

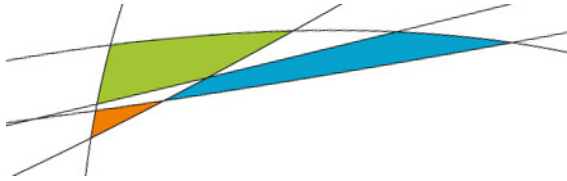
Amélioration des performances énergétiques d'un échangeur pas brumisation

F. Trinquet





- Travaux de l'équipe ENERFRI
- Spray : Impact sur un échangeur à air



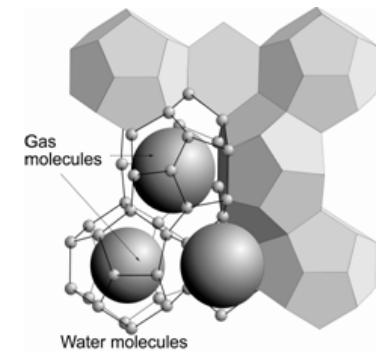
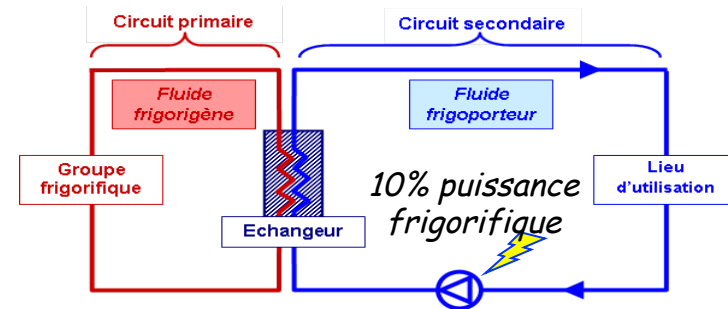
- Travaux de l'équipe ENERFRI
 - *Coulis d'hydrates*
 - *Matériaux à changement de phase*
 - *Réduction de charge*

- Spray : Impact sur un échangeur à air

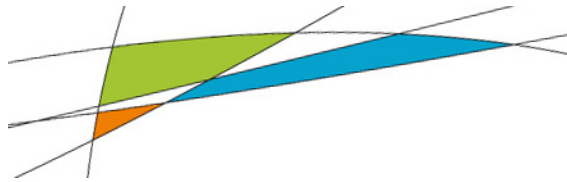


Coulis d'hydrates

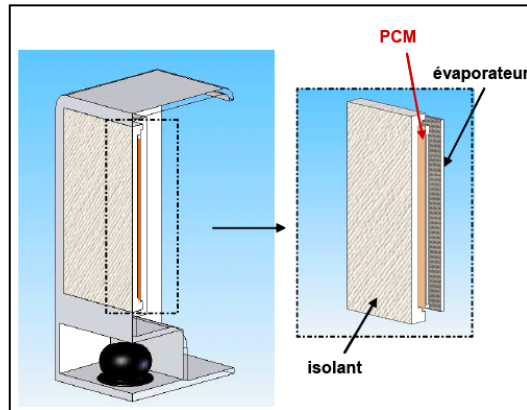
- Secondary refrigeration
 - ⇒ Containment of refrigerants
 - ⇒ Reduction by a factor of 10
- Two phase secondary refrigerant
 - High energy density : Slurry of 25% (100 kJ/kg) ~ 5 x Monophasic liquid ($\Delta T=5^{\circ}\text{C}$)
 - Increase the energy efficiency of the system (offset losses : pumps, exchanger)
- Applications
 - Air conditioning, Distribution Networks (Japan), Storage ...
- What is a hydrate?
 - Like crystal compound of ice water molecules forming cages, which trap other molecules, ex : CH_4 , CO_2 ...
- Interest for refrigeration
 - Equivalent latent heat or > than the ice.
 - Stable at $T > 0$ (air conditioning)
 - Formation by injecting CO_2 (non-mechanical)



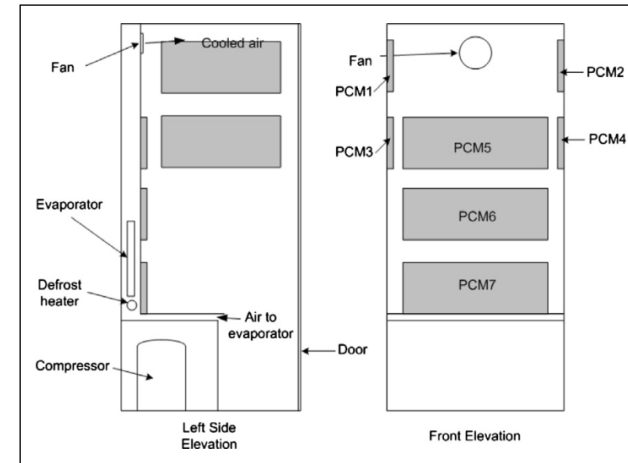
Coulis d'hydrate de TBAB
 Tanasawa et Takao, 4th Int. Conf. on
 Gas Hydrates, Yokohama, 2002



Matériaux à Changement de Phase (MCP)

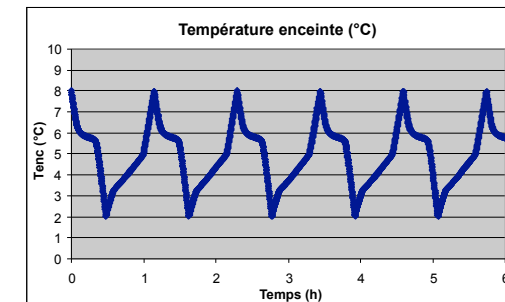
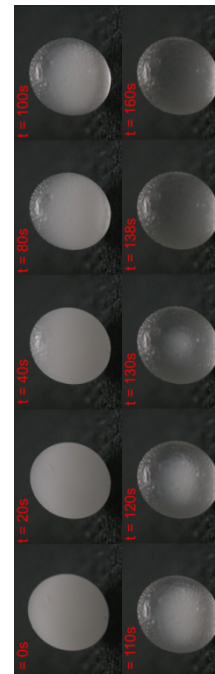
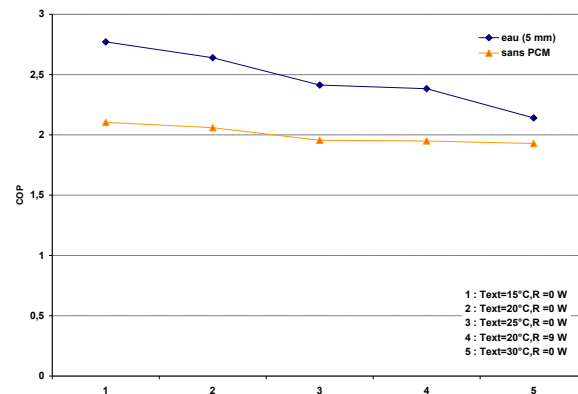


domestic refrigerator



Positionnement des plaques de M.C.P. dans le congélateur - B. Gin et al. (2010)

