

Interest of the multi-scale characterization of a heterogeneous material for the prediction of its thermal radiative behaviour

B. Rousseau*,

H. Gomart, D. De Sousa Meneses, P. Echegut



J.-F. Thovert



(ex CRMHT) Conditions Extrêmes et Matériaux : Haute Température et Irradiation
1D, avenue de la Recherche Scientifique, 45071, Orléans, Cedex 02

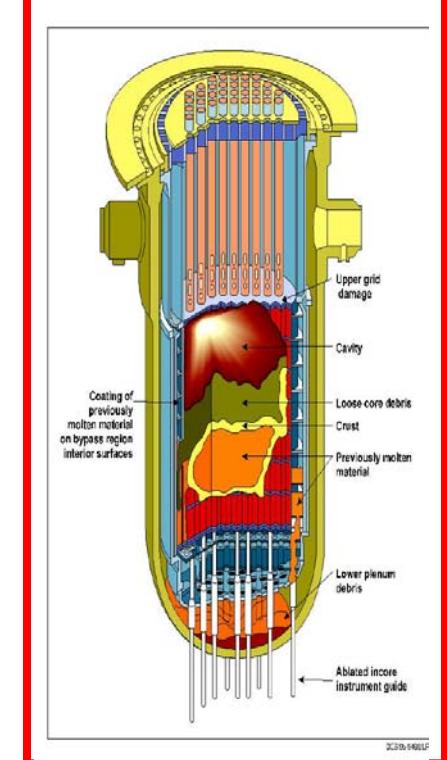
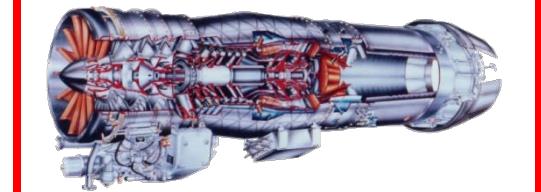
500 K

1000 K

1500 K

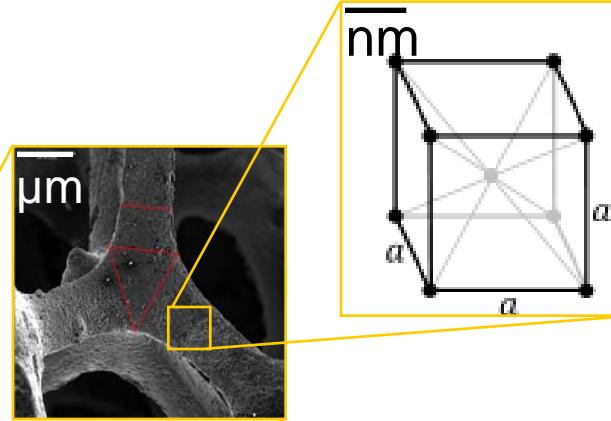
2000 K

2500 K

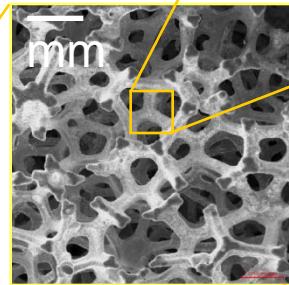


S. Gauthier, Ph. D, CETHIL, 2008

Heat Tranfer



Ex : Metallic Foam

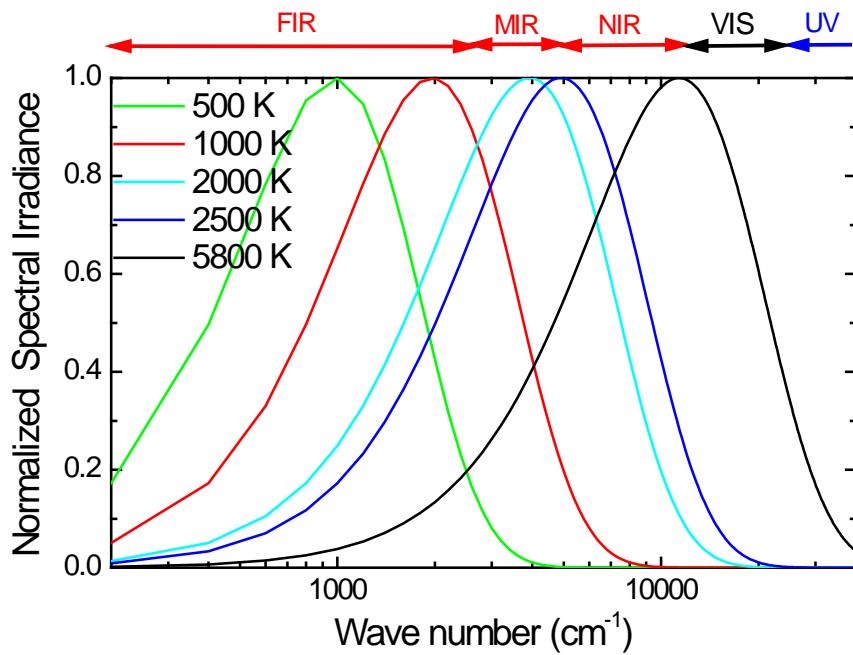
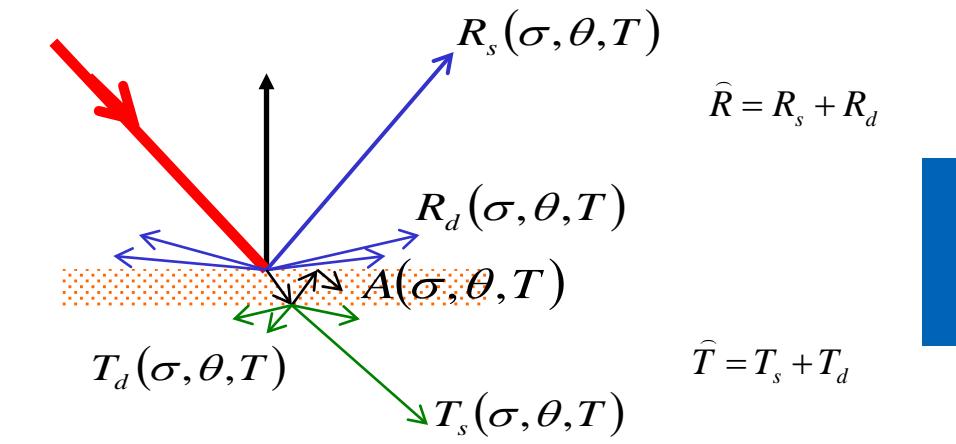


Thermal Radiative Properties

Microstructure + Chemistry

Material Characterization

DIRECT RADIATIVE PROPERTIES



Kirchhoff's law:

Energy balance

- $A(\sigma, \theta, T) = 1 - \hat{R}(\sigma, \theta, T) - \hat{T}(\sigma, \theta, T)$

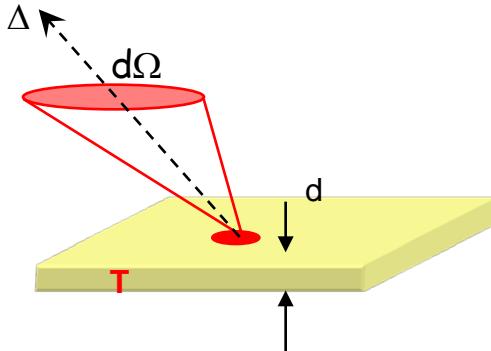
Local Thermodynamic Equilibrium

- $E(\sigma, \theta, T) = A(\sigma, \theta, T)$

$$E(\sigma, \theta, T) = \frac{L(\sigma, \theta, T)}{L^0(\sigma, T)}$$

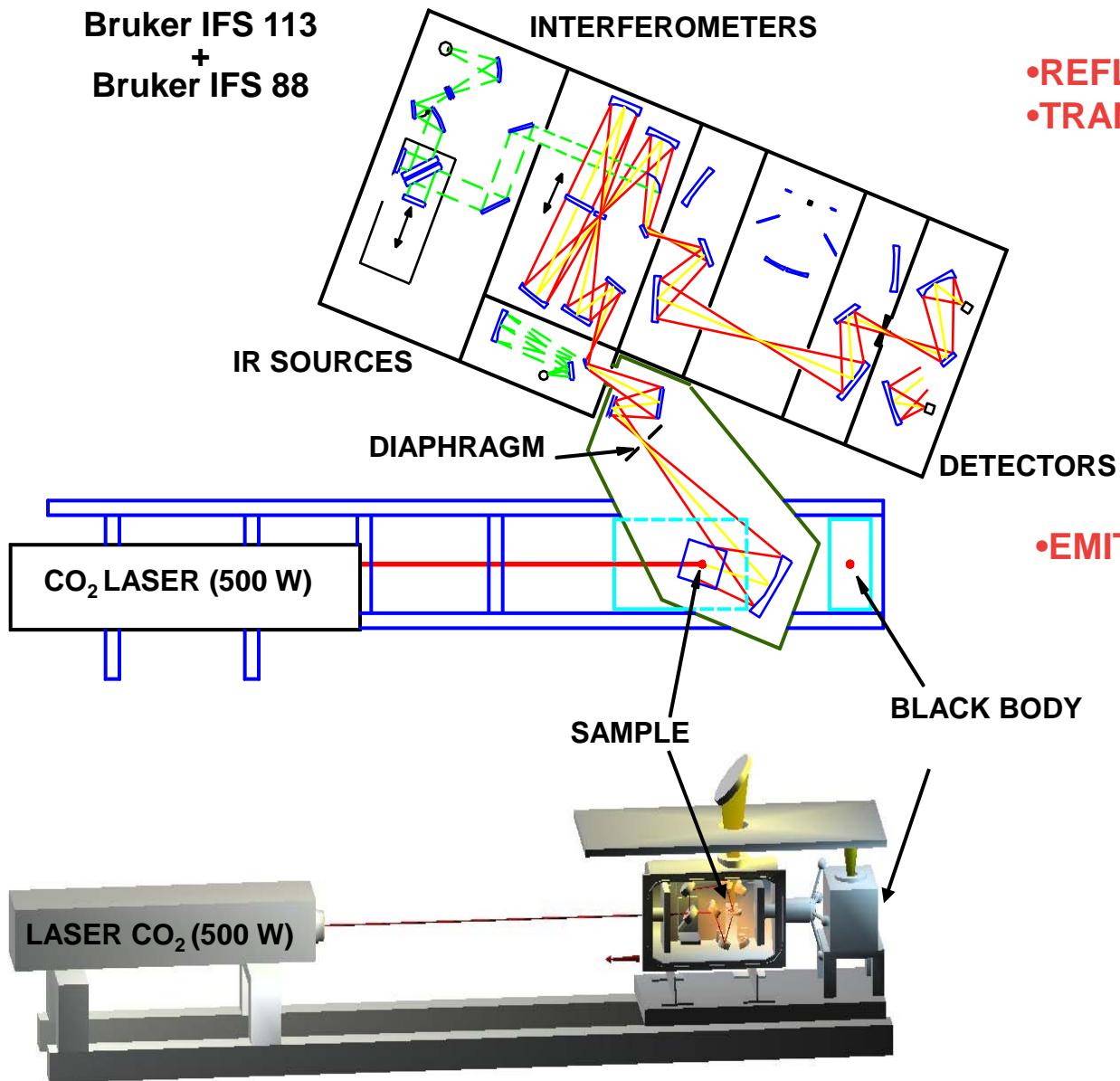
- $L^0(\sigma, T) = \frac{C_1 \sigma^3}{e^{\frac{C_2 \sigma}{T}} - 1}$ Planck's law

- $L(\sigma, \theta, T)$



EXPERIMENTAL SET UP

Bruker IFS 113
+
Bruker IFS 88

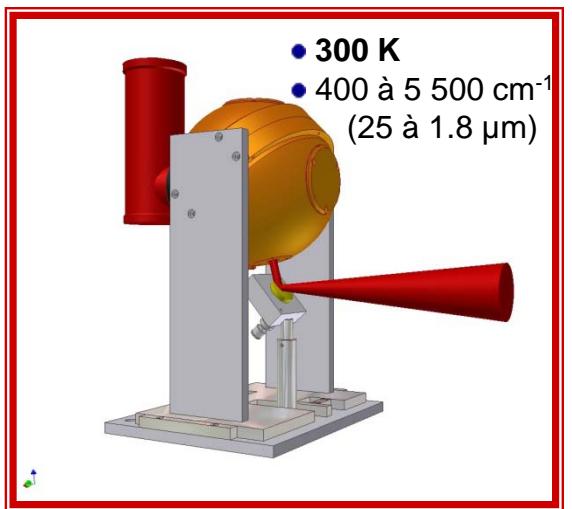


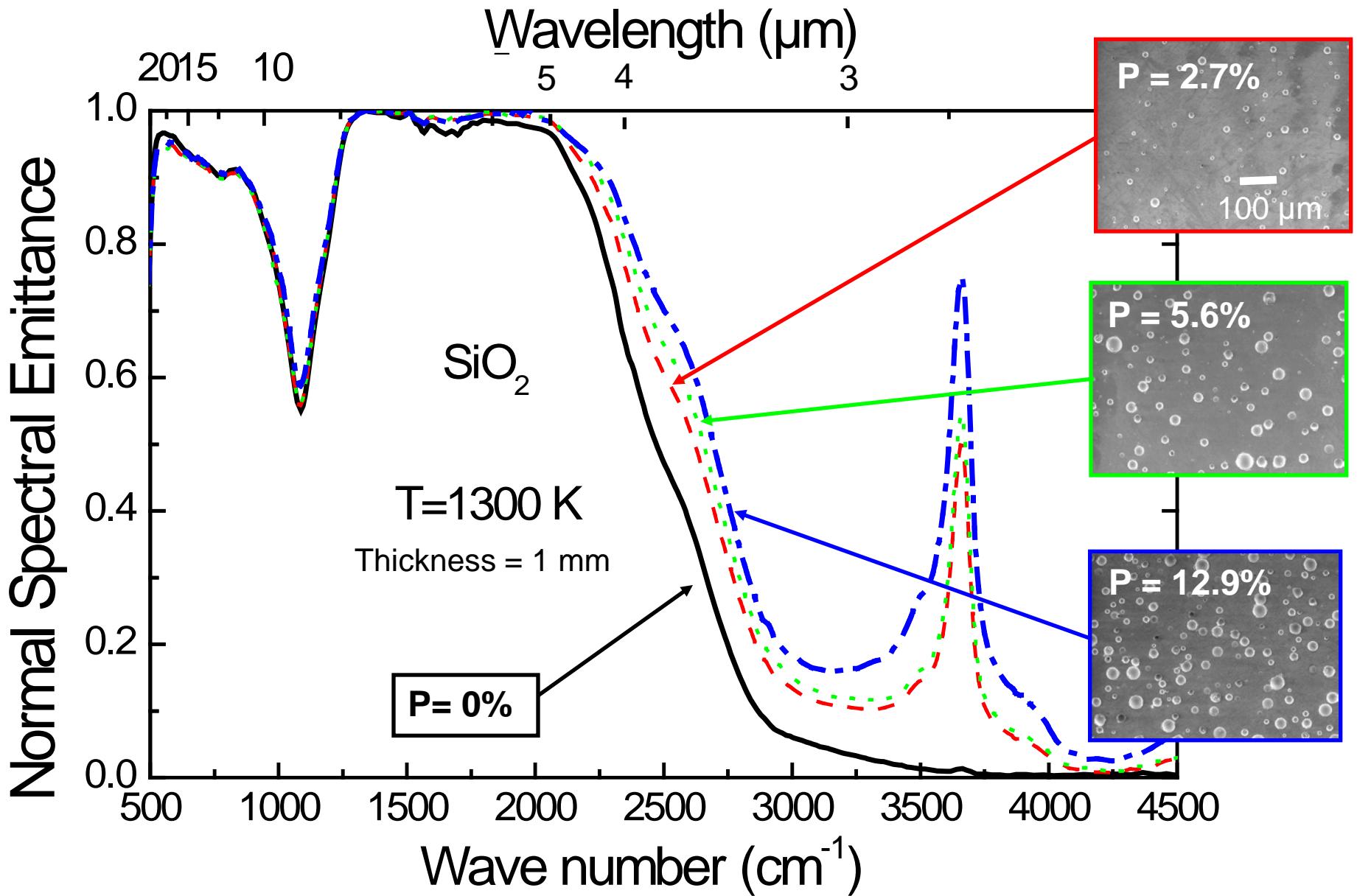
- REFLECTANCE
- TRANSMITTANCE

- 4 - 1200 K
- 10 - 40 000 cm⁻¹
(1 000 - 0.25 μm)

