partial v}{\partial y} + \zeta \frac{\partial v}{\partial z} + Pr \nabla^2 \eta + Ra Pr \left(\sin \phi \frac{\partial T}{\partial z} - \cos \phi \frac{\partial T}{\partial x} \right)$$

$$\frac{\partial \zeta}{\partial t} + u \frac{\partial \zeta}{\partial x} + v \frac{\partial \zeta}{\partial y} + w \frac{\partial \zeta}{\partial z} = \xi \frac{\partial w}{\partial x} + \eta \frac{\partial w}{\partial y} + \zeta \frac{\partial w}{\partial z} + Pr \nabla^2 \zeta - Ra Pr \sin \phi \left(\frac{\partial T}{\partial y} \right)$$

Equation de l'  nergie

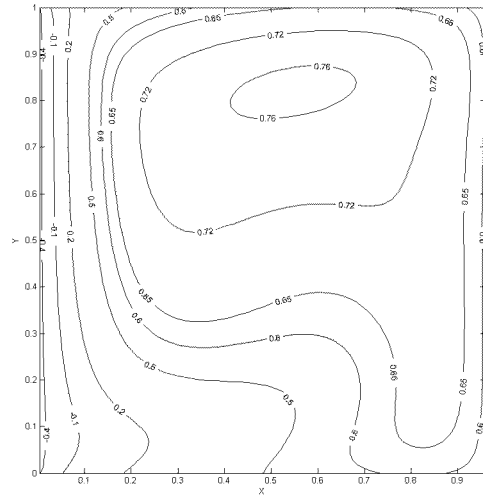
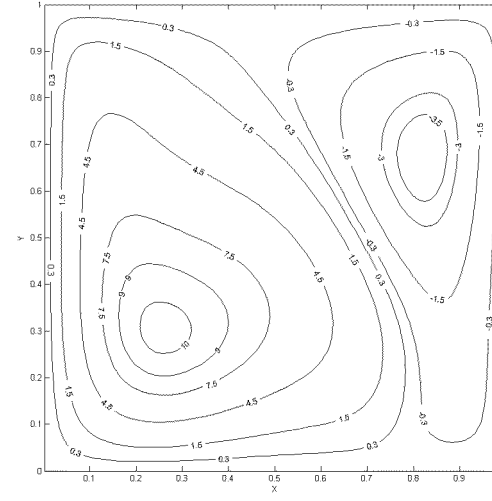
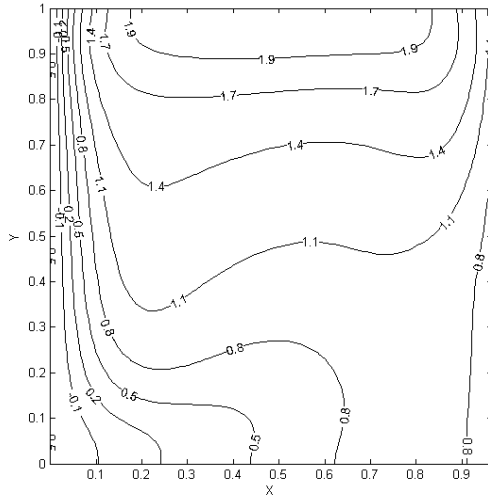
$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \nabla^2 T - \frac{1}{Pl} \cdot \frac{1}{\Delta T} \cdot \frac{\text{div} \vec{q}_r}{4\sigma T_{ref}^3} + \frac{Ra^I}{Ra}$$

Planck $Pl = \frac{k / L}{4\sigma T_{ref}^3}$

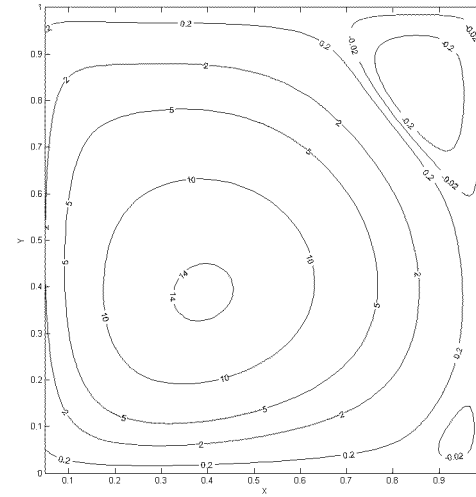
$Ra^I = \frac{g\beta\dot{q}L^5}{v_0\alpha_0k}$