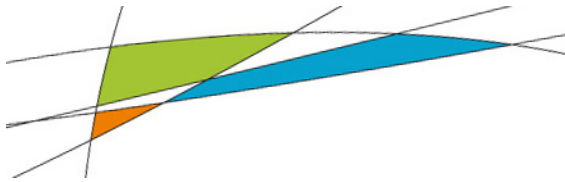
K. Azzouz (2008)



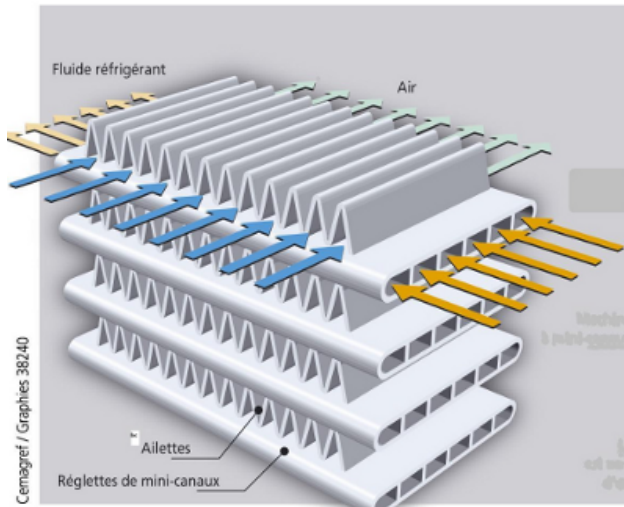
F. Trinquet, L. Fournaison, D. Leducq, A. Delahaye

- Amortization of temperature changes
- Up to 30% savings on COP
- Autonomy

- Energy savings to defrost and door openings (~ 50%)
- Limit the number of starts the chiller
- Stabilize the temperature in the enclosure



Réduction de charge



- Under control technology for condensers automobile air conditioning.
- Compact, lightweight.
- Reduced internal volume : load reduced refrigerant.
- Thermal performance.

- Refrigerant distribution.
- Behavior frosting / icing.

→ Some results ...

Installation	Classique	Charge réduite
Constructeur	Searle MDA 22-6	mini-canaux Valeo
D_{int}	7,93 mm (3/8")	1,49 mm
V_{int}	6 l	0,77 l
L_{totale}	122 m (4x30,3)	250 m (2x32x7x0,56)
S_{air}	33 m ²	32 m ²
$S_{frigorigène}$	3,0 m ²	1,5 m ²
Pas ailettes	2,12 mm	1,28 mm
Coeff. d'échange	20 W/K	32,8 W/K
Débit d'air	5 200 m ³ /h	5 100 m ³ /h + VEV



- Travaux de l'équipe ENERFRI
- Spray : Impact sur un échangeur à air



- Travaux de l'équipe ENERFRI
- Spray : Impact sur un échangeur à air
 - *Contexte de l'étude*
 - *Moyens mis en œuvre*
 - *Résultats*



Contexte de l'étude

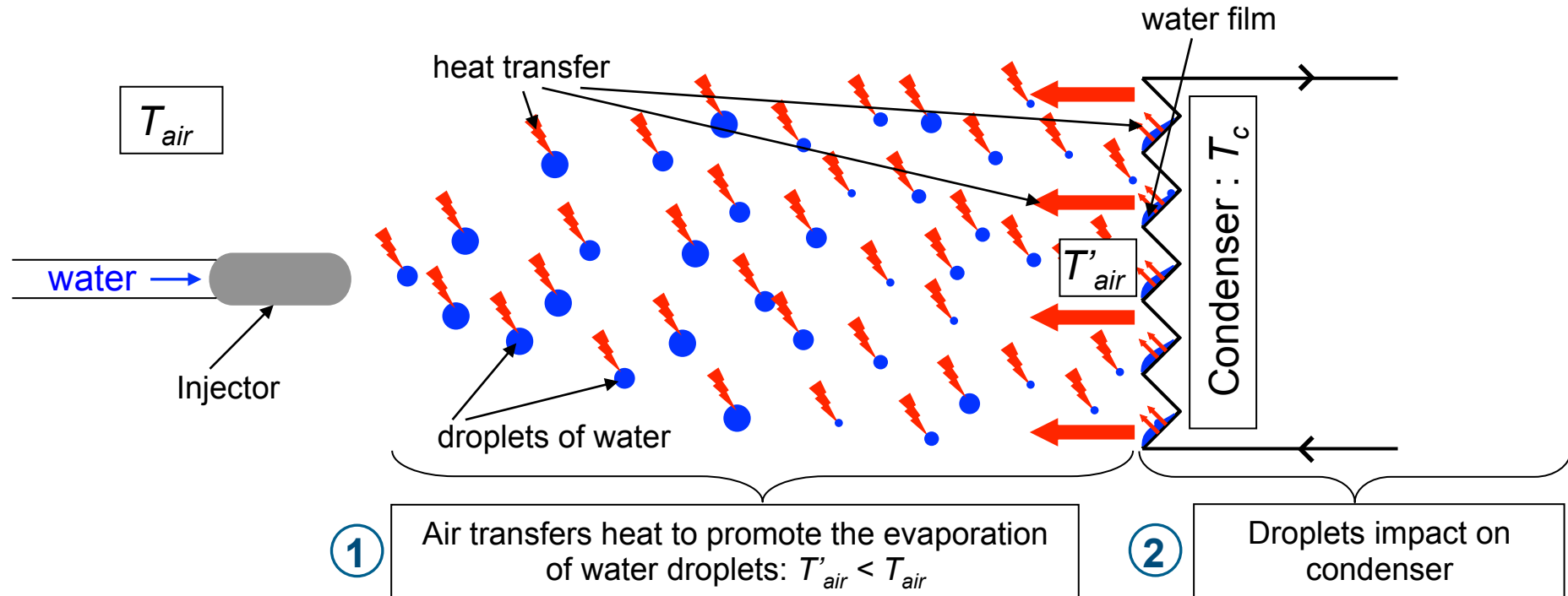
- **Goals**

- **Significant reduction in the amount of energy compared to traditional systems.**
- **Operating conditions during high ambient temperatures.**
- **No risk of bacterial growth : Legionella type for example.**
- **Optimize water consumption in this type of installation.**