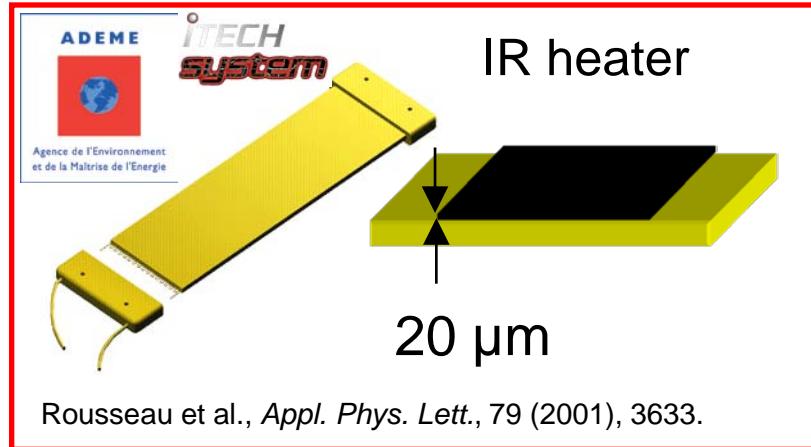
- EMITTANCE

- 500 - 2 500 K
- 10 - 14 500 cm⁻¹
(1 000 - 0.7 μm)



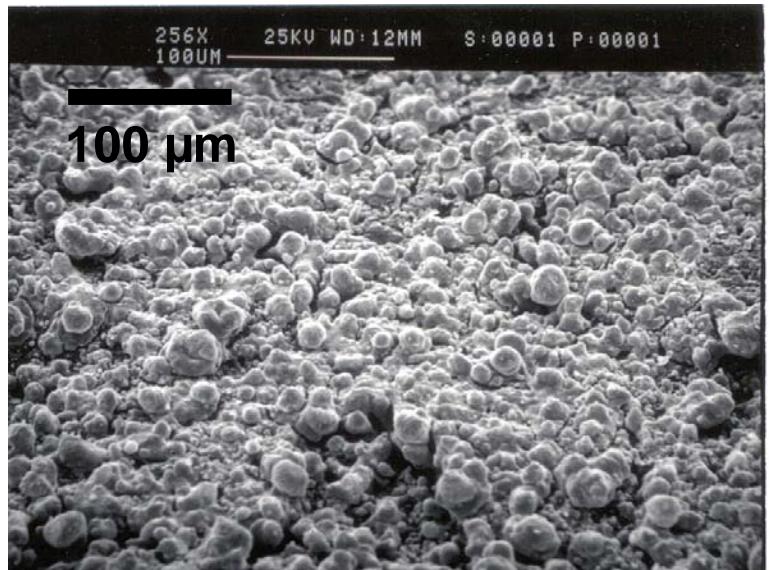
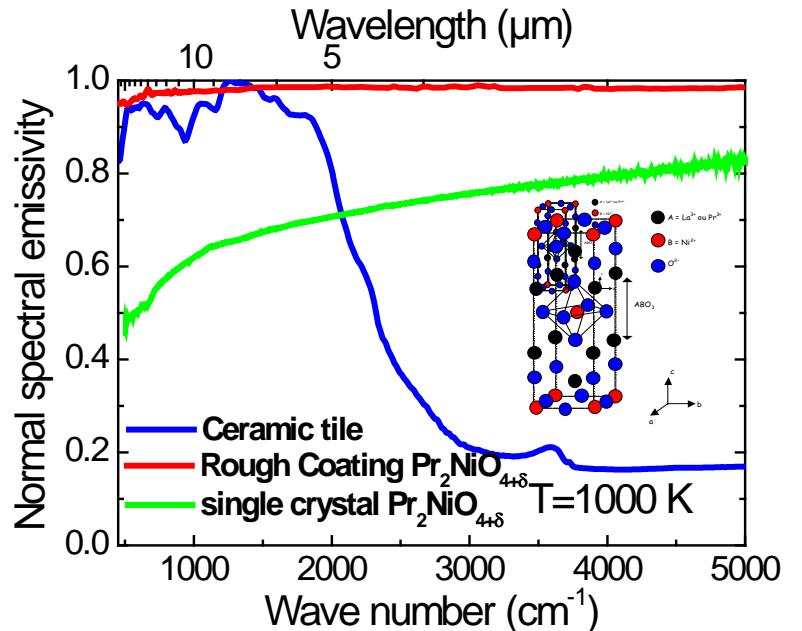


BLACK BODY COATING

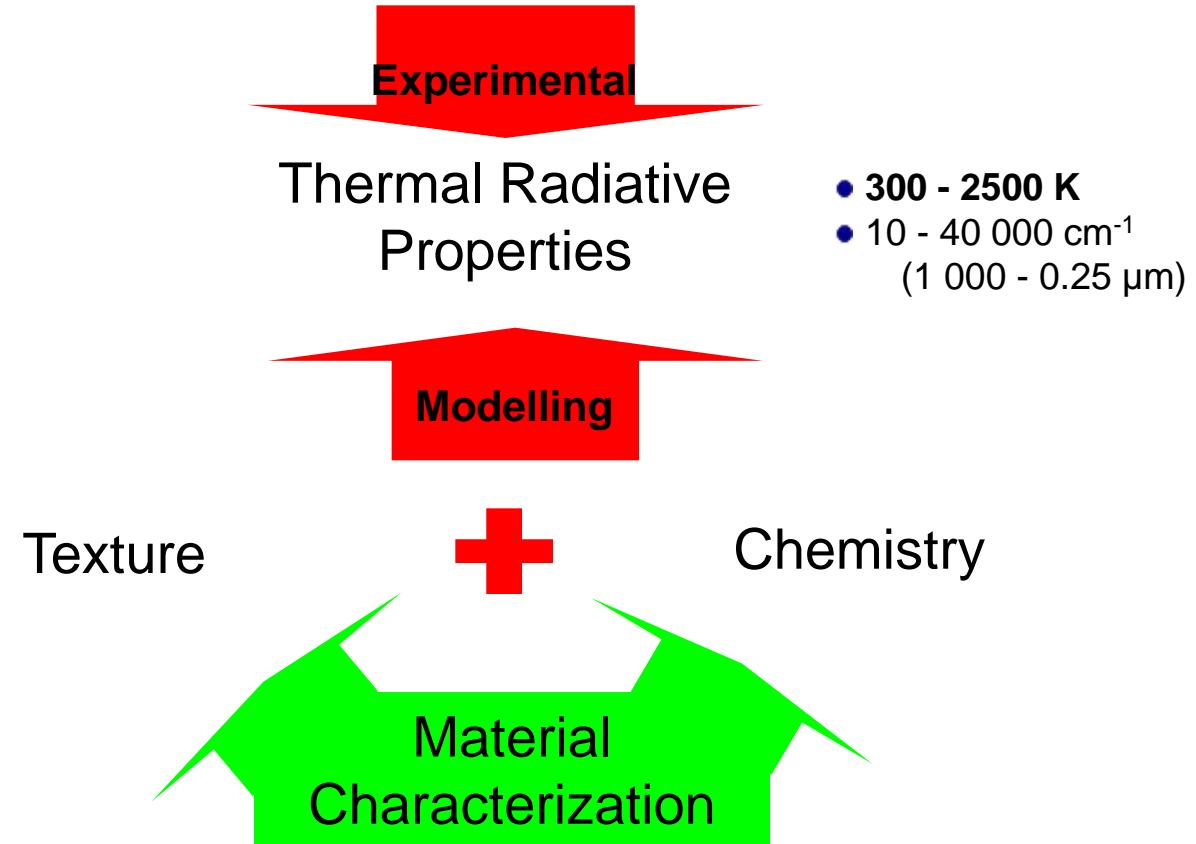


IR heaters

- Ceramic tile
- Praseodymium nickelate ($\text{Pr}_2\text{NiO}_{4+\delta}$)
- roughness
- nearly black body behavior



Infared emission spectroscopy



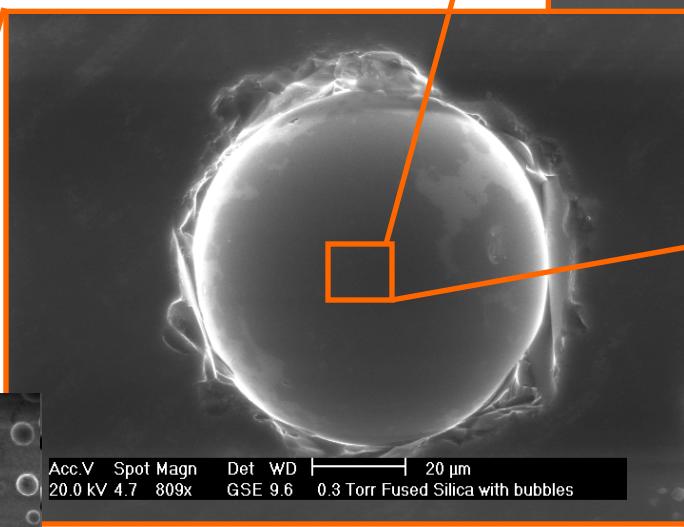
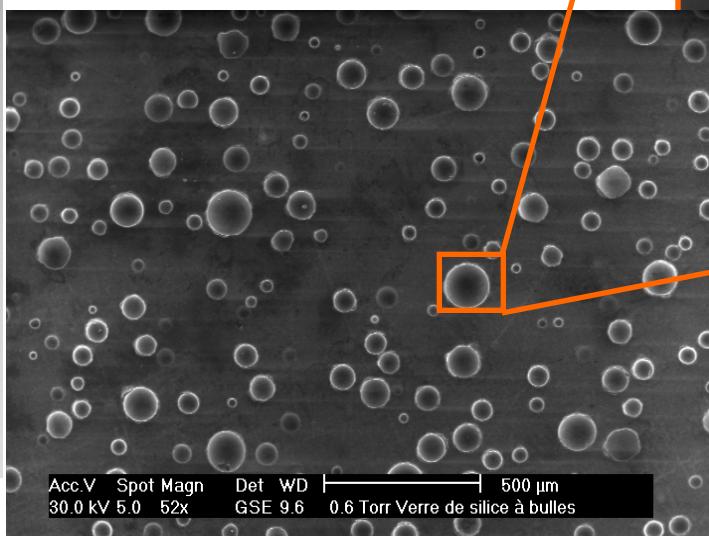
A SEMI TRANSPARENT COMPOUND :

SILICA GLASS WITH BUBBLES

Chemical Analysis

- fused silica based on grain quartz grains of high purity (99.99 %)
- amount of metallic impurities ~ 100 ppm

Textural Analysis

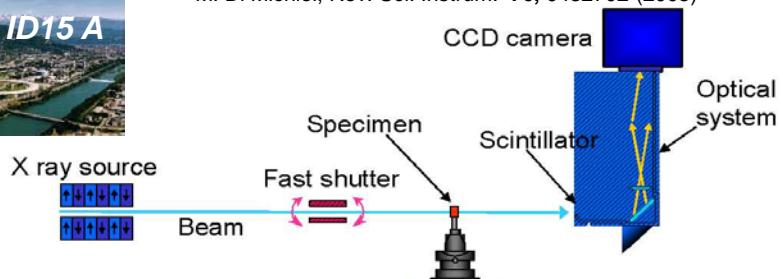


Magn Det WD 2 µm
8000x GSE 9.7 0.3 Torr Fused Silica with bubbles

IMAGE ANALYSING OF 3D DATA ($P = 12.9 \%$)

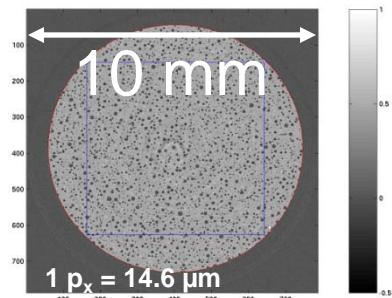


M. Di Michiel, Rev. Sci. Instrum. **76**, 0432702 (2005)

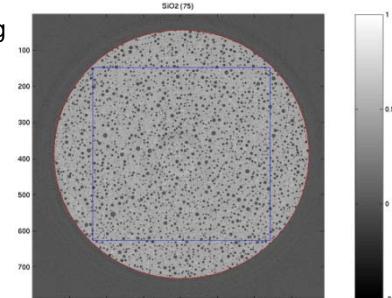


150 slides

SiO₂_plane_01.jpg



SiO₂_plane_075.jpg



SiO₂_plane_150.jpg

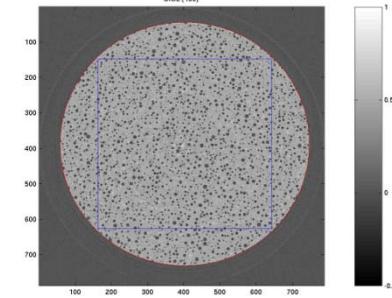
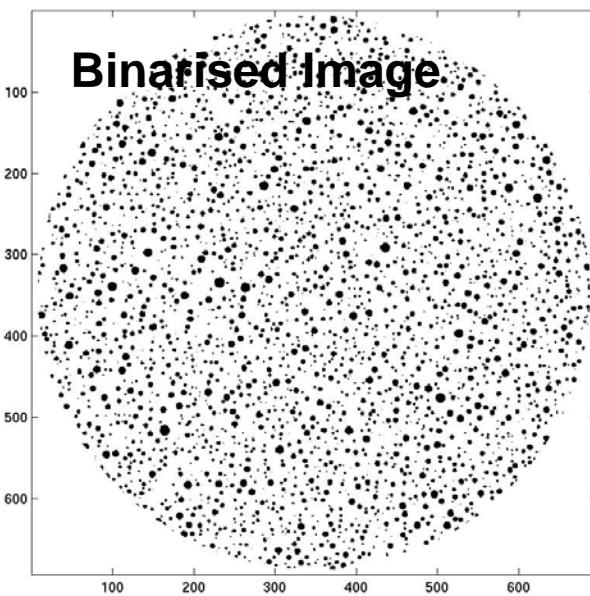
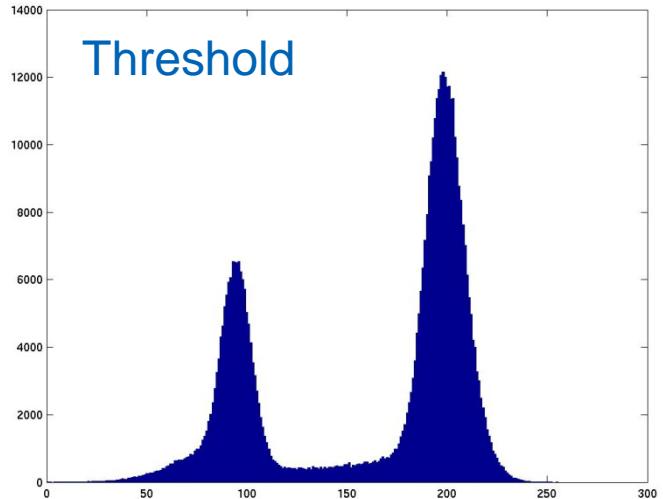
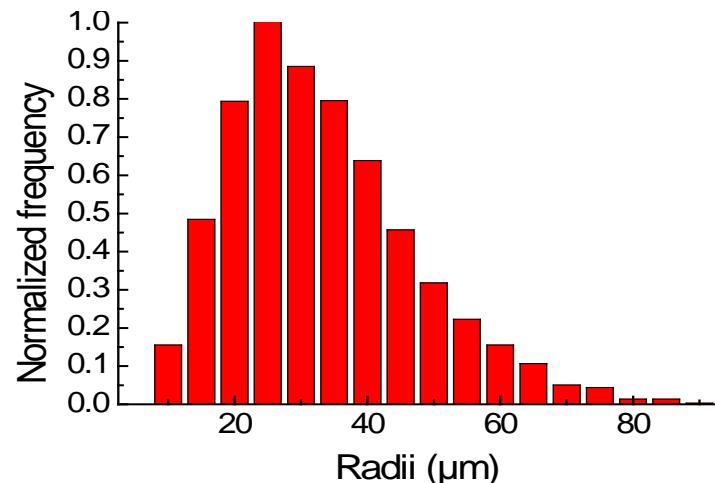