Rayleigh $Ra = \frac{g\beta\Delta TL^3}{v_0\alpha_0}$

Convection



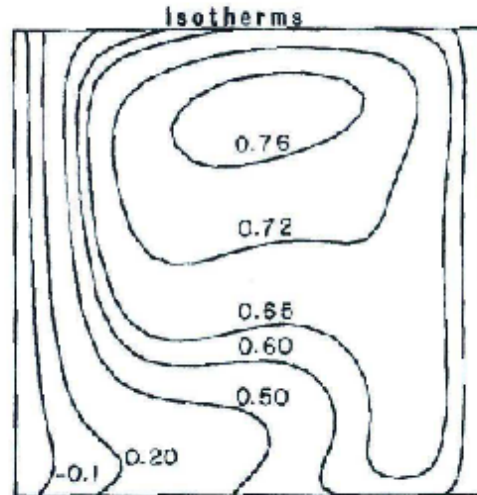
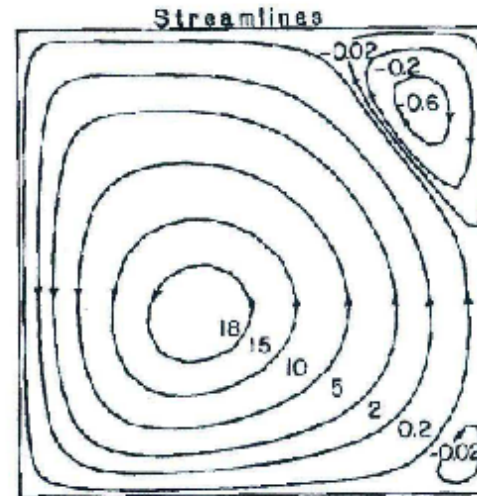
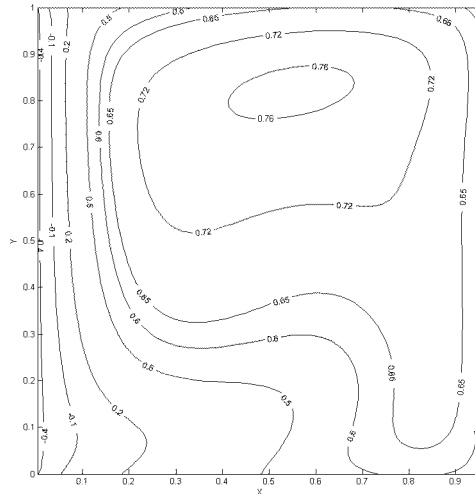
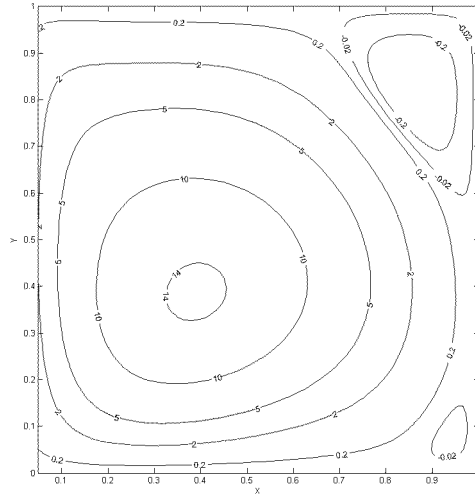
$\tau = 1.0$



Convection+Rayonnement

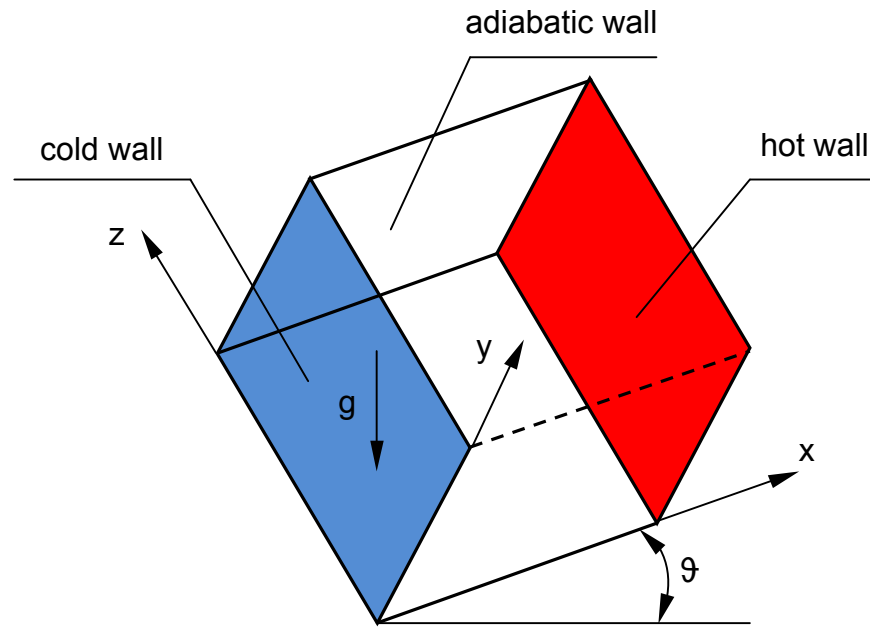
Cavité avec generation interne de puissance

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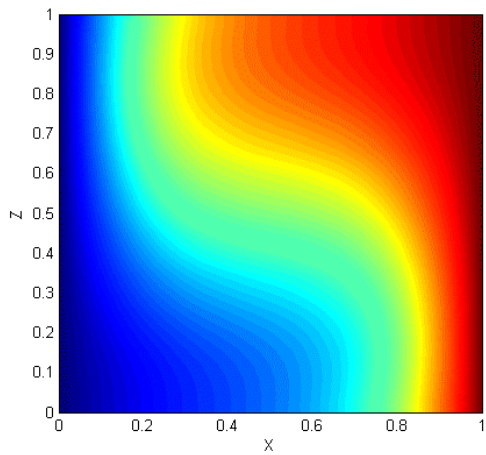


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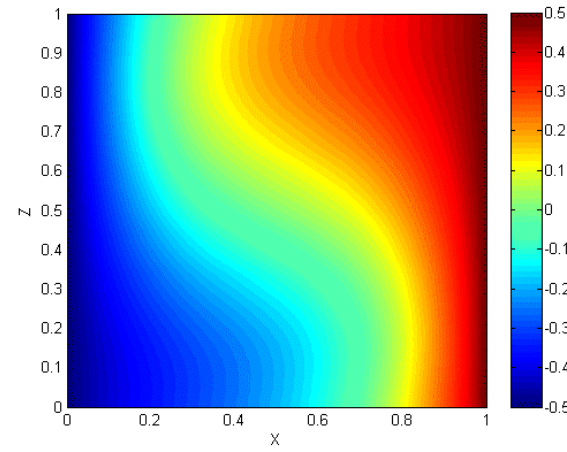
Cavité 3D différentiellement chauffée



Colomer et al,
IJHMT,2004



k=30



k=10

Merci