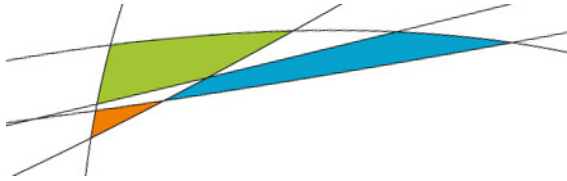


Contexte de l'étude

- Some principles



→ Possibility of lower T_c therefore increased COP



Contexte de l'étude

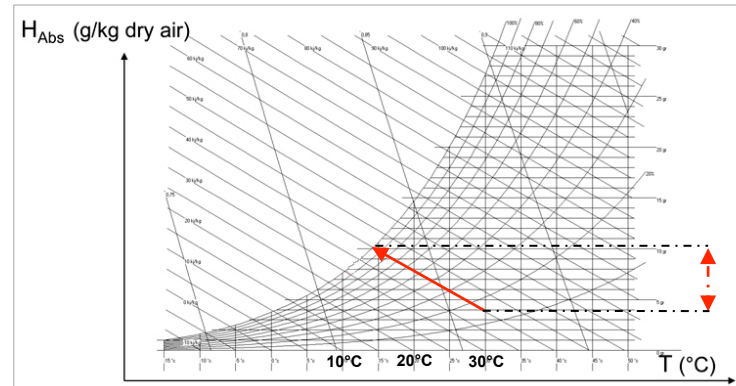
- Moist air and chiller

Initial conditions :

30°C & 15%HR

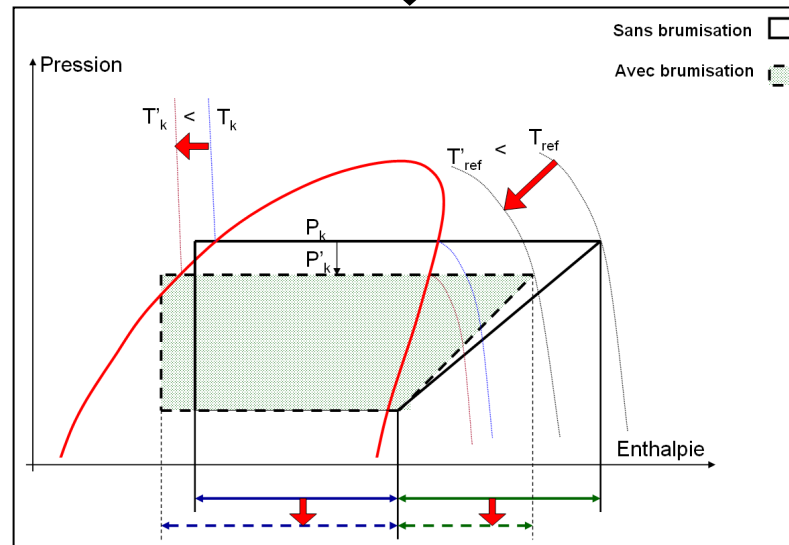
After spraying :

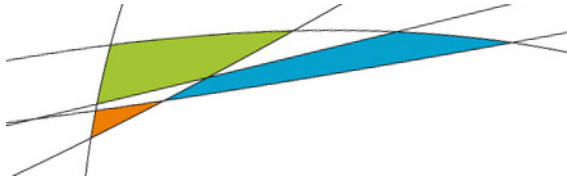
15°C & 100%HR



Amount of water injected to saturate the air (100%HR)

Performance of the chiller





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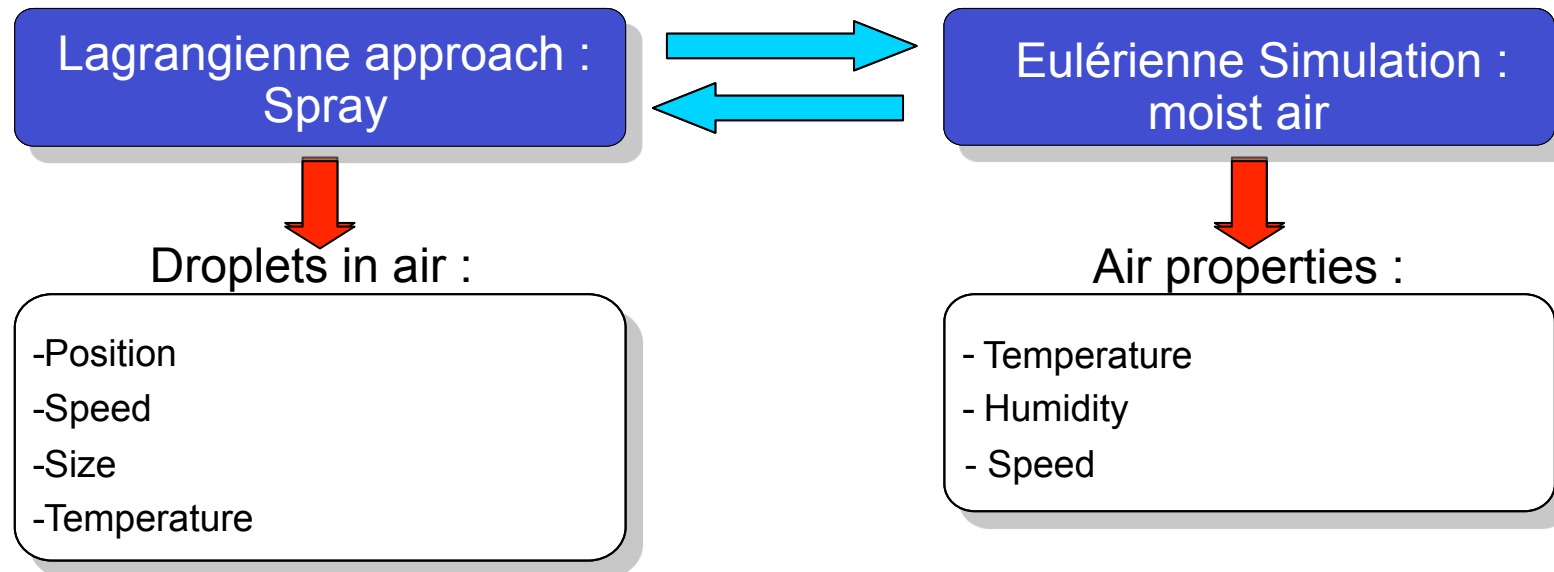