Image analyzing



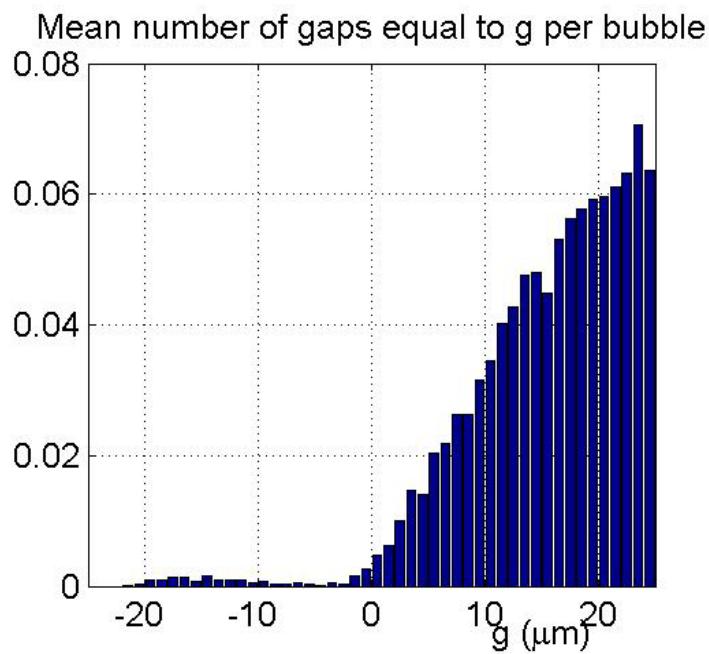
“MATERIAL PARAMETERS” → RAY TRACING?



$$25 < \lambda < 2 \mu\text{m} \quad (400 < \sigma < 5000 \text{ cm}^{-1})$$

$$x = \frac{2\pi \langle r \rangle}{\lambda} > 1$$

- ❖ Geometrical optics
- ❖ No diffraction



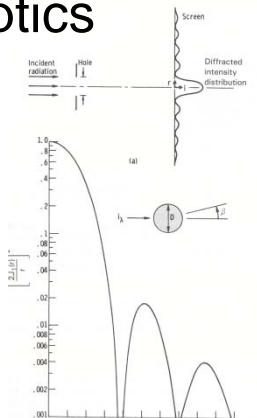
$$g/\lambda > 1/2$$

$$\langle r \rangle \approx g$$

- ❖ No interferences
- ❖ Multiple scattering

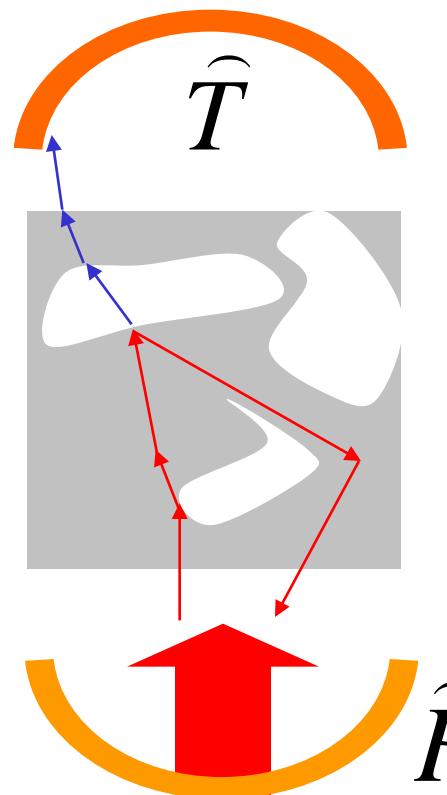
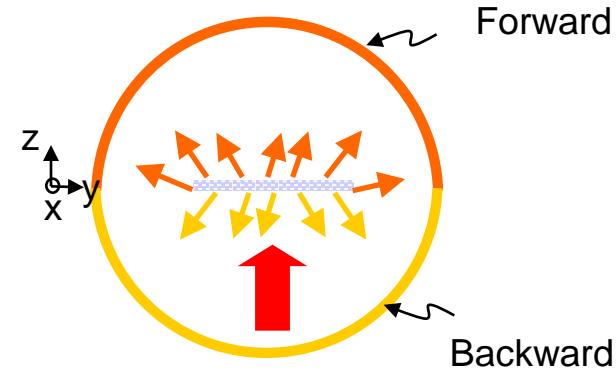
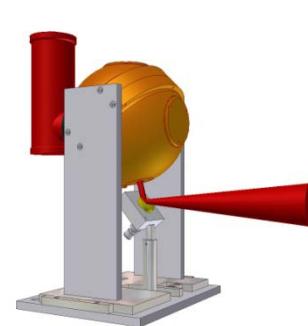


Multiple reflection



NUMERICAL EXPERIMENT

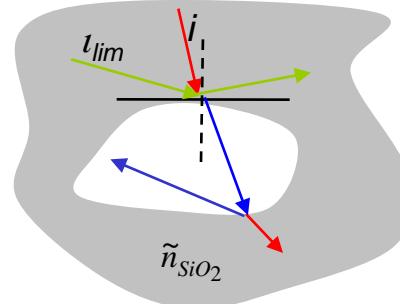
$$E(\sigma, \theta, T) = 1 - \hat{R}(\sigma, \theta, T) - \hat{T}(\sigma, \theta, T)$$



- Large number of rays : 10^5 - 10^6
- Simulation in a realistic reconstructed volume
- Large spectral domain [1-25 μm]
- Large set of statistic data
 - path length in the solid phase (transparent, semitransparent, opaque)
 - path length in the void phase
 - number of intercepted interfaces
 - position and incident angle of a photon (at the beginning of its travel)
 - position and exhaust angle of a photon (at the end of its travel)

ABSORPTION/SCATTERING PROCESS

❖ Refraction index gradient : **scattering**



MCRT procedure ($0 < \xi < 1$)

$\xi < \rho$: reflexion

$\xi > \rho$: refraction

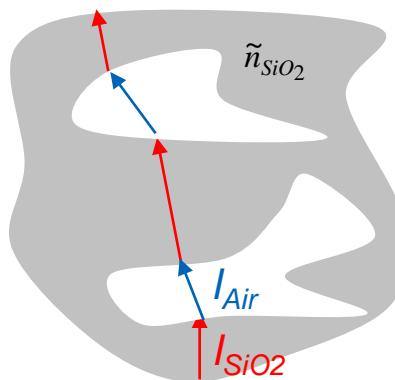
Fresnel's law

$$\rho(\sigma, T) = \frac{1}{2} \left[\left| \frac{\cos i / \cos \tilde{r}(\sigma, T) - \tilde{n}_1(\sigma, T) / \tilde{n}_2(\sigma, T)}{\cos i / \cos \tilde{r}(\sigma, T) + \tilde{n}_1(\sigma, T) / \tilde{n}_2(\sigma, T)} \right|^2 + \left| \frac{\cos \tilde{r}(\sigma, T) / \cos i - \tilde{n}_1(\sigma, T) / \tilde{n}_2(\sigma, T)}{\cos \tilde{r}(\sigma, T) / \cos i + \tilde{n}_1(\sigma, T) / \tilde{n}_2(\sigma, T)} \right|^2 \right]$$

Snell-Descartes 's law

$$\tilde{n}_{SiO_2} \sin i = \sin \tilde{r}$$

❖ Chemin optique : **absorption**



MCRT procedure

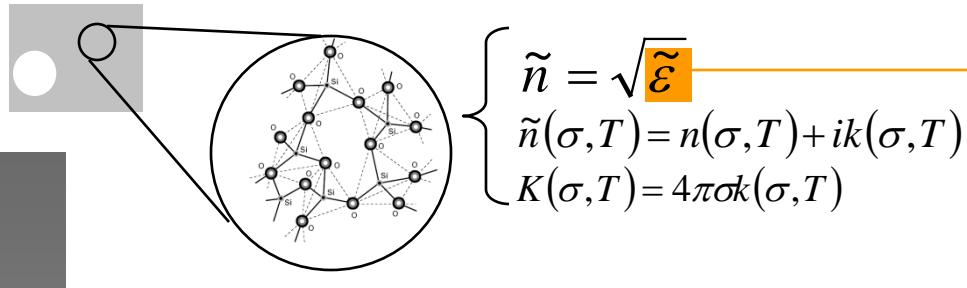
$$\sum_i I_i < 0.01$$

Beer-Lambert 's law

$$I_i = I_0 e^{-l_i K_i}$$

Key role :
Optical function (n, k , K)

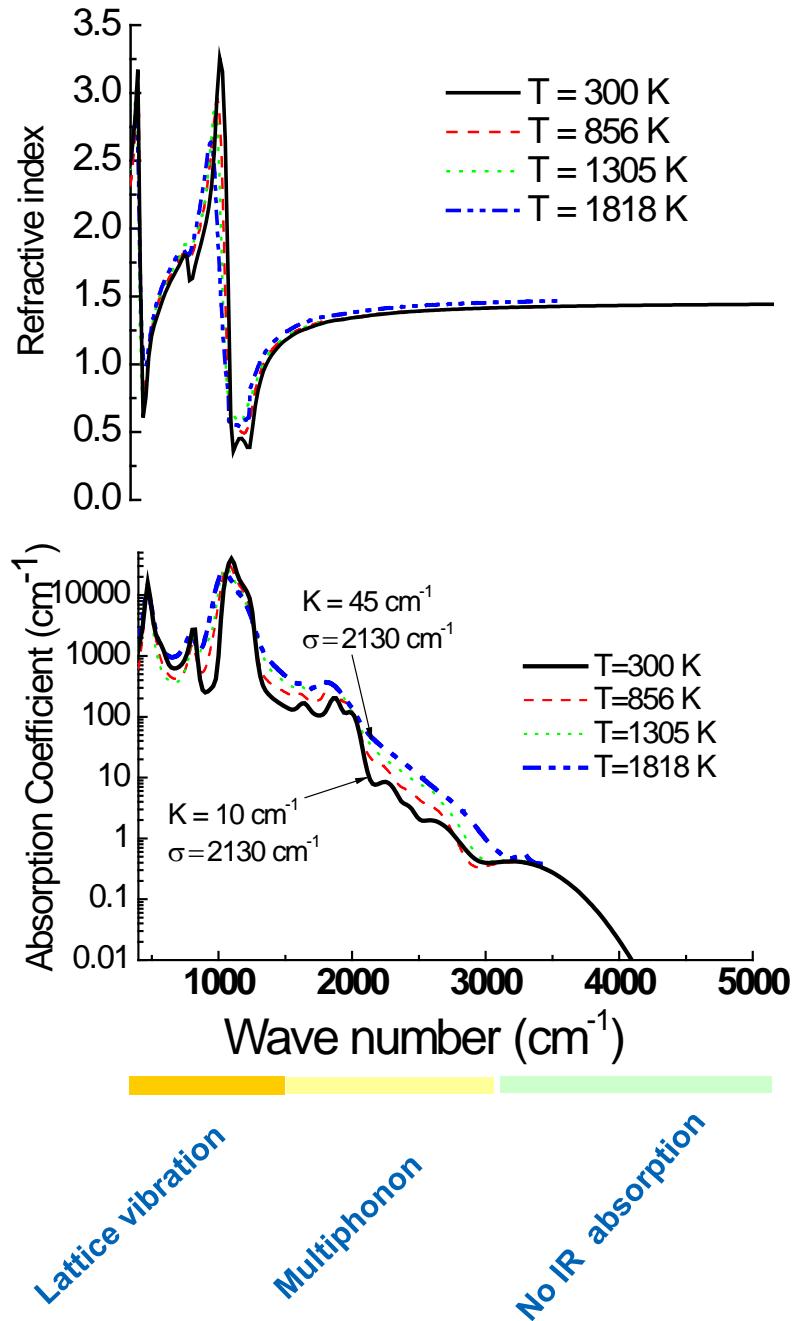
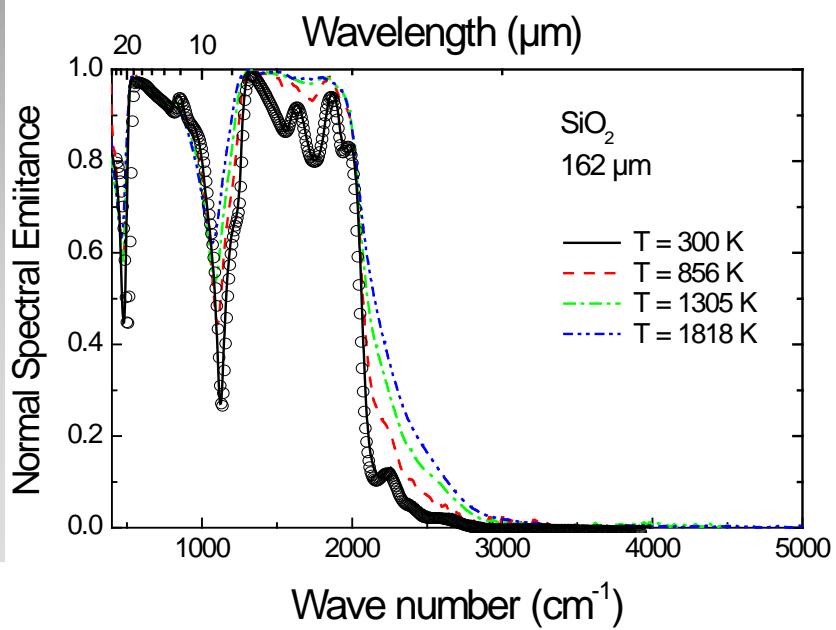
OPTICAL FUNCTIONS OF SiO_2



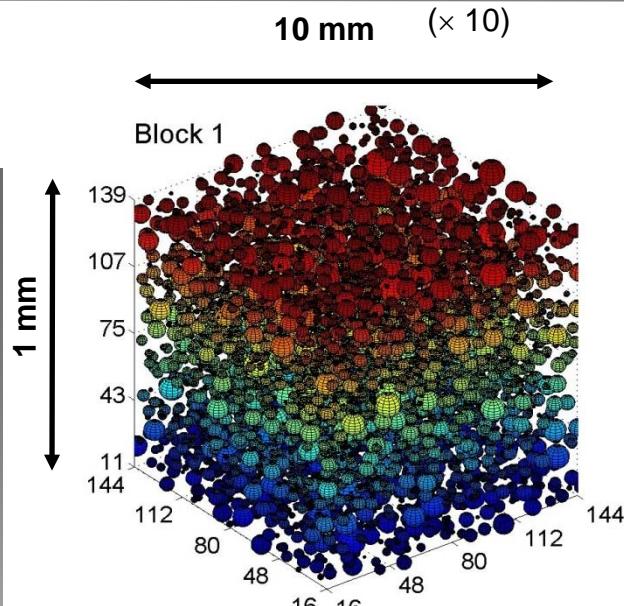
$$\tilde{\epsilon}(\omega, T) = \epsilon_{\infty} + \sum_j C_{Vj}(\omega; \omega_{0j}, \gamma_{Gj}, \gamma_{Lj})$$

De Sousa Meneses et al., JNCS, 351, (2005)

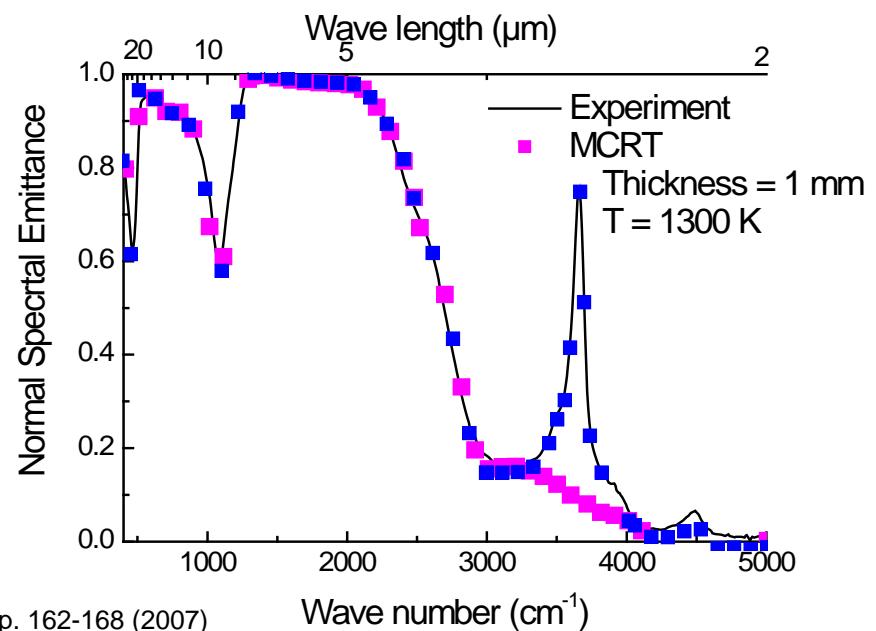
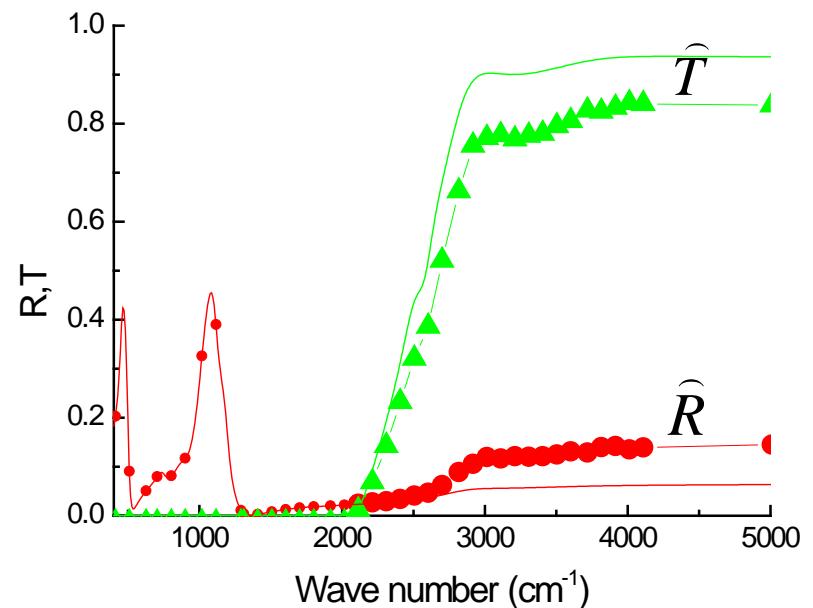
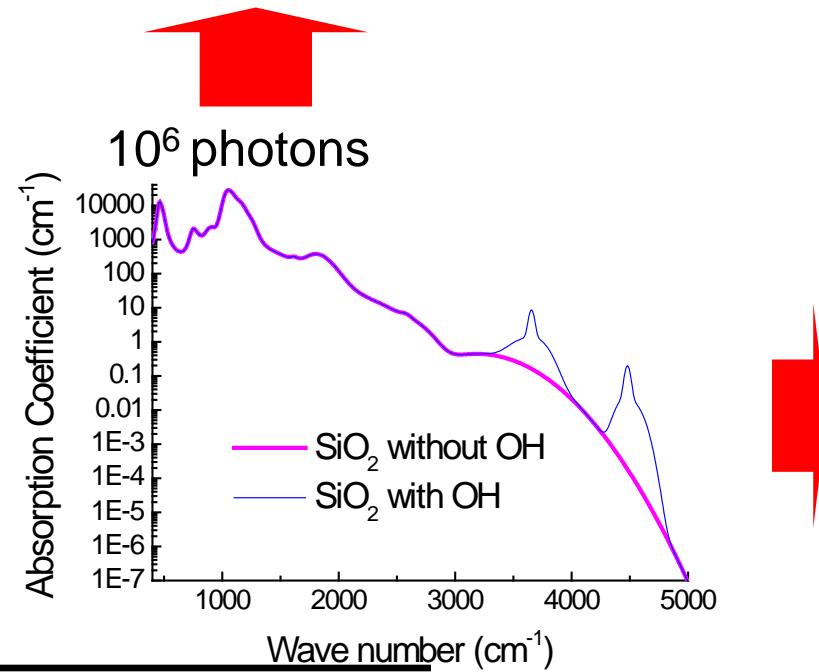
$$E(\omega, T) = \frac{(1 - \rho(\omega, T))(1 - e^{-K(\omega, T)d})}{1 - \rho(\omega, T)e^{-K(\omega, T)d}}$$



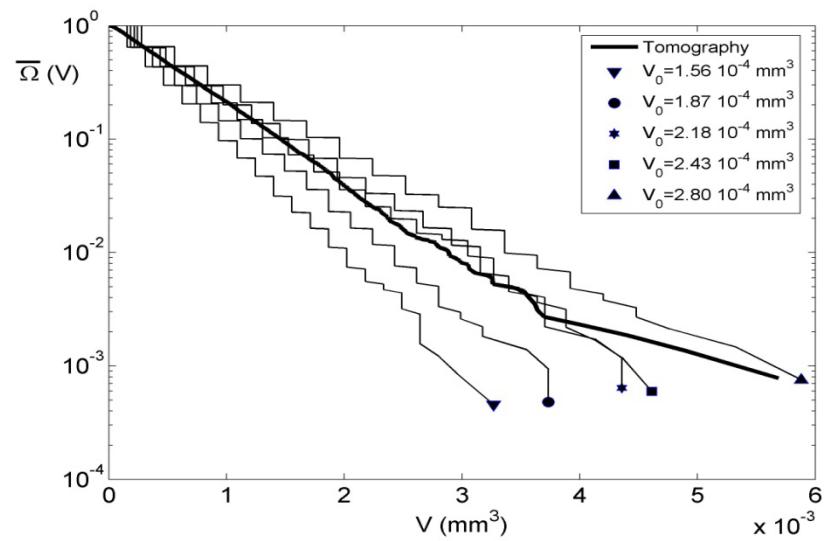
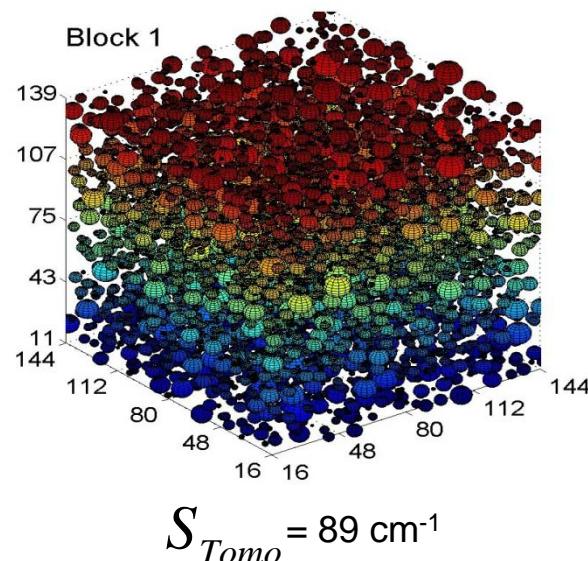
CHEMISTRY+MICROSTRUCTURE ?



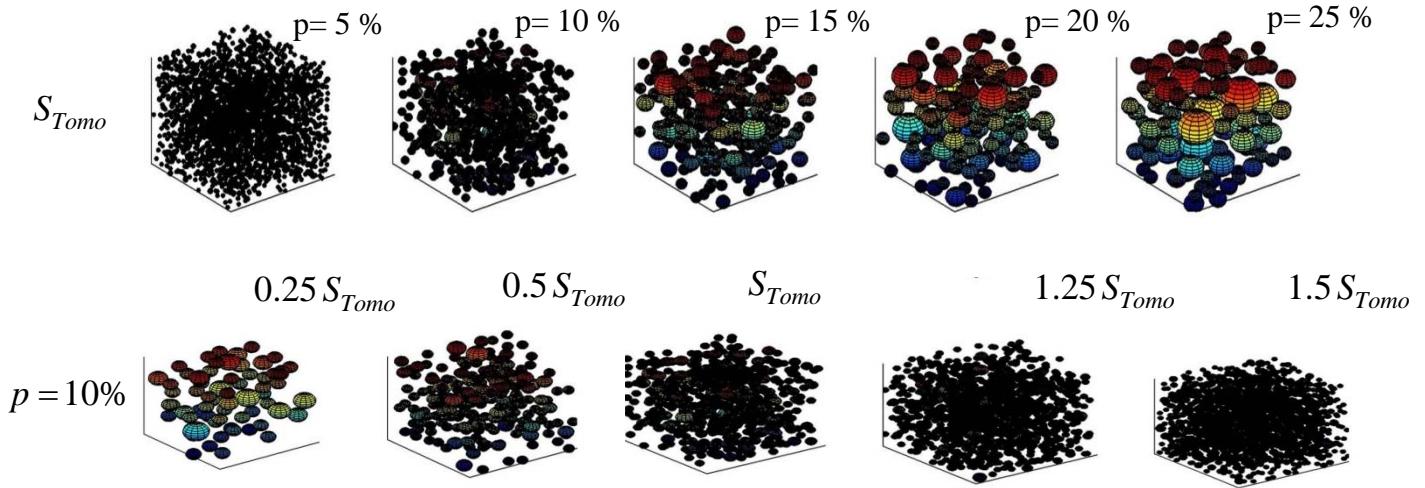
$$E = 1 - \hat{R} - \hat{T}$$



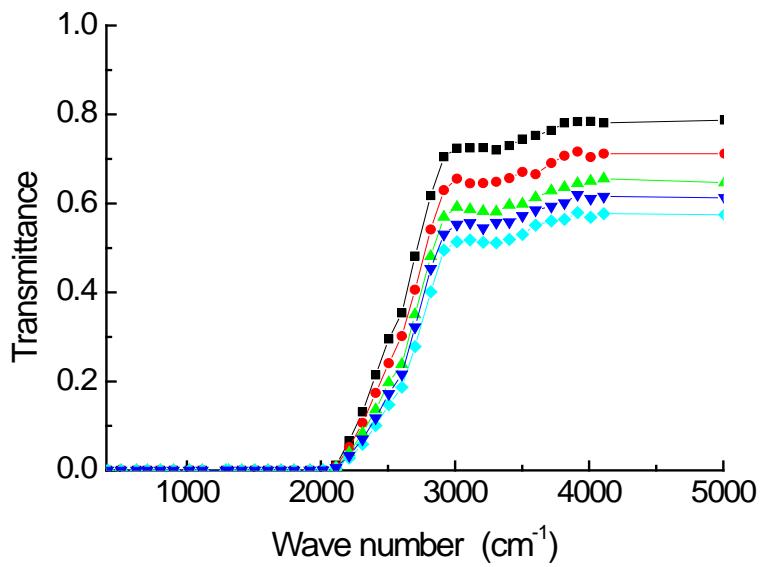
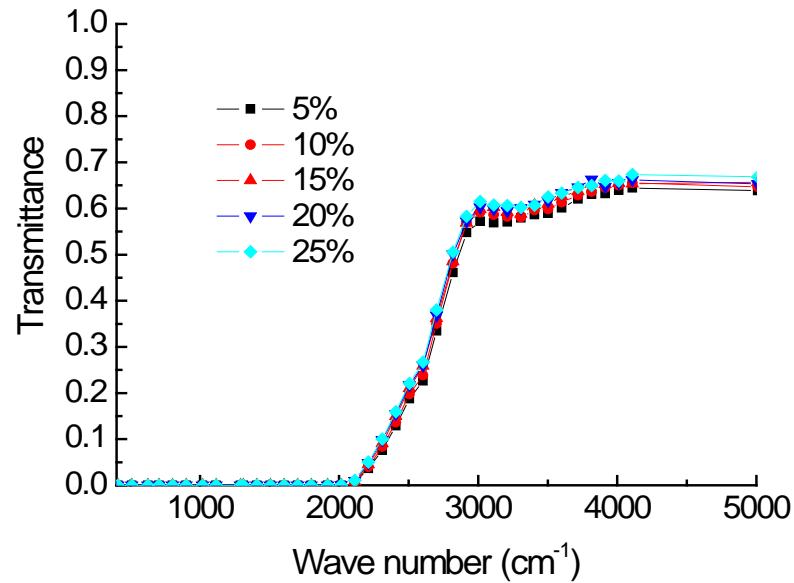
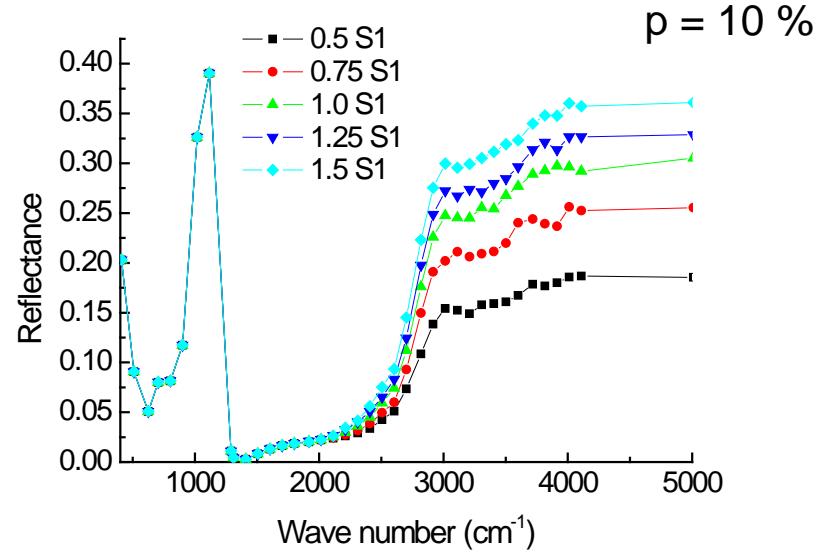
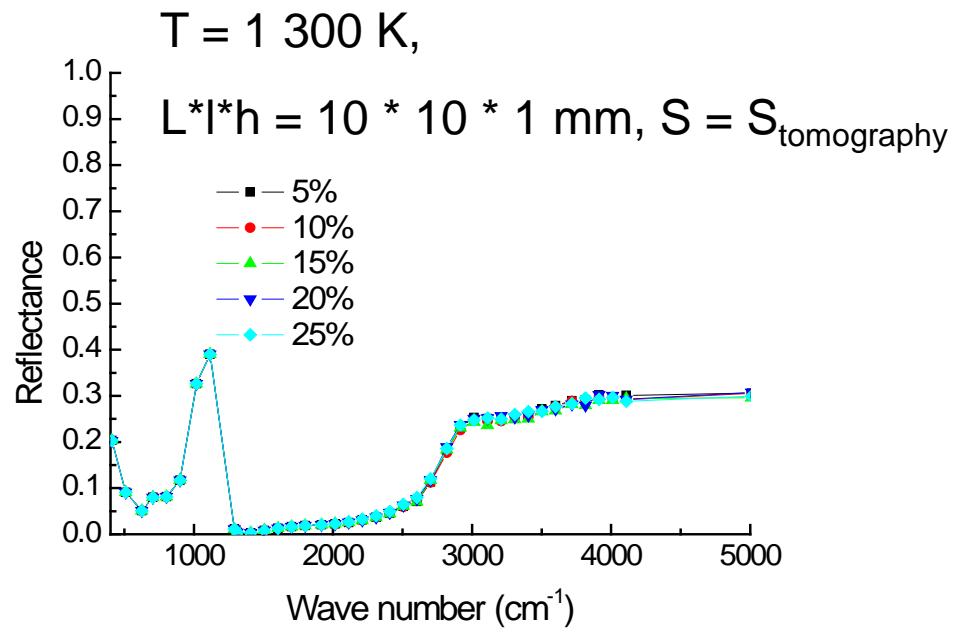
DESIGN OF POROUS GLASSES