Moyens mis en œuvre

- Theory and numerical tools – J.Tissot PhD 2011 (Lemta/Irstea)

Two-phase flow

[Collin, 2006]

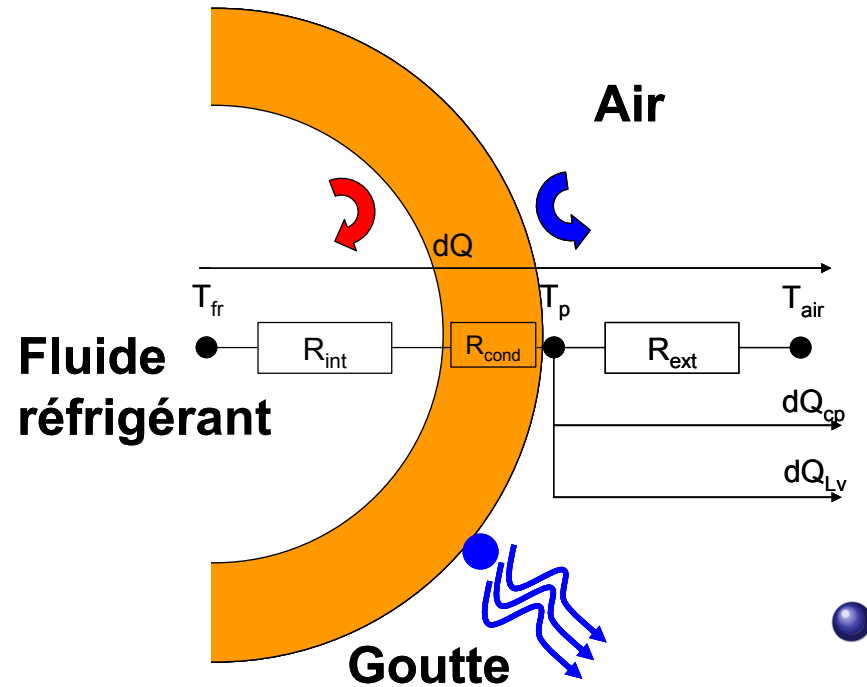




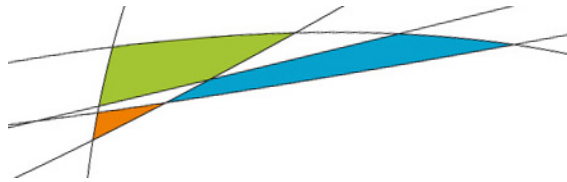
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● Heat transfer _