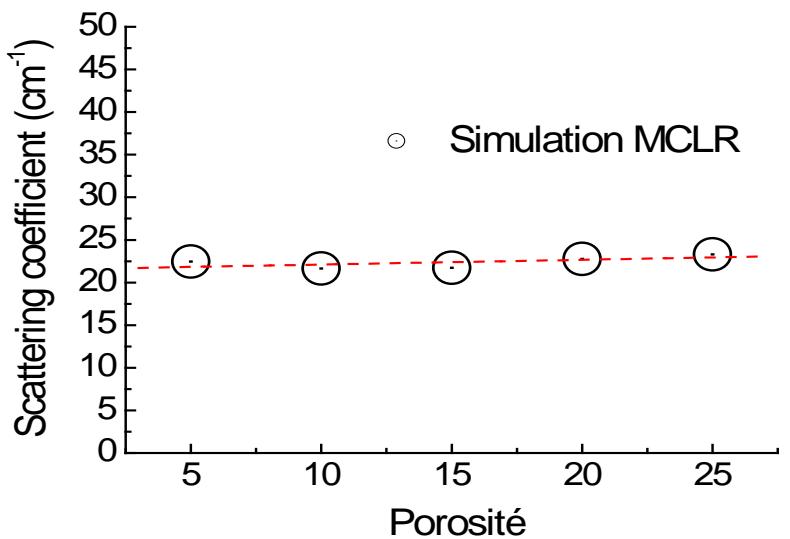
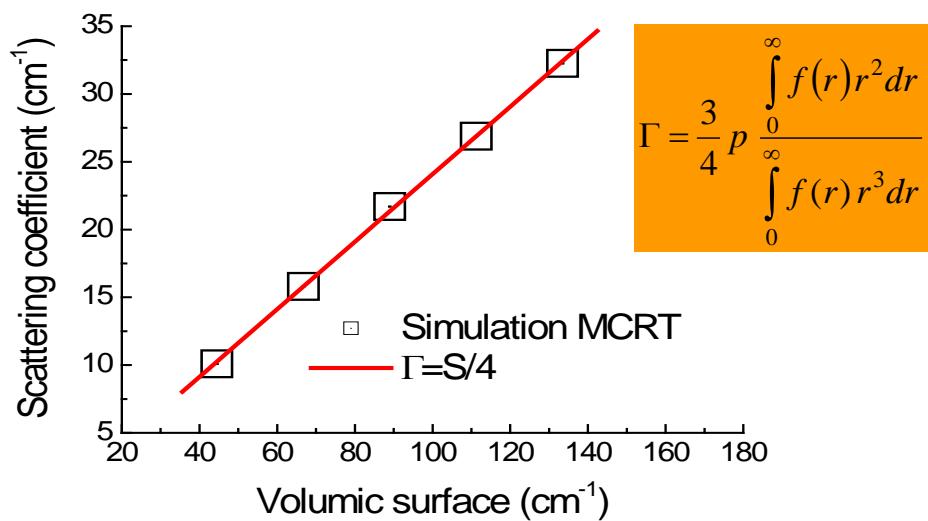
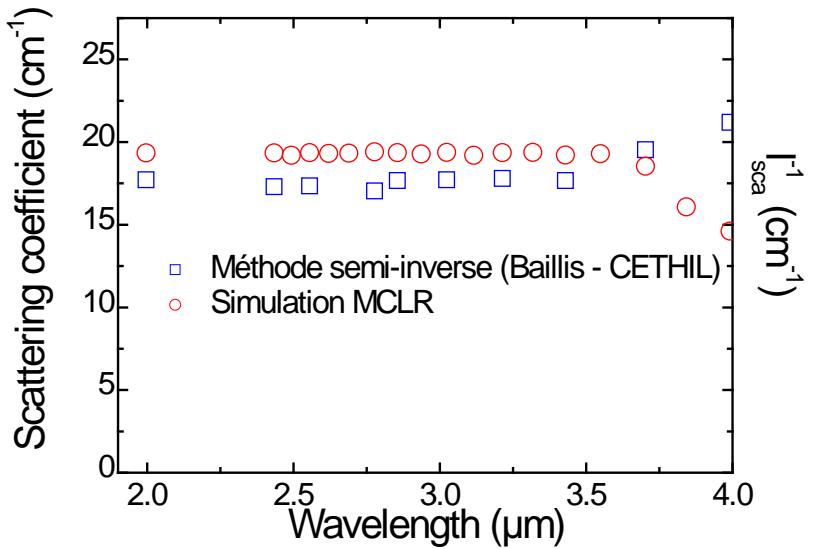
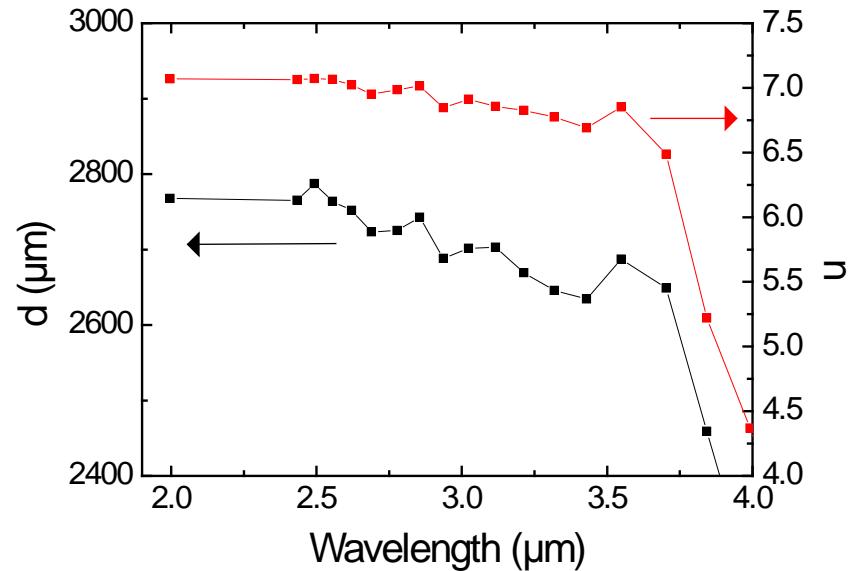
COALESCENCE MODEL



NUMERICAL RESULTS

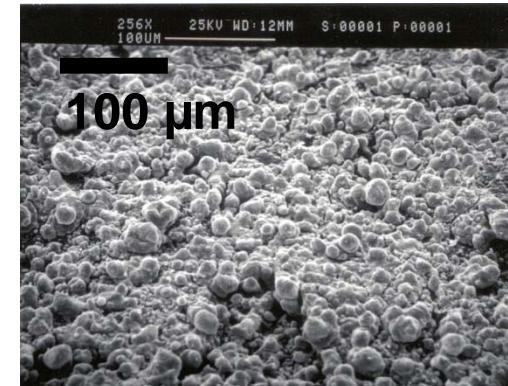


INFLUENCE OF THE VOLUMETRIC SURFACE

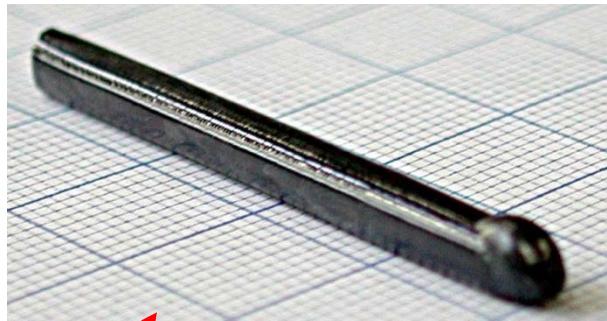


AN OPAQUE MEDIUM

ROUGH COATING OF $\text{Pr}_2\text{NiO}_{4+\delta}$



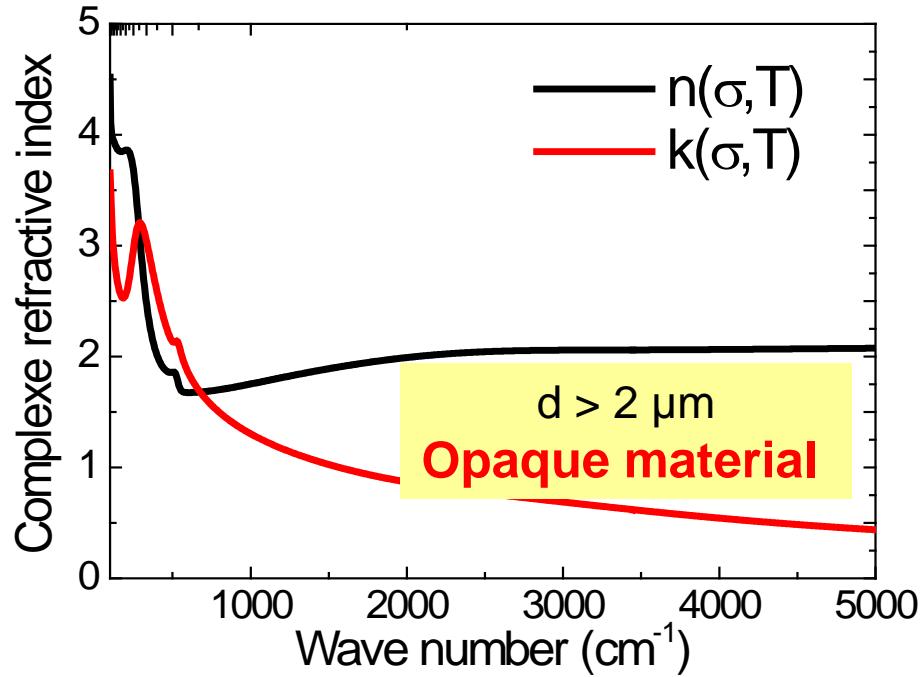
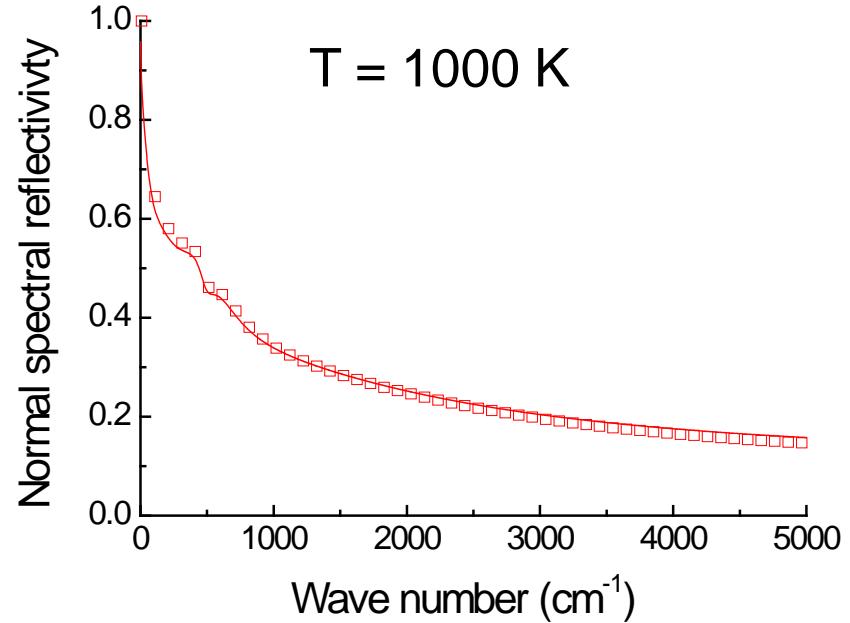
OPTICAL FUNCTIONS OF $\text{Pr}_2\text{NiO}_{4+\delta}$



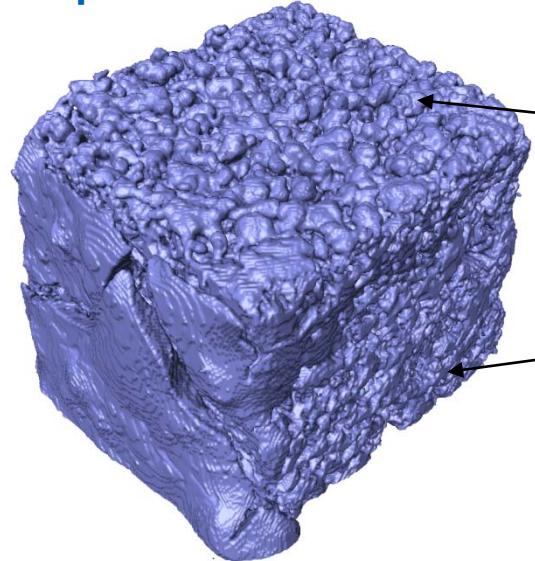
$$\rho(\sigma, T) = \frac{I_{\text{reflected}}(\sigma, T)}{I_0(\sigma, T)} = \left| \frac{\tilde{n}(\sigma, T) - 1}{\tilde{n}(\sigma, T) + 1} \right|^2 = \left| \frac{\sqrt{\tilde{\varepsilon}(\sigma, T)} - 1}{\sqrt{\tilde{\varepsilon}(\sigma, T)} + 1} \right|^2$$

$$\frac{\tilde{\varepsilon}(\sigma, T)}{\varepsilon_\infty} = \prod_j \frac{\Omega_{Loj,T}^2 - \sigma^2 + i\gamma_{Loj,T}\sigma}{\Omega_{Toj,T}^2 - \sigma^2 + i\gamma_{Toj,T}\sigma} - \frac{\Omega_{pl,T}^2 - \sigma^2 + i\gamma_{pl,T}\sigma}{\sigma(\sigma - i\gamma_{o,T})}$$