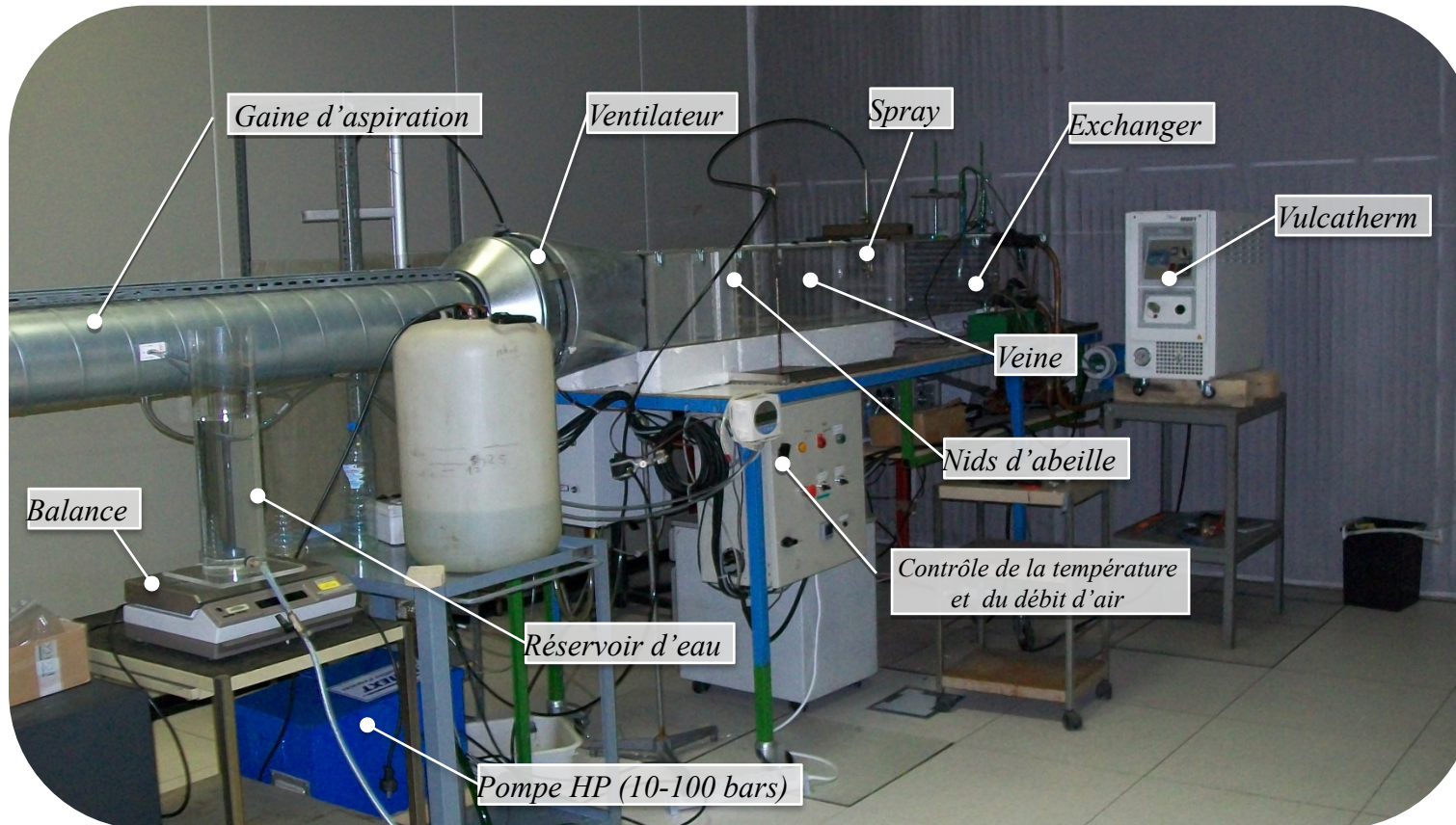


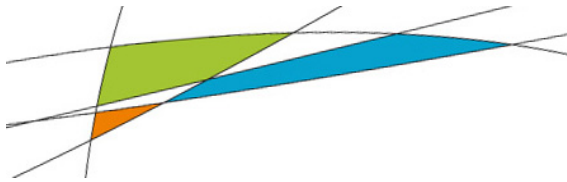
$$dQ = \frac{1}{R_{int} + R_{cond} + R_{ext}} \left((T_{fr} - T_{air}) + (dQ_{Lv} + dQ_{cp}) R_{ext} \right)$$



Moyens mis en œuvre

- Laboratory pilot

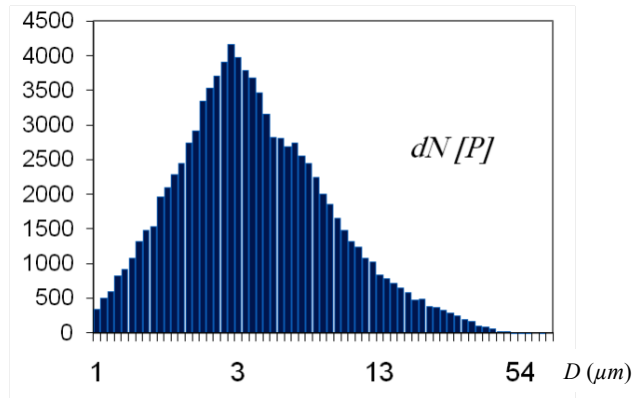




Moyens mis en œuvre

- Metrology developed

Particle size

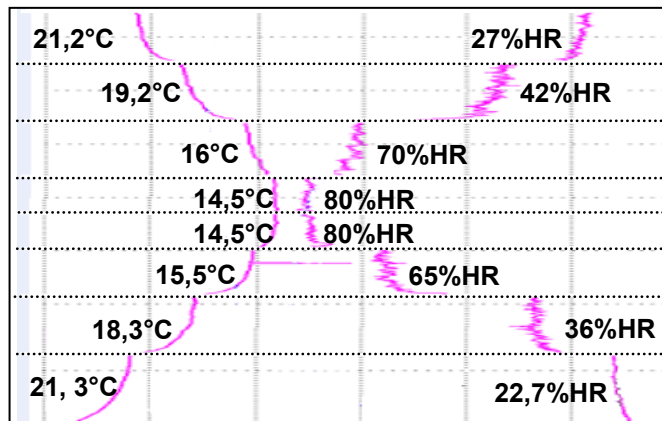
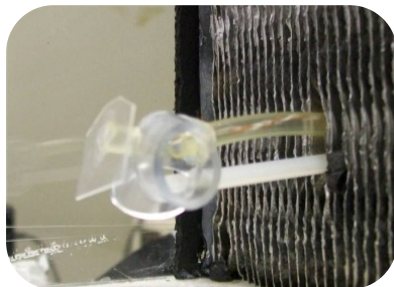


Spray angle



Temperature & humidity

• Thermometers



■ hygrometers





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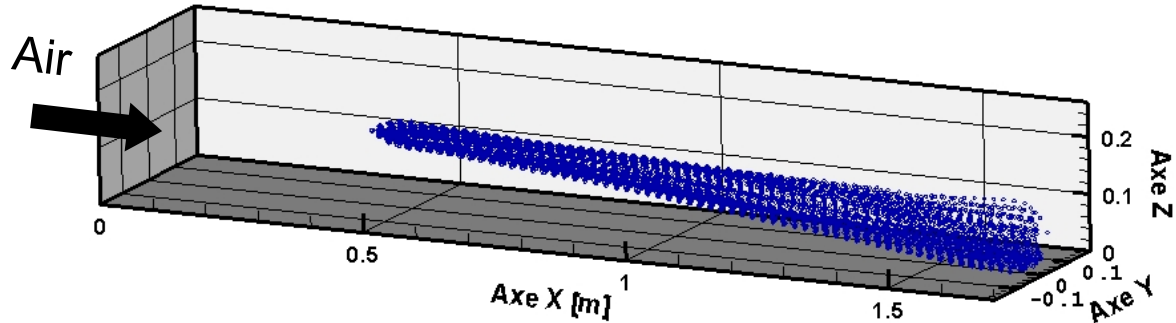


Résultats

- Numerical results

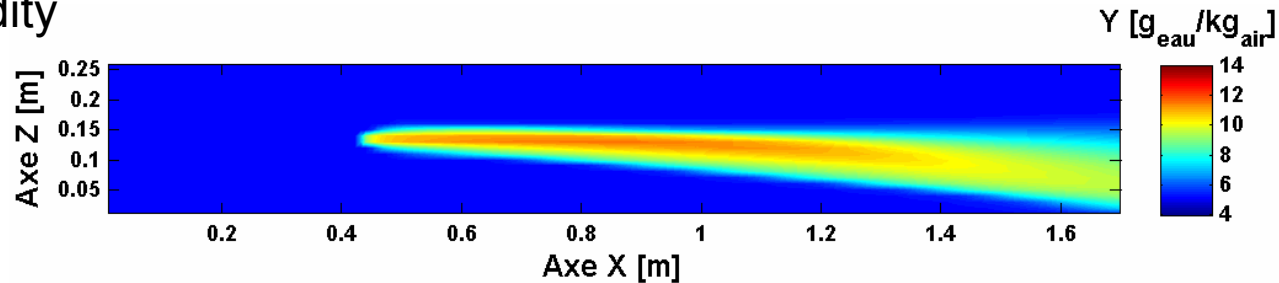
- Trajectory with the air flow (50 μm)

$V_{\text{air}} = 1 \text{ m.s}^{-1}$
 $T_{\text{air}} = 298 \text{ K}$
 $\text{HR} = 30\%$

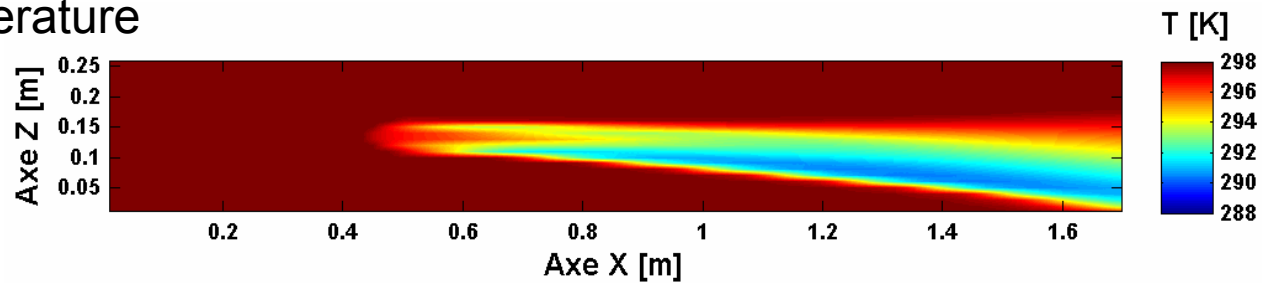


Spray
 $\dot{m}_{\text{spray}} = 1,5 \text{ l.h}^{-1}$
 $V_{\text{spray}} = 10 \text{ m.s}^{-1}$
 $T_{\text{spray}} = 298 \text{ K}$
 $\Phi = 72^\circ$

- Humidity



- Temperature



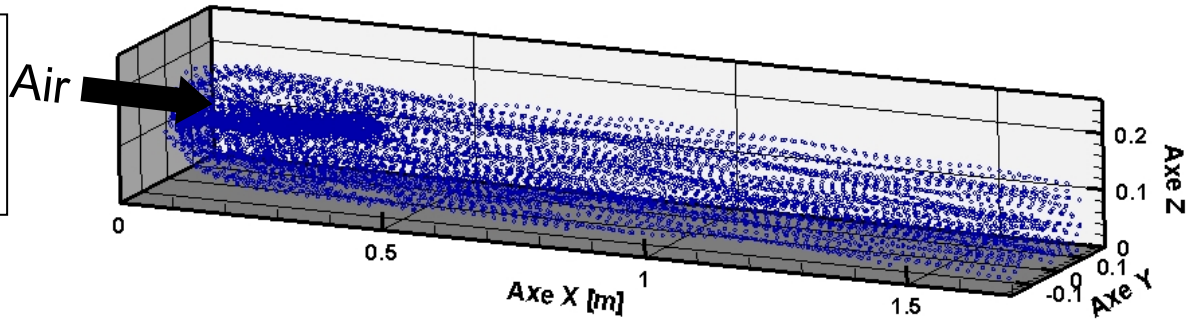


Résultats

- Numerical results
- Trajectory against the air flow (50 μm)

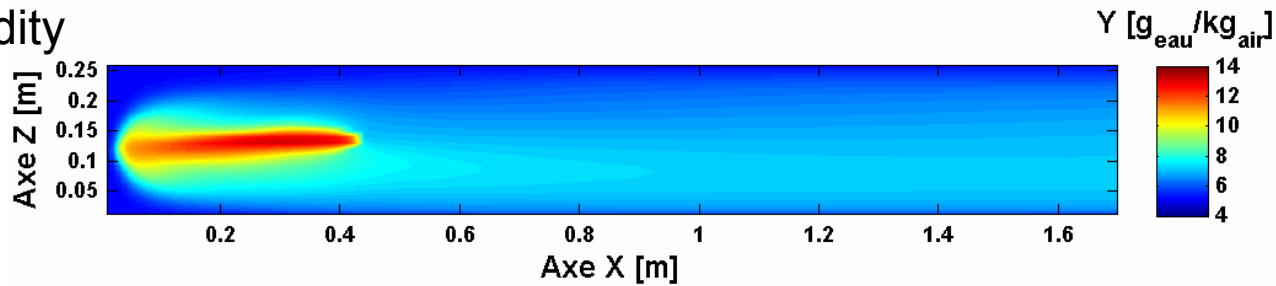
Spray

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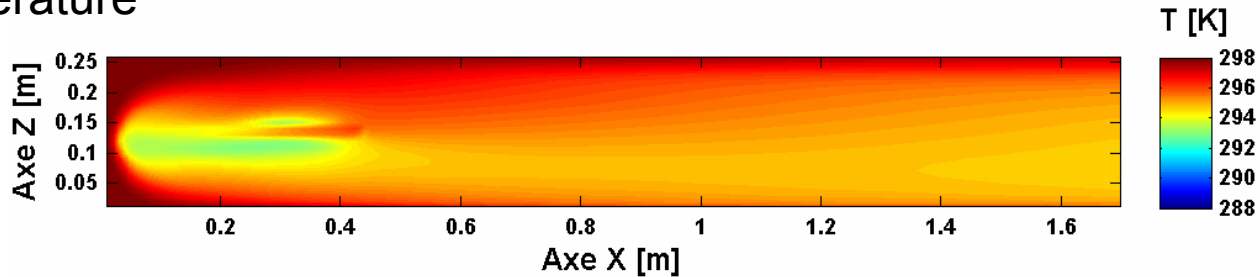


$\text{spray} = 1,5 \text{ l.h}^{-1}$
 $V_{\text{spray}} = 10 \text{ m.s}^{-1}$
 $T_{\text{spray}} = 298 \text{ K}$
 $\Phi = 72^\circ$

● Humidity



● Temperature





Résultats

- Comparison between expérimental résultats and numerical simulation

$T_{\text{air}} = 298,2 \text{ K}$

HR : 30 %

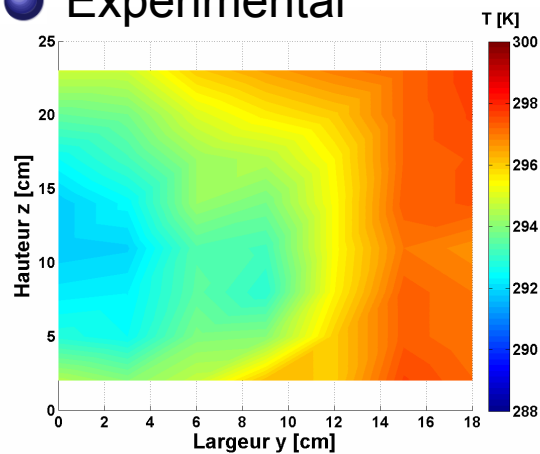
$\dot{m}_{\text{spray}} : 1,4 \text{ l.h}^{-1}$