B. Rousseau et al. PRB 2005

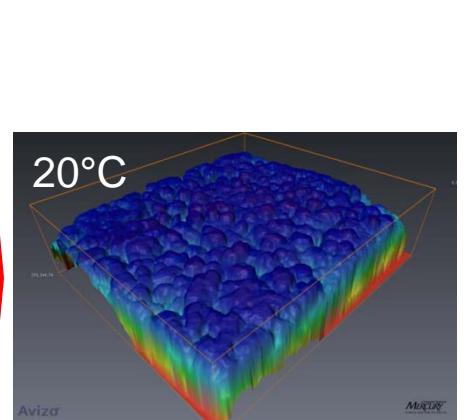
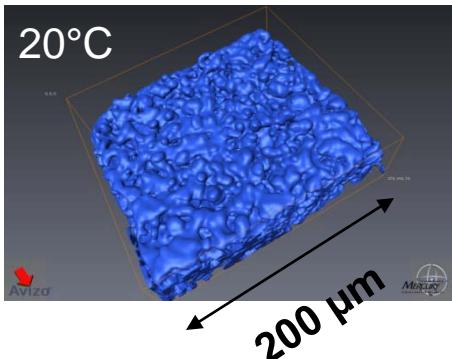
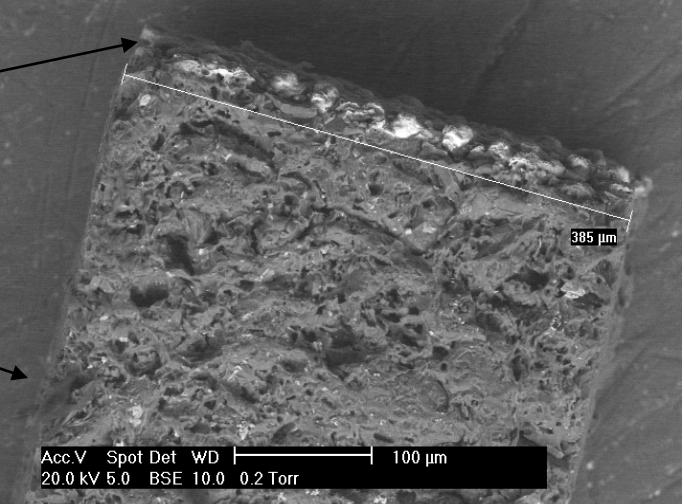


X-RAY μ -TOMOGRAPHY Resolution $\sim 0.7 \mu\text{m}$

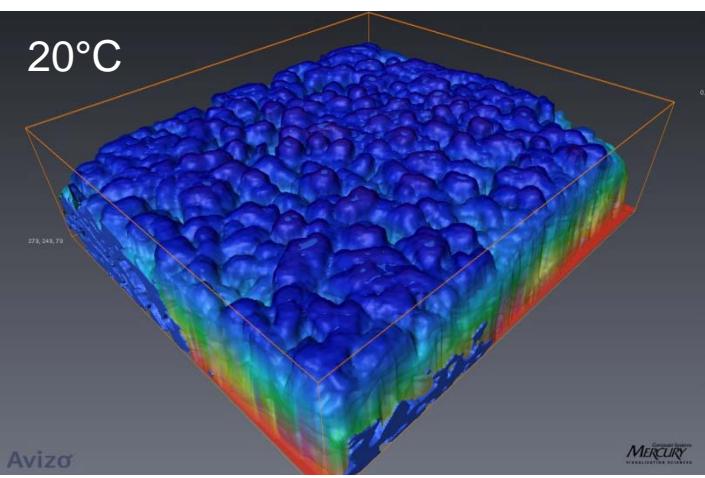


Rough coating
 $\text{Pr}_2\text{NiO}_{4+\delta}$

Alumino-silicate tile



HEIGHT CARD ON
A REGULAR GRID
[280×250]

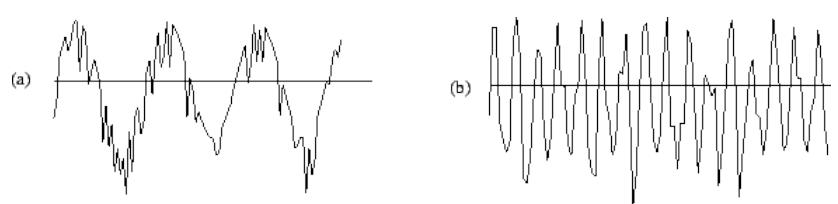


Statistical parameters

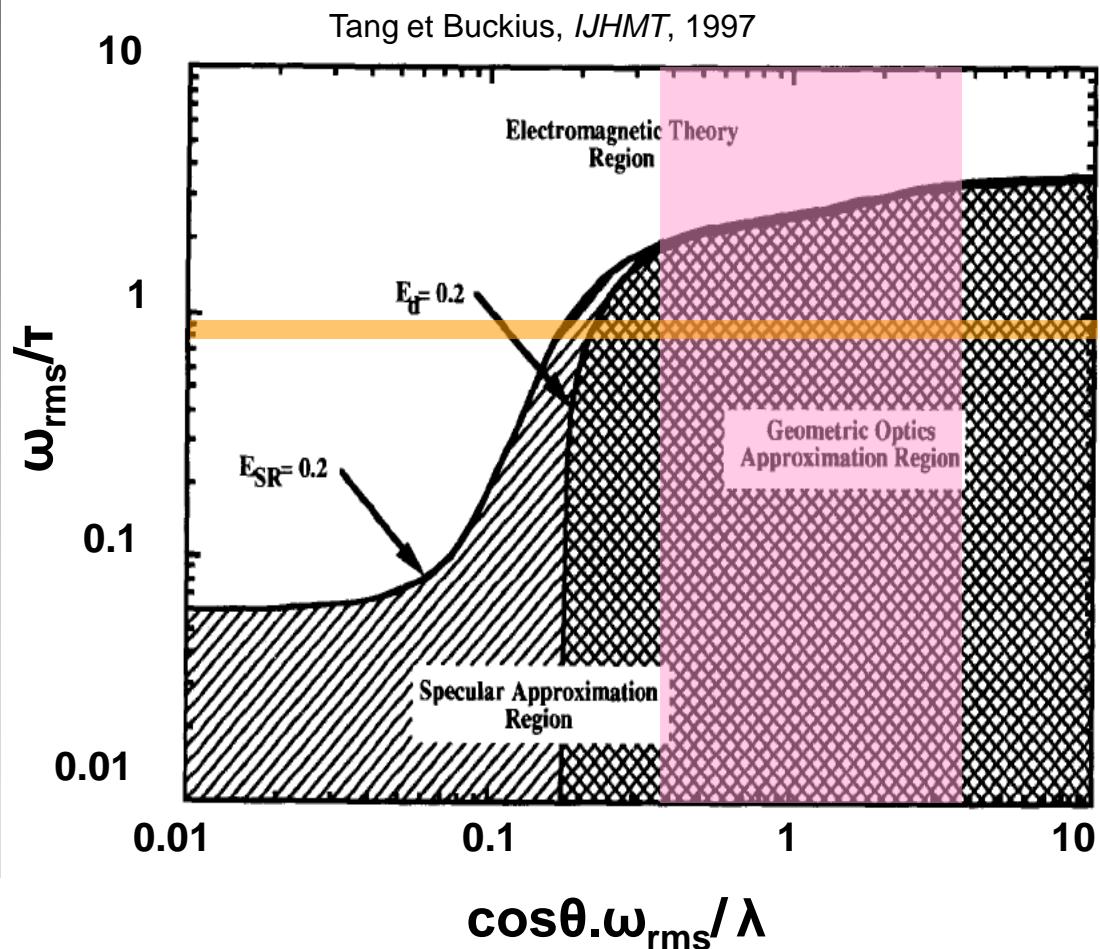
$$R_z(u) = \frac{\langle\langle Z(x,y)\rangle\langle Z(x+u,y)\rangle}{\langle Z(x,y)^2\rangle}$$

$$\omega_{rms} = \sqrt{\langle Z(x,y)^2 \rangle}$$

$$\tau = R_z(e^{-1})$$



Light Matter Interaction



300 K

$$\omega_{rms} = 5.5 \mu\text{m}$$

$$\tau = 8.4 \mu\text{m}$$

500 K

$$\omega_{rms} = 5.7 \mu\text{m}$$

$$\tau = 8.7 \mu\text{m}$$

900 K

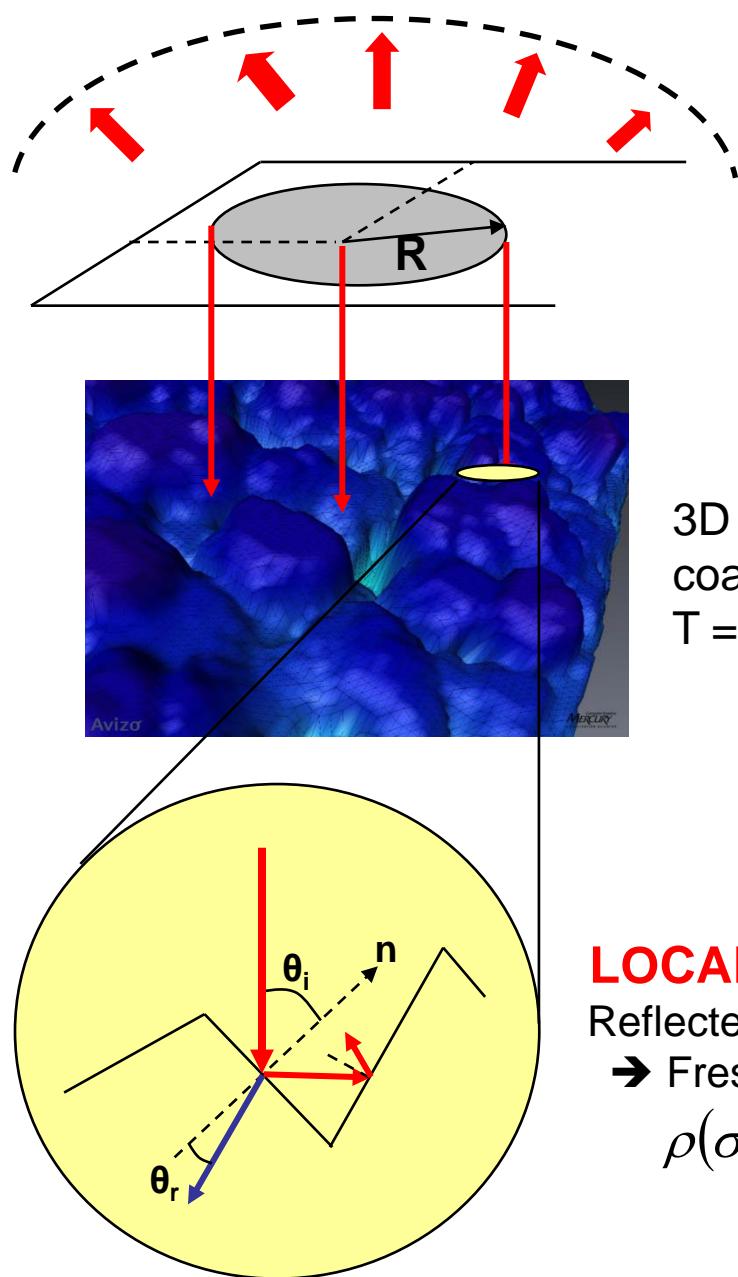
$$\omega_{rms} = 5.6 \mu\text{m}$$

$$\tau = 8.3 \mu\text{m}$$



Geometrical optics

MODELLING : ROUGH SURFACE

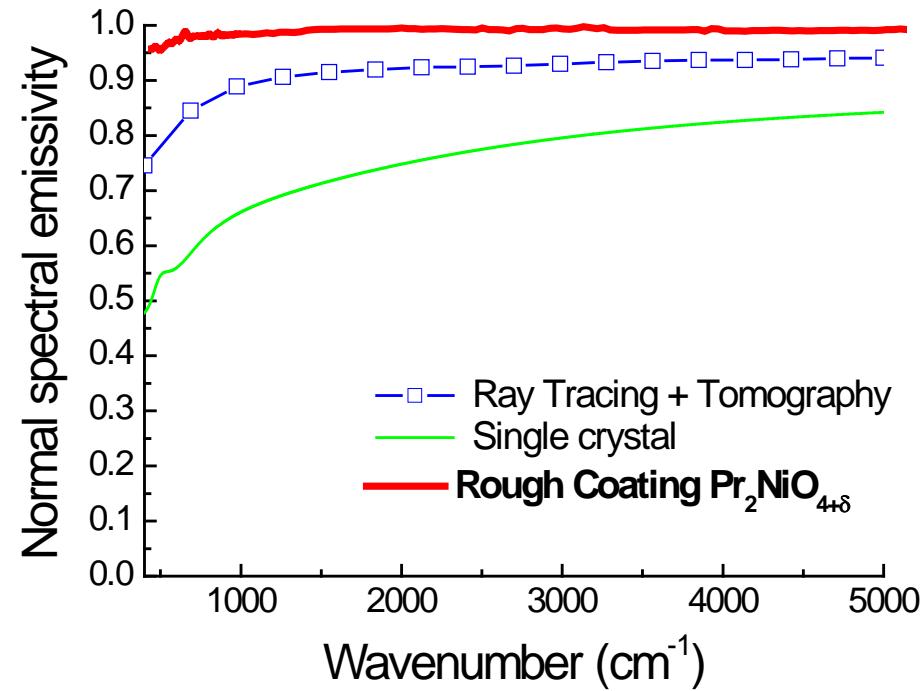


To reproduce an experiment where :

$$E = 1 - \bar{R}$$

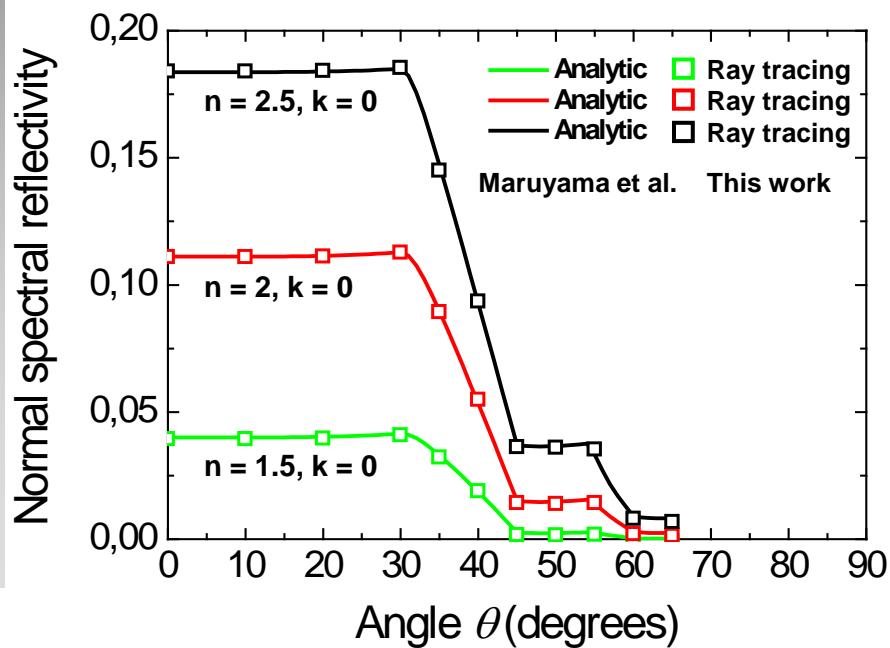
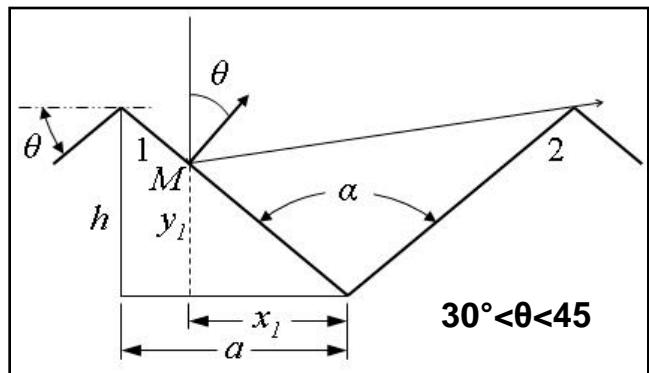
Large number (10^6) of rays issued from an infrared parallel beam are thrown onto the numeric surface

3D image of the coating surface
 $T = 900 \text{ K}$



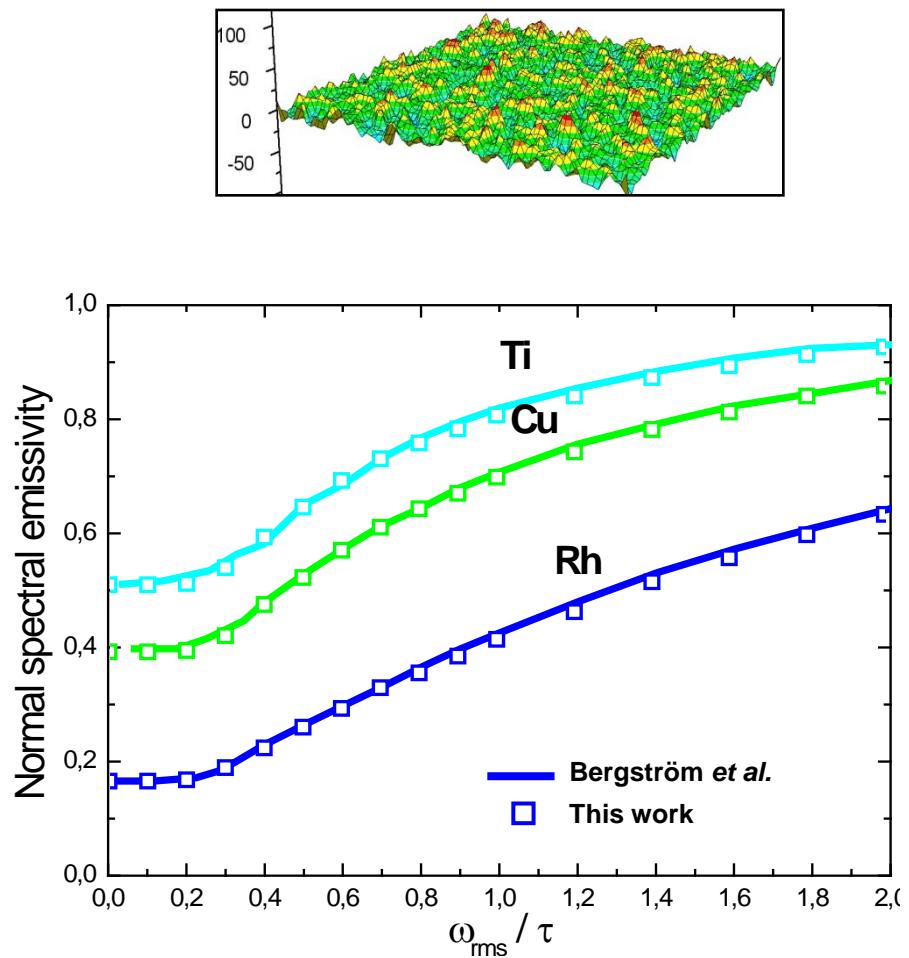
2D-surface with V-groove cavities: An analytic model

(Sacadura, IJHMT, 1972 & Maruyama et al., SEMSC, 2004)

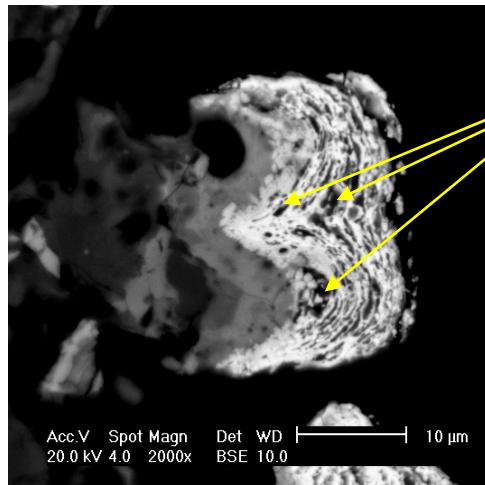


3D-random rough surface (gaussian): Literature-ray tracing data

(Bergstrom et al., JAP, 2008)



EFFECT OF THE INTERNAL MICROSTRUCTURE



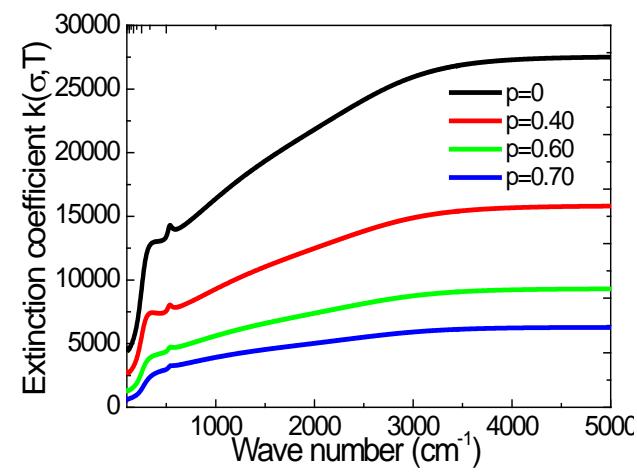
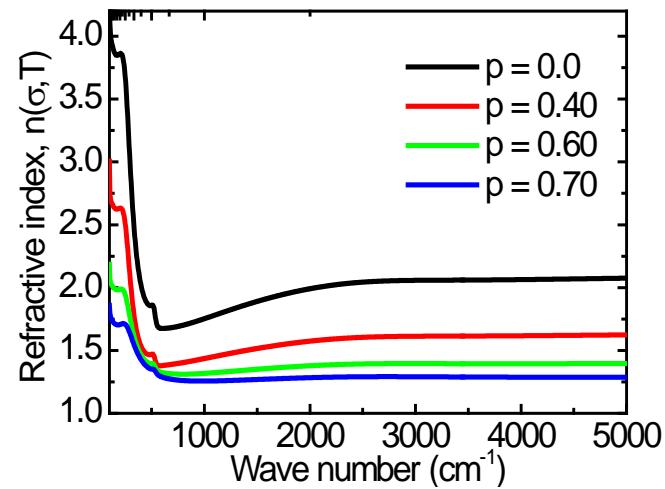
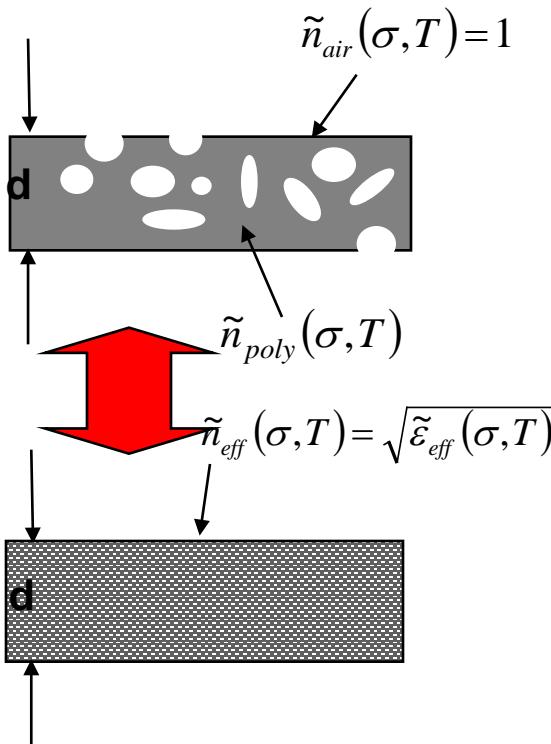
pore : 50 -200 nm

$d_{pore} \ll \lambda_{infrared} (2-20 \mu\text{m})$

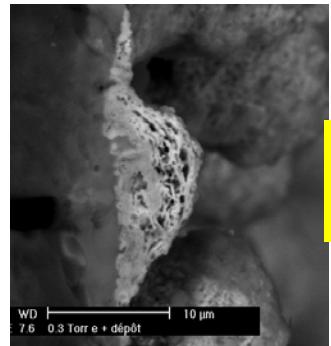
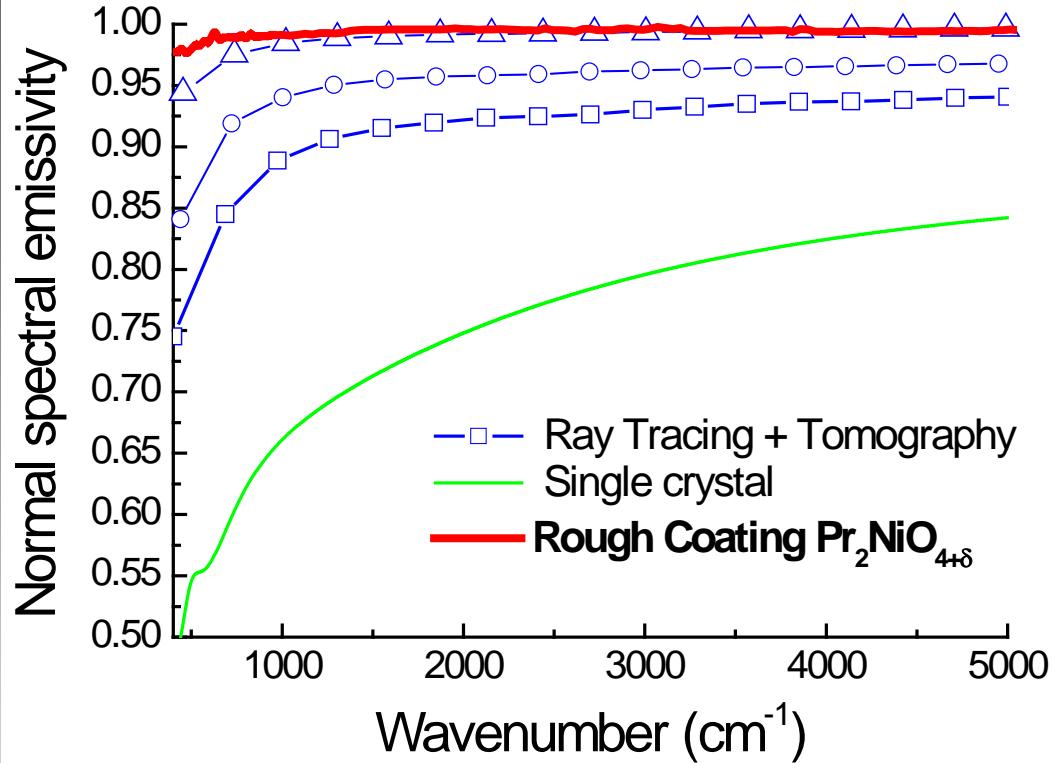
$$(1-p) \frac{\tilde{\varepsilon}_{poly}(\sigma, T) - \tilde{\varepsilon}_{eff}(\sigma, T)}{\tilde{\varepsilon}_{eff}(\sigma, T) + y_{poly}(\tilde{\varepsilon}_{poly}(\sigma, T) - \tilde{\varepsilon}_{eff}(\sigma, T))} + p \frac{\tilde{\varepsilon}_{pore}(\sigma, T) - \tilde{\varepsilon}_{eff}(\sigma, T)}{\tilde{\varepsilon}_{eff}(\sigma, T) + y_{pore}(\tilde{\varepsilon}_{pore}(\sigma, T) - \tilde{\varepsilon}_{eff}(\sigma, T))} = 0$$

Effective Medium Approximation

D.E. Apnes, optical properties of thin films, Thin Solid Films 89 (1982) 249



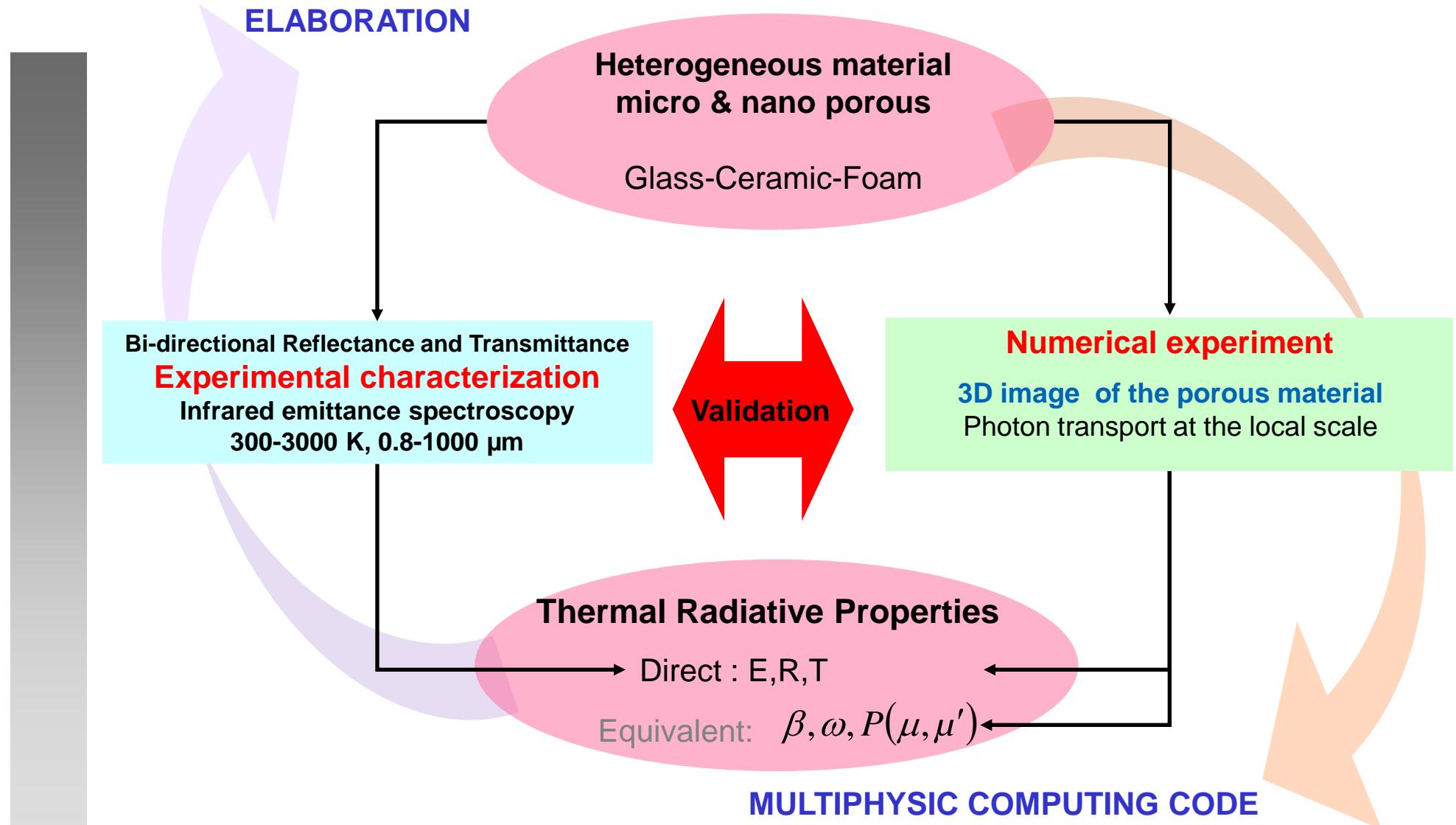
$p = 70\% \quad d > 11 \mu\text{m}$ (opaque)



ESTIMATION OF THE POROSITY OF A
COLLECTION OF GRAINS?