$\dot{m}_{\text{air}} : 0,1 \text{ m}^3.\text{s}^{-1}$

Distance [cm]	Mean température [K]	
	Expérimental	Numérique
5	295	294,9
20	295,1	294,7
40	294,9	294,6
60	294,8	294,6

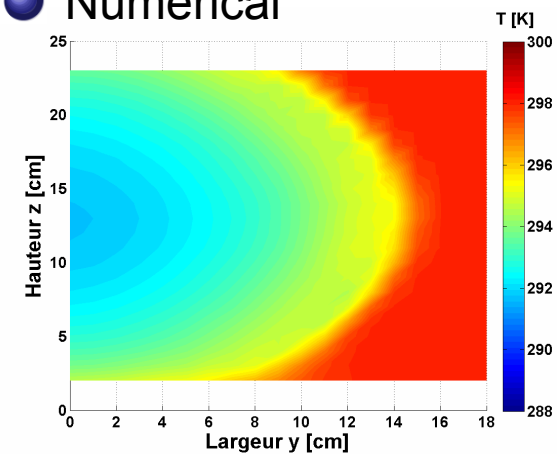
Low temperature variation with distance

● Experimental



At 5 cm of the injection point

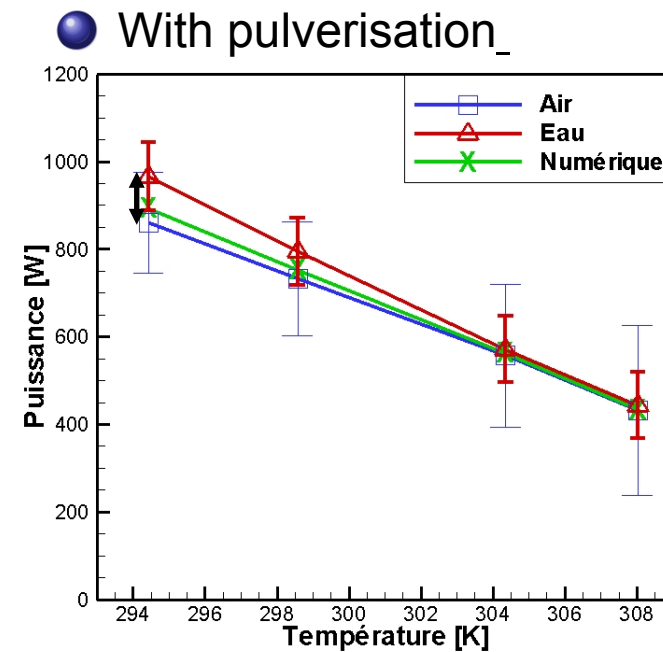
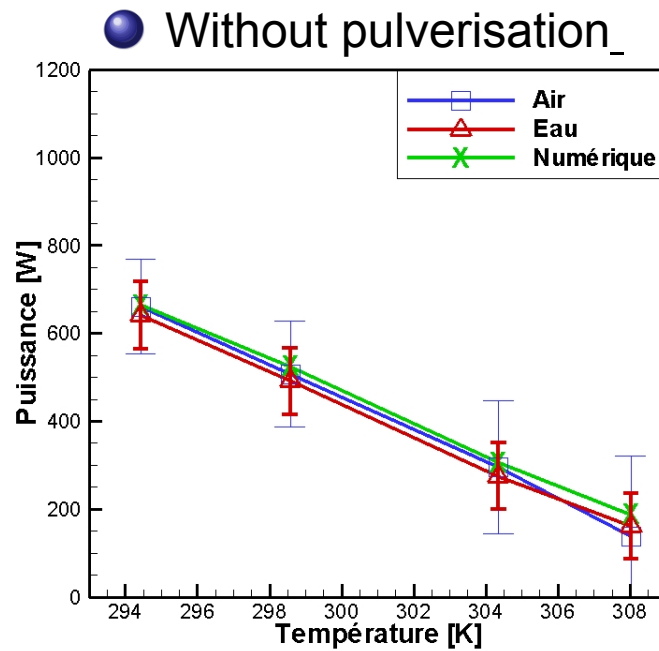
● Numerical





Résultats

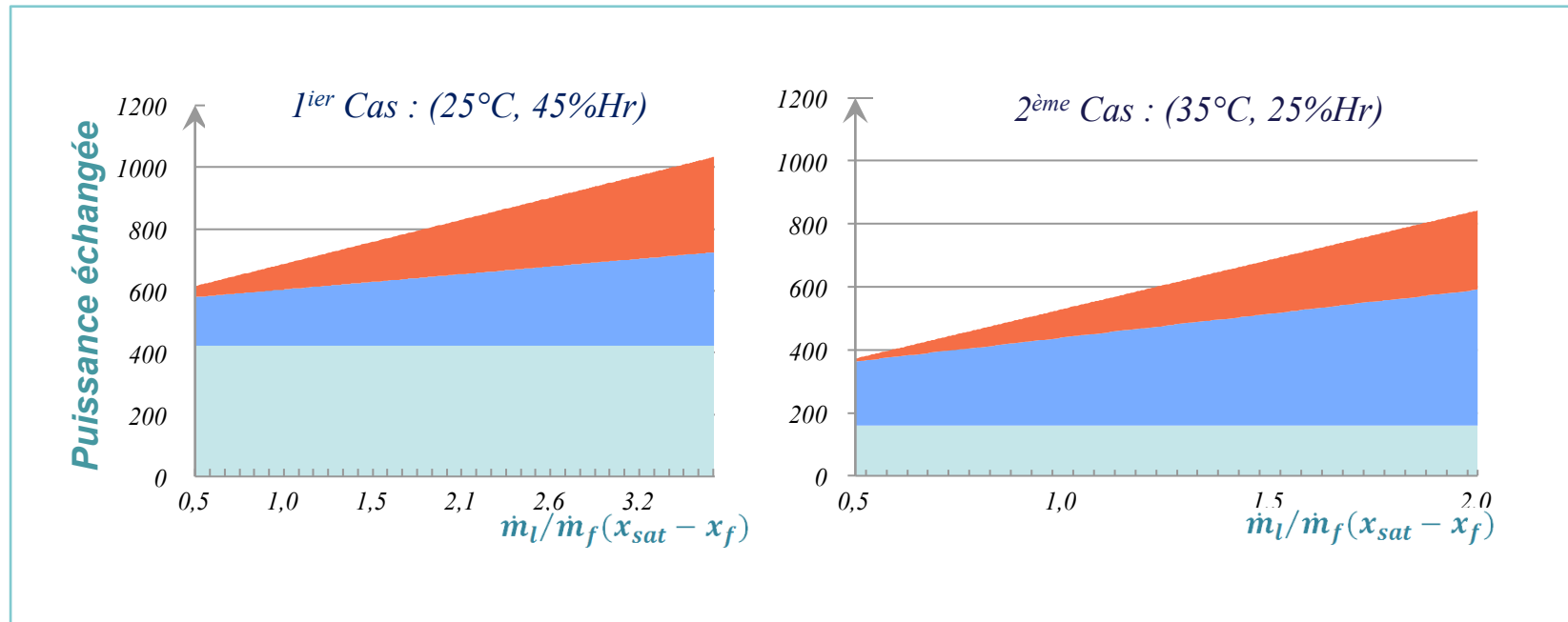
- Comparison between experimental results and numerical simulation








Résultats

- Experimental results

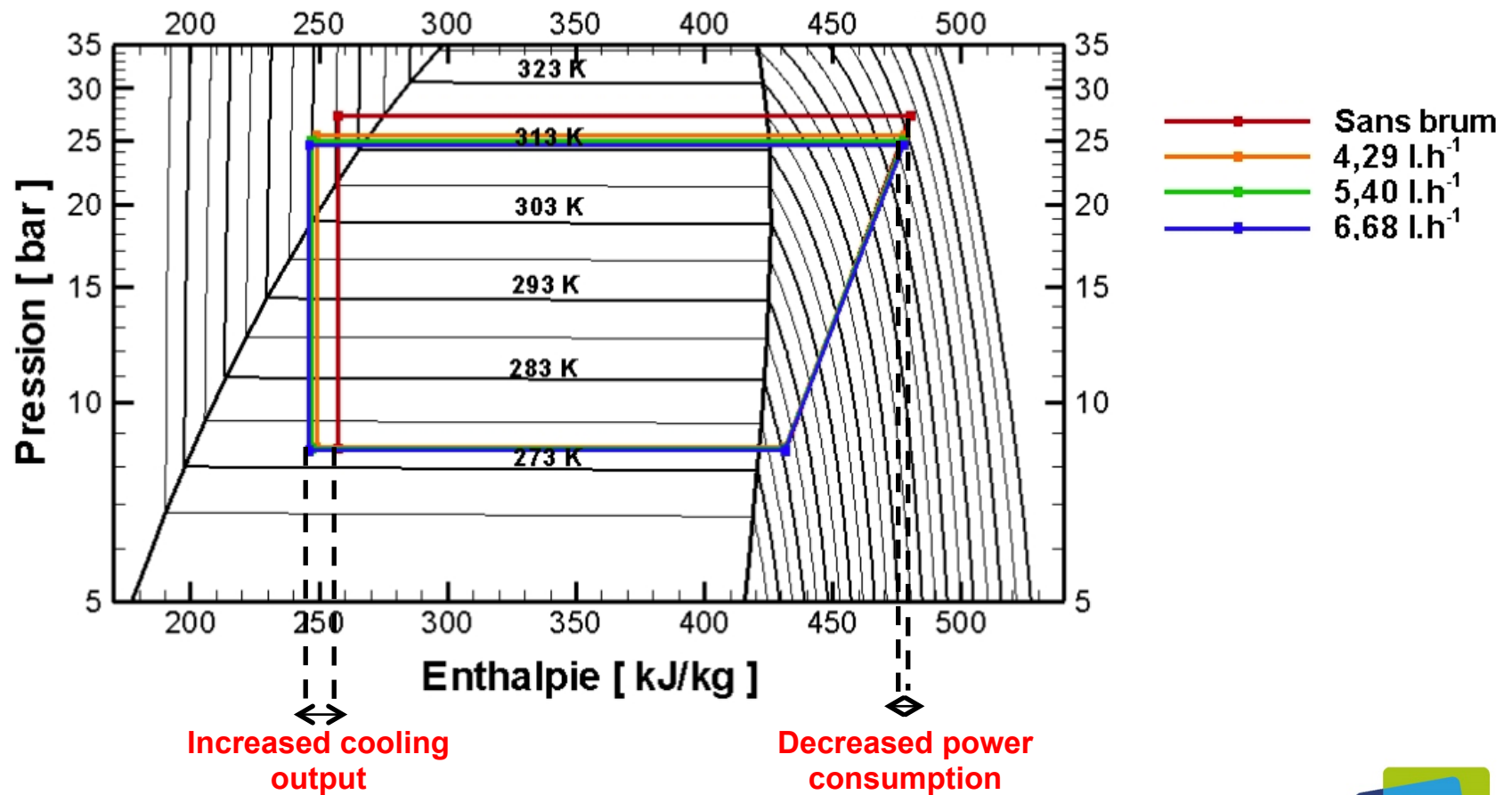


-  Droplets impzct
-  Cooling air
-  Exchanged power without spraying



Résultats

- Effect of the spray on the chiller cycle (SprayPAC project – CIAT – ADEME)





Résultats

- Effect of spray on the chiller

% Evaporation

Up to 86 %

($T_{\text{air}} = 293 \text{ à } 308 \text{ K}$ et $\text{HR} = 47 \text{ à } 20 \%$)

Power consumption

↘ 10 à 25 %

Cooling production

↗ 6 à 8 %

$$\text{gain} = \frac{|P_{\text{sans brum}} - P_{\text{avec brum}}|}{P_{\text{sans brum}}}$$

Coefficient of performance

COP

↗ 13,5 à 29 %

COP with spraying system

↗ 9 à 23 %

$$\text{COP} = \frac{P_{\text{utile}}}{\sum P_{\text{consommée}}}$$



Conclusion & perspectives

- **Conclusion**

- Spraying against the current more effective :

- Uniformity of temperature distributions upstream of the heat exchanger.*

- Identifying the part due to the impact of water droplets on the heat exchanger on the intensification

- Implementation of a suitable metrology

- Improvement of the coefficient of performance u_o to 23% in our case of study

- **Perspectives**

- Optimization of the system : development of experimental and numerical tools

- Droplets flow through a heat exchanger

- Cost of the dispersion phase production