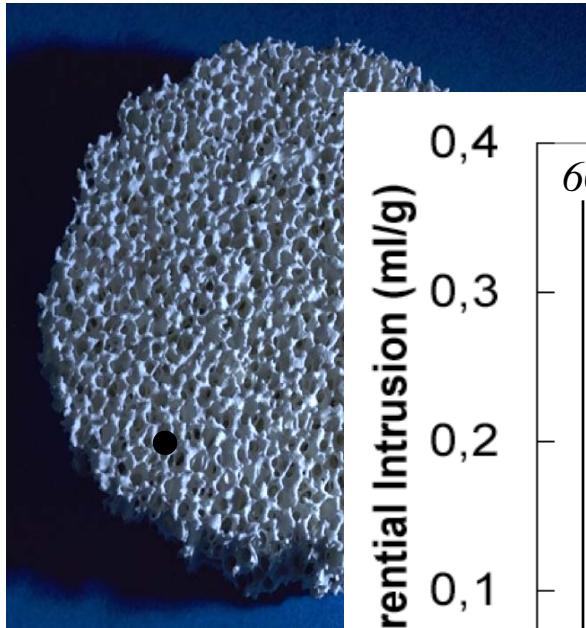
Thèse Hector Gomart, Université d'Orléans, 2008

MATERIAL

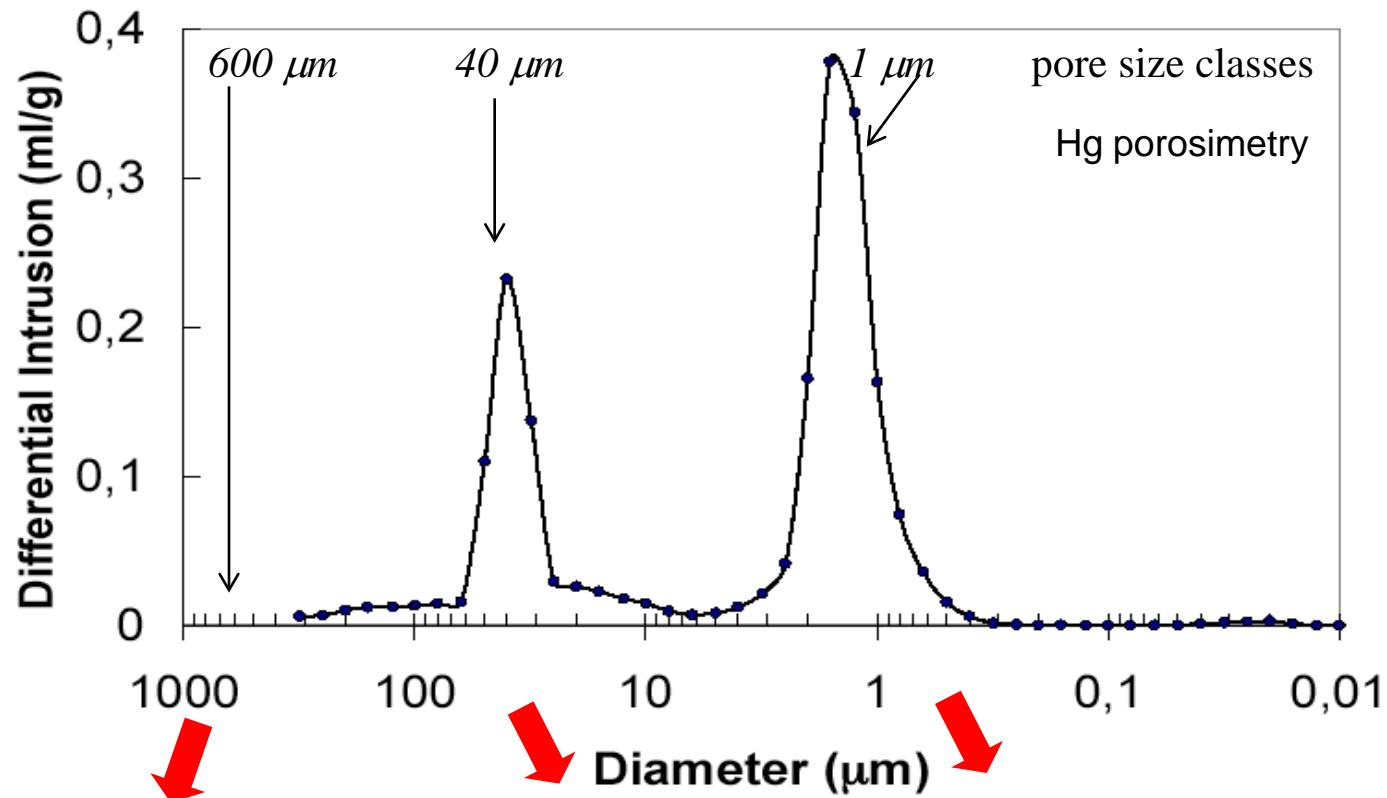


A MORE COMPLEX SAMPLE :MULLITE FOAM

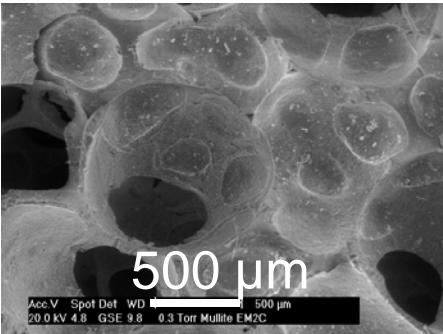
WORK PERFORMED WITH EM2C & CETHIL



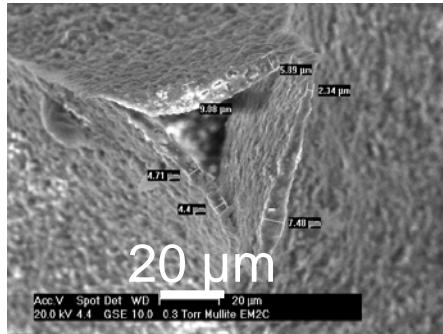
Mullite f (porosity) for catalytic c



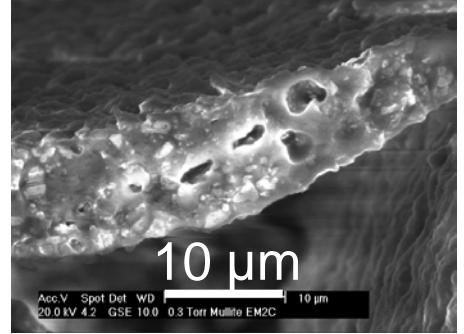
500 μ m



500 μ m



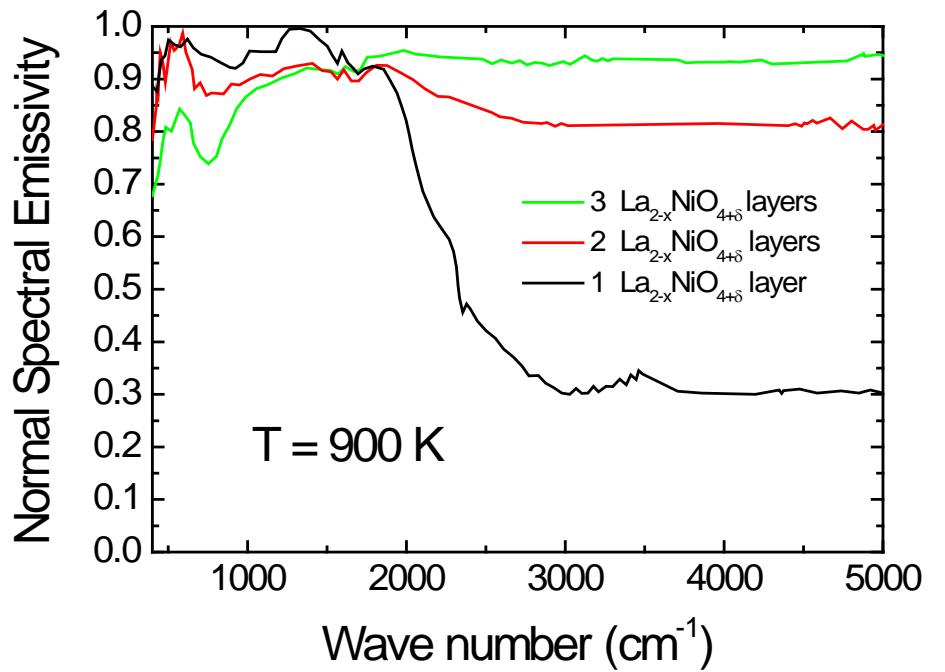
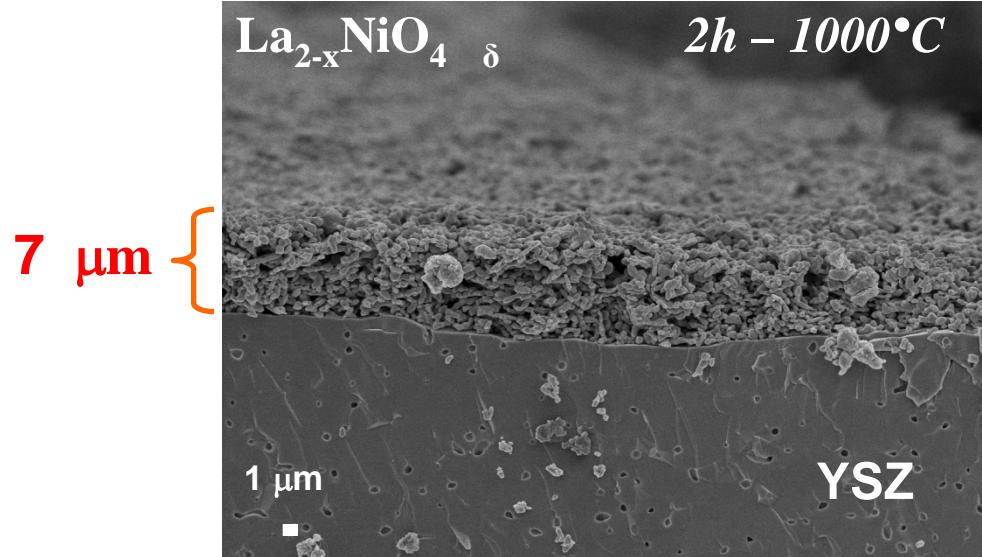
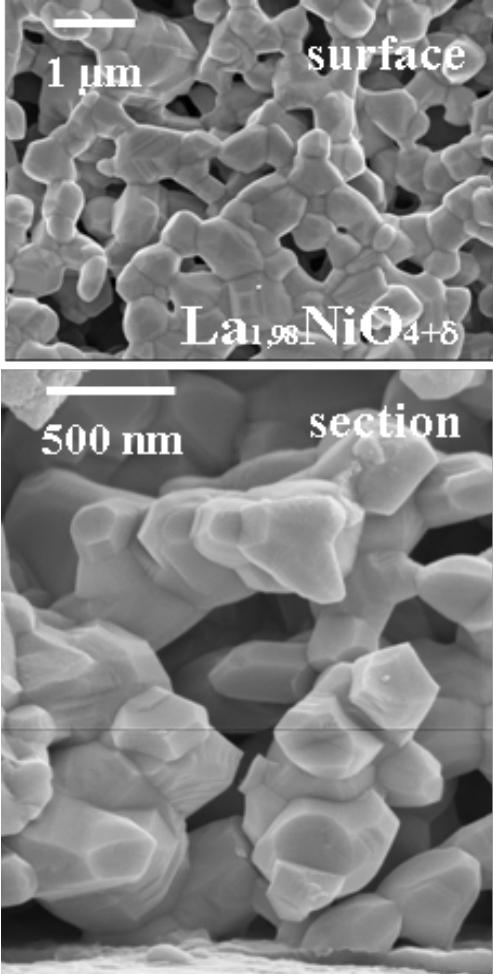
20 μ m



10 μ m

SOFC CATHODE

MIEC cathode

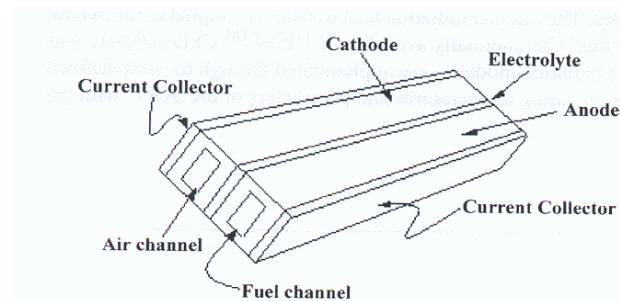


HEAT TRANSFER IN SOFC?

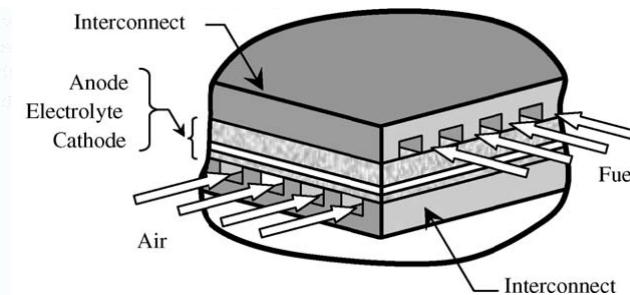
Thermo-mechanical failures in the ceramics used in the design of SOFC

Local temperature gradient at the interface of each component

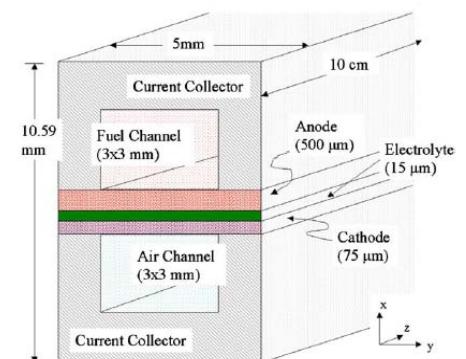
**Prediction of the temperature field in the cell
(ceramics+interconnects)**



Murthy et al., J. Power Sources 2006



K.J. Daum et al. , J. Power Sources (2006)



Damm et al., Transaction of the ASME, 